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HESSELØ OFFSHORE WIND FARM

SITE INVESTIGATIONS FOR HDD

GILBJERG HOVED



HESSELØ OFFSHORE WIND FARM SITE INVESTIGATIONS FOR HDD GILBJERG HOVED

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1. EXECUTIVE SUMMARY

This report has been prepared to provide geotechnical, geological, and geophysical data in order to disclose the basic soil conditions for the horizontal directional drilling (HDD) location of Gilbjerg Hoved. A risk assessment has been part of the process whereas potential risks has been identified and evaluated for the HDD.

In order to disclose the basic soil conditions, a site investigation campaign was carried out involving a total of 5 geotechnical boreholes performed on the expected HDD location to the depths from 25 to 50 meters below ground level. Furthermore, approximately 1310 meter of Multi Electrode profiling was carried out.

The HDD crossing will be performed in glacial deposits with a known risk of encountering obstructions such a boulders, cobbles and firm sand deposits. Additionally, the HDD crossing will be performed in saturated and unsaturated sand- and gravel deposits where sufficient pressure can be challenging to maintain during drilling. Furthermore, the HDD crossing should be expected to drill below- and above water table which can require adaptation to maintain sufficient pressure and set-up.

In connection with the design and planning of the HDD, calculations to evaluate the factor of safety against blow up of drilling fluid should be performed for the HDD crossing during the final design process. These calculations should be used to determine the maximum fluid pressure limitations and modify the alignment of the HDD, if necessary, to maintain appropriate factors of safety against blow up.

Furthermore, additional factors must be implemented to reduce the potential for blow up of drilling fluids, including the following:

- Preparing spill prevention, control, and countermeasure for the HDD crossing
- Establishing minimum requirements for HDD contractors
- Requiring HDD contractors to develop and follow fluid monitoring programs and blow up prevention plans.

2. INTRODUCTION

2.1 General

Rambøll has been appointed to perform the geophysical and geotechnical site investigation for a planned HDD at the location of Gilbjerg Hoved in the northern part of Zealand.

This report summarizes the results of the performed geophysical and geotechnical investigation.

This report provides recommendations and a risk assessment for tackling problems in the subsurface when using the horizontal directional drilling (HDD) technique for the crossing. HDDs will typically be considered where obstacles at the ground surface, such as sand dunes, protected areas, roads, railway, and water channel, make traditional cut and cover pipeline installation problematic, or where natural amenities such as the wet area are crossed.

This report contains a description of the proposed project, information on the HDD installation technique, a summary of the location where this technique is being considered and discussions concerning surface, geological, and geotechnical conditions at the location. An assessment of the risks for the successfully completing an HDD installation at the locations is provided based on all available information.

All boring locations and depths and sites for geophysical investigations have been selected and defined by Energinet.

2.2 Project description

2.2.1 Background

In June 2020 the Danish Parliament decided to commence the development of the offshore wind farm (OWF) project, Hesselø aiming for a capacity of ca. 1000 MW. It is planned to build and connect the OWF to the Danish onshore electrical grid.

The OWF site is located in the inner Danish Sea, Kattegat, and has been subject to screening studies. The area of investigation subject to the OWF spans an area of ca. 247km².

Following the political decision, the Danish Energy Agency has instructed Energinet to initiate site investigations, environmental and metocean studies and analysis for grid connection for the area of investigation.

On the basis of the instruction from the Danish Energy Agency, Energinet requests Rambøll to carry out a geotechnical and geophysical site investigation at the landing site of the export cable from the OWF prior to the planning and execution of an HDD (Horizontal Directional Drilling).

2.2.2 The project

The HDD process involves boring under a feature and pulling the pipeline into place through the borehole that has been reamed to accommodate the diameter of the pipeline.

This process has three main phases: pilot-hole drilling, subsequent reaming passes, and pipe pullback. These phases will not be described in further details since the techniques are assumed to be familiar to the contractors.

Figure 2-1 presents an overview map of the location. Figure 2-2 presents an overview map of the planned HDD position at Gilbjerg Hoved.

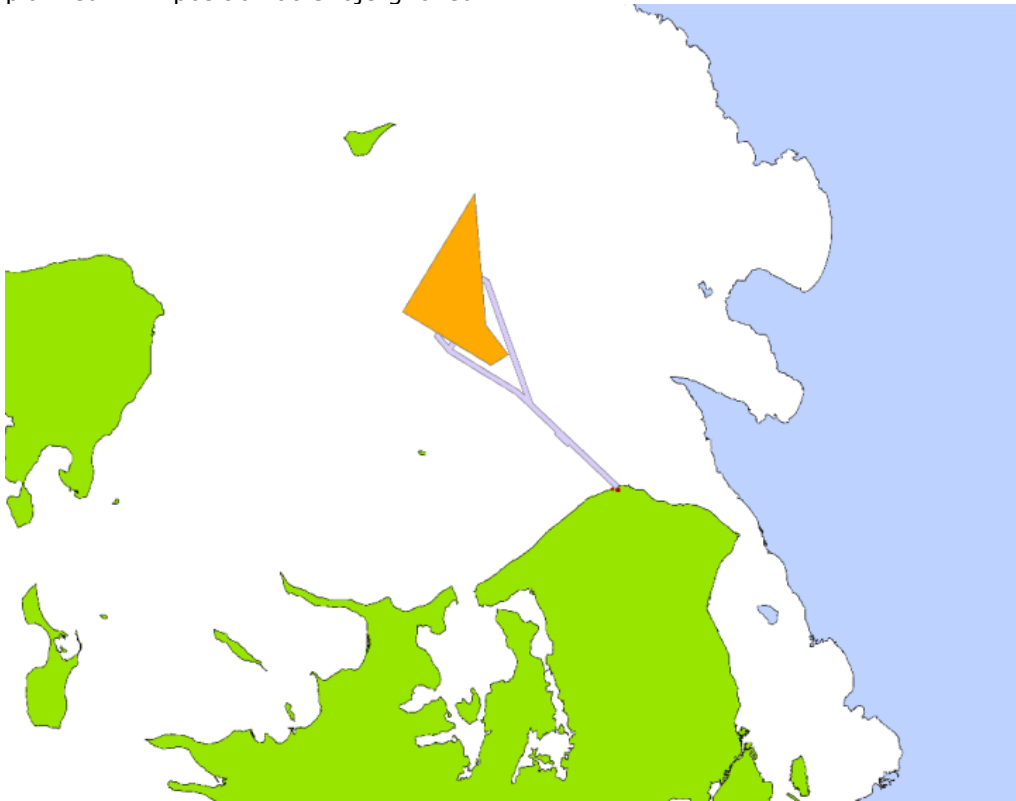


Figure 2-1: Overview map of the location. Orange polygon: OWF area. Pink polygon: cable routes ending at the landing site at Gilbjerg Hoved west of Gilleleje.

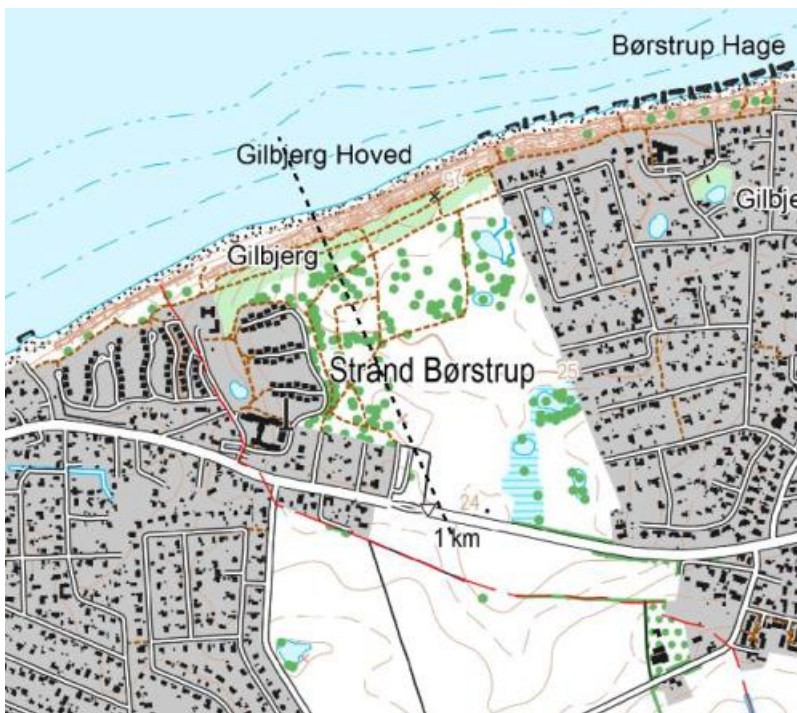


Figure 2-2: Black dotted line: Planned HDD position, Gilbjerg Hoved.

2.3 Regional geological background

2.3.1 General geology

The landscape in the northern part of Zealand was created by a series of glaciations.

The surface soils in the northern Zealand are dominated by Clay Till, meltwater sand and gravel.

The Quaternary landscape of the northern Zealand is the result of a series of events in Late Weichsel glaciation. The period extends about 25.000 to 11.000 years back. During this period, three major glaciers formed the landscape present today. First The Kattegat Isstrøm (Kattegat Iceflow) from South Norway, followed by a mid-Sweden glacial advancement called NØ-isen (NE-ice) ending with a progression from East, The Østjyske Isstrøm. Several locations show how the ice has folded, stacked and pressed up the Kattegat Isstrøm and NØ-isen, forming elongated slightly twisted N-S directed moraines. Between these elongated moraines are valleys with meltwater deposits. These meltwater rivers flowed from south to north, draining large dead-ice areas around Esrum Sø. The imprints of these meltwater rivers are still seen today and are now known as Esrum Ådal and Pandehave Ådal.

A cross-section of Esrum Ådal is shown in Figure 2-3 where the Kattegat Isstrøm was responsible for the lowermost Till deposits and the NØ-isen, the upper most Till-deposits, the section is separated by meltwater and lake- deposits.

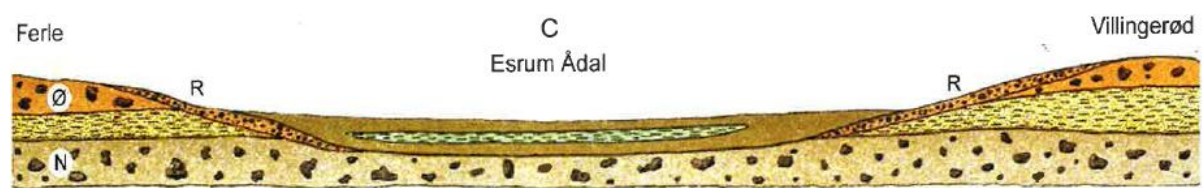


Figure 2-3: From Houmark-Nilsen, 2021 [4]. Terrain model of an area between Gilleleje and Esrum. Ø = Upper Till deposited by the NØ-isen/NE-ice. N = the Lower most Till deposited by the Kattegat Isstrøm/ Kattegat Iceflow. R = Pebble Gravel. N and Ø are separated by meltwater deposits.

2.3.2 Local geology

The survey area is located in an area dominated by meltwater deposits. The nearest archive boreholes in the area are >200 meters away from the current area of study. Due to the large distance, it won't be relevant to take this material into consideration.

The geological map, Figure 2-4, is a representation of the present geology in 1,0 m depth. As seen on Figure 2-4, the boreholes are all positioned in the meltwater deposit-zone, except for BH05 which is located near the coastline and therefore in a marine environment. As described above, the geological map is a representation only of the uppermost 1,0 m soil, and it can be expected, that the meltwater deposits that characterize the four other boreholes will define BH05 as well.

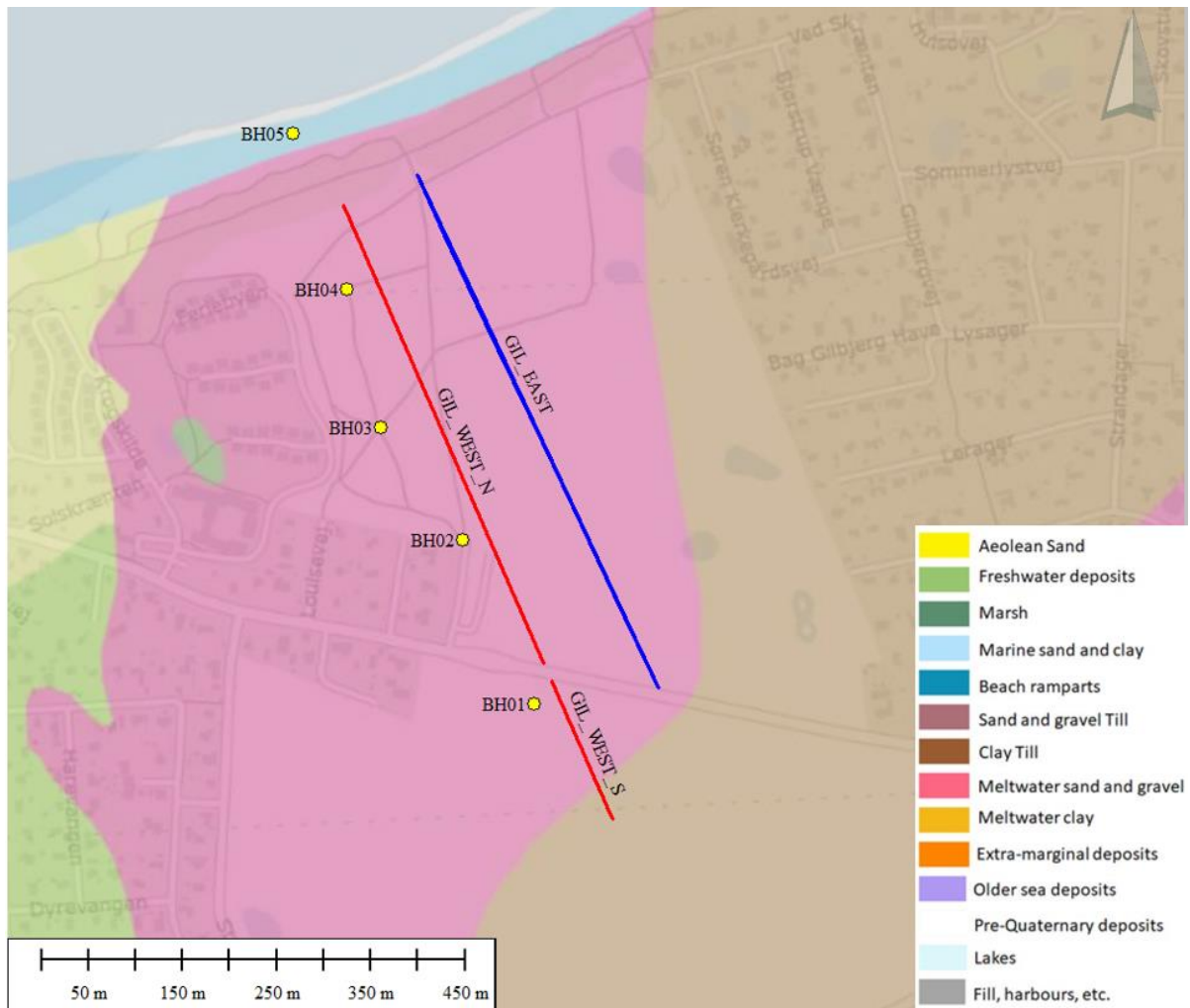


Figure 2-4: Geological map of the survey area including legend, borehole positions and (blue and red) MEP-interpretation lines

3. PURPOSE OF THE INVESTIGATION

The purpose of the site investigations is to investigate and document the geotechnical and geological conditions along with the possible lines for the HDD, so that:

- Informing the client and HDD suppliers about the ground conditions
- Decreasing the soil-related risks for performing HDDs
- Selection of HDD equipment feasible for performing the planned HDDs
- Design of the HDD underground trajectory

The work has been carried out in accordance with Eurocode EC7, Part 1, Part 2, with its associated Danish Annex, DS/CEN ISO/TS 17892 and the Danish Geotechnical Association's Bulletins.

4. EXTEND OF FIELD INVESTIGATIONS

4.1 General

In accordance with the program of the site investigation campaign, a total of 5 boreholes have been performed on site to depths from 25 to 50 meters below ground level (bgl). For this, a total of 160 borehole meters was completed. Furthermore approximately 1310 m Multi Electrode Profiling (MEP) was carried out on site.

Table 4-1 provides details about the five geotechnical boreholes.

Table 4-1: Boreholes drilled at the HDD-site

Borehole [-]	Depth [m]	Date [YYYYMMDD]	Projection [-]	X [-]	Y [-]	LSYS [-]	Z [m. DVR90]
HESS.HDD.BH01	25,00	2022-05-17	UTM32E89 ETRS89	703431	6224376	DVR90	+17,80
HESS.HDD.BH02	25,00	2022-05-03	UTM32E89 ETRS89	703355	6224550	DVR90	+20,39
HESS.HDD.BH03	35,00	2022-05-31	UTM32E89 ETRS89	703268	6224669	DVR90	+20,64
HESS.HDD.BH04	50,00	2022-05-23	UTM32E89 ETRS89	703233	6224815	DVR90	+30,64
HESS.HDD.BH05	25,00	2022-04-25	UTM32E89 ETRS89	703176	6224980	DVR90	+3,13

Per Aarsleff has carried out setting out of borehole positions in the field with GPS and with reference to the coordinate system ETRS89 UTM32N and DVR90.

Boreholes were performed by Per Aarsleff with the shell and auger method as 6" to 8" drillings with casing. The geotechnical field exploration program was performed in the April and May 2022.

The geophysical measurement was carried out by Rambøll in April 2022.

An overview of legend and definitions are provided in Appendix 1.1.

Borehole location plans- and MEP location plans are provided in Appendix 2.1.

Geotechnical- and geophysical longitudinal profiles for respectively the western and eastern site investigation lines, are provided in Appendix 3.1-3.4.

4.2 Extend of geotechnical investigations

During drilling strata boundaries were recorded and soil samples were taken as bag samples (disturbed samples) and A-tubes for geological assessment, classification tests and thermal resistivity tests. Disturbed soil samples were collected at depths of 0.2 and 0.5 m and then generally every 0.5 m, and at least one sample per strata. If assessed possible A-tubes were extracted at an interval of 5 meter. In case of a soil stratum consisting of sand or gravel big bags have been collected instead of the A-tubes.

Field vane tests have been performed in cohesive soils (clay and silt) in accordance with Reference sheet no. 1 from Danish Geotechnical Society in order to evaluate the undrained shear strength (c_u , c_{ur}). Standard Penetration Tests have been performed in cohesionless layers in accordance with Reference sheet no. 3 from Danish Geotechnical Society in order to evaluate the relative density and the angle of internal friction (ϕ') in the sand.

A total of 4 standpipe piezometers ($\varnothing 25\text{mm}$) have been installed in borehole BH01-BH04 for registration of the groundwater table. In borehole BH05, no standpipe piezometers have been installed as the borehole is located near the coastline and therefore sealed upon termination of the drilling.

A total of 5 attempts of extracting A-tubes were done, however, failed due to the tube being damaged in all the attempts.

The recovered samples have been geologically described in the laboratory. On all samples, the water content has been determined.

Boreholes were sealed with bentonite pellets after completion and just after the final round of ground water soundings were collected.

4.2.1 Laboratory tests

The laboratory works have included geological description of the soil samples in accordance with Danish Geotechnical Society Bulletin, denoted DGS, ref. [1].

Based on the site investigation results Rambøll prepared laboratory testing proposals for each borehole, which were approved by Energinet before commencement.

The program included classification tests as well as advanced laboratory tests:

- Determination of the moisture content in accordance with Danish Geotechnical Society Bulletin 15, section 3.1, approximately per meter.
- Particle size distribution including hydrometer testing in accordance with CEN ISO/TS 17892-4 performed on selected samples.

A limited amount of laboratory tests was performed due to the relatively homogenous soil conditions that were found in the geotechnical boreholes.

The borehole logs are provided in Appendix 4.1-4.5.

Laboratory test results from the particle size distribution are provided in Appendix 5.1-5.5.

4.2.2 Comments to geotechnical drilling works

Comments provided by the driller during the performed drilling works, concerning general drilling and complications such as milling and presence of stones or boulders, are presented in Table 4-2 below. For further detailed, refer to the field logs in Appendix 6.1-6.5.

Table 4-2: Overview of the comments to the geotechnical drilling works

Borehole [-]	Depth [m]	Comment [-]
HESS.HDD.BH01	25,00	<ul style="list-style-type: none"> • Presence of very sandy Clay Till layers at the top of the strata. • Presence of silty and gravelly sand layers embedded below the Clay Till layers, to the bottom of the strata. • Vane test (V5) in Sand Till. measured maximum strength at 3,40 meters bgl. • Vane test (V4) in Clay Till measured maximum strength at 4,40 meters bgl
HESS.HDD.BH02	25,00	<ul style="list-style-type: none"> • Presence of sand layers with gravel and stones throughout the strata. • Milling from 13,00-13,25 meters bgl. Approximate milling duration, 3,5 hours. • Milling from 14,00-14,25 meters bgl. Approximate milling duration, 2,0 hours. • Milling from 16,10-16,36 meters bgl. Approximate milling duration, 1,0 hour. • Milling from 17,30-17,50 depth bgl. Approximate milling duration, 1,0 hour.
HESS.HDD.BH03	35,00	<ul style="list-style-type: none"> • Presence of stony, gravelly, and silty sand layers throughout the strata has slowed the borehole drilling.
HESS.HDD.BH04	50,00	<ul style="list-style-type: none"> • Presence of stony, gravelly, and silty sand layers throughout the strata has slowed the borehole drilling.
HESS.HDD.BH05	25,00	<ul style="list-style-type: none"> • Presence of stony, gravelly, and silty sand layers throughout the strata has slowed the borehole drilling.

Furthermore, all attempts of extracting A-tubes have resulted in the tube being damaged.

4.2.3 Ground water conditions

Standpipe piezometers have been installed in four out of five boreholes. The measured water levels are listed in the Table 4-3 below. The measured levels and standpipe piezometers can be seen in the borehole logs in Appendix 4.1-4.5.

Table 4-3: Measured water levels

Borehole	Pipe	Terrain	Date	Water depth	Water level
[-]	[mm]	[m. DVR90]	[YYYYMMDD]	[bgl]	[m. DVR90]
HESS.HDD.BH01	Ø25	+17,80	2022-05-17	15,60	+2,20
			Lost due to plowing	-	-
HESS.HDD.BH02	Ø25	+20,39	2022-05-03	18,62	+1,77
			2022-05-27	18,64	+1,75
HESS.HDD.BH03	Ø25	+20,64	-	-	-
			2022-06-10	18,97	+1,67
HESS.HDD.BH04	Ø25	+30,36	-	-	-
			2022-05-27	29,84	+0,52
HESS.HDD.BH05	-	+3,13	Sealed after termination of borehole	-	-

The water level was measured for BH01 on May 17th, 2022, and was observed at a level of +2,20m DVR90. No 2nd observation was made due to the loss of borehole and standpipe piezometer from plowing.

The water level was measured for BH02 on May 3rd, 2022, and was observed at a level of +1,77m DVR90. The 2nd observation on May 27th, 2022, showed a water level at +1,75m DVR90.

The water level was measured for BH03 on June 10th, 2022, ten days after completion of the borehole, and was observed at a level of +1,67m DVR90.

The water level was measured for BH04 on May 27th, 2022, fourteen days after completion of the borehole, and was observed at level +0,52m DVR90.

The water level was not measured for BH05 due to no standpipe piezometer installation as the borehole is located near the coastline and therefore sealed upon the termination of the drilling.

The observation of the measured water levels shows a steady decrease towards the coastline.

4.3 Extend of geophysical investigations

In the geotechnical realm, geophysical methods are valuable in mapping the subsurface, such as including the ability to collect data over large areas in a relatively short period of time. This survey includes the MEP method (Multi electrode profiling) - a geoelectrical geophysical method, whereby it is possible to determine the resistivity of the subsurface.

The method is also called ERT (electrical resistivity tomography) and CVES (continuous vertical electrical sounding) but will be called MEP in this report.

4.3.1 MEP

The resistivity measurements were acquired as MEP with a roll-along technique. The survey lines were acquired with cables with an electrode spacing of 2 m south of Tinkerup Strandvej and with

an electrode spacing of 5 m north of Tinkerup Strandvej. Steel electrodes fastened to the ground were attached to the electrodes on the cables. For each measurement 4 electrodes are actively used, 2 electrodes emit the direct current, and 2 receiving electrodes measure the potential difference between the electrodes in the subsurface. The electrode configuration was set to GradientXL and was measured using a GuidelineGeo Terrameter LS2 instrument. Resistivities are measured in ohm.m.

This method results in a 2D resistivity profile along the measured line. Resistivity is a measure of a materials ability to conduct an electrical current. It is therefore possible to differentiate between materials with low resistivity such as clays, medium resistivity such as saturated sediments, medium-high resistivity such as unsaturated sediments and materials with high resistivity such as very dry coarse-grained sediments or bedrock.

The results from the measurements are presented in section 6 and the technical drawings are presented in Appendix 3.1-3.4

4.4 Results

The siteplan and the longitudinal profiles for the HDD site are provided in Appendix 3.1-3.4

Geotechnical borehole logs are provided in Appendix 4.1-4.5, including site investigation results and laboratory results from moisture content and bulk density/unit weight.

Laboratory test results from particle size distributions are provided in Appendix 5.1-5.5.

Field logs are provided in Appendix 6.1-6.5.

The risk analyses are provided in appendix 7.1.

5. HDD CROSSING CONDITIONS

Surface and subsurface conditions at the proposed HDD crossing location are provided in this section. Discussions of subsurface conditions include information from published geological mapping, groundwater observations, and conditions observed in geotechnical boreholes. Based on this information, an interpretation of the geological and geotechnical conditions at the HDD location is provided.

5.1 Ground properties

For the HDD construction both lower and upper values of strength parameters are required. The low characteristic values of strength parameters will mainly be needed for design of possible temporary constructions like sheet pile walls, containment dams or possible foundations etc. The high values of the strength parameters are mainly needed for the HDD contractor to assess the method and suitability of the drilling equipment, to assess the time for drilling and estimate the abrasion of the bit and drill rods for the job and to estimate pullback forces.

Proper selection of reamer and the number of passes needed depends on soil conditions, the hole size and pump capacity.

For installation in quaternary deposit (till and sand) as described in the boreholes a substantial wear (the borehole drilling works has been challenged by the ground conditions) on machinery should be expected. Enlarging the hole size to much in one pass will wear on the machinery. A reamer that is too large will result in excessive torque and pullback loads.

For the site, the intervals (minimum value and maximum value) for the measured (or derived) strength- and deformation parameters for each soil type have been provided in a table with ground properties.

In the tables below the following symbols apply:

γ	:	Soil unit weight – utilized above water level
γ'	:	Submerged soil unit weight – utilized below water level
c_u	:	Undrained shear strength (short term situation)
ϕ'	:	Effective angle of internal friction (long term situation)
c'	:	Effective cohesion (long term situation)

5.1.1 Geotechnical investigations

The geotechnical investigations include several tests performed in the encountered soil types in borehole BH01-BH05. Table 5-1 below, presents an overview of the field- and laboratory tests performed.

Table 5-1: Overview of tests performed in the encountered soil types in borehole BH01-05

Soil Type		No. Of Shear Vane tests	No. Of MC tests	No. Of SPT tests	No. Of particle size distribution
[-]	[Env., Age]	[No]	[No]	[No]	[No]
FILL	Fi, Re	0	7	0	0
SAND	Mw, Lg	0	12	2	1
GRAVEL	Mw, Gc	0	12	3	1
SAND	Mw, Gc	5	191	75	25
GRAVEL TILL	Gl, Gc	0	11	4	1
SAND TILL	Gl, Gc	0	57	14	3
CLAY TILL	Gl, Gc	6	9	1	0
Total		11	299	99	31

The sections below, present a general description of the encountered soil types and present the interpreted results for each soil type encountered.

5.1.1.1 FILL, Fi, Re

In borehole BH01, BH02 and BH03, fill has been observed in the top of the strata as sandfill, fine – medium, mully, slightly gravelly, slightly silty dark yellowish brown, and not calcareous. In some samples, plant remains have been observed. Laboratory tests have been performed in the fill layers and below are the results summarized and depicted as a range and average value in Table 5-2. No field tests have been performed in the fill layers.

Table 5-2: Laboratory test results of FILL, Fi, Re

Test	Minimum measured value	Maximum measured value	Average value	Number of tests
Moisture content [%]	5,91	10,11	8,18	7
Particle size distribution [No]	-	-	-	0

5.1.1.2 SAND, Mw, Lg

In borehole, BH02 and BH05, lateglacial meltwater sand has been observed in the upper layers near the surface as fine – coarse, slightly silty, a few grains of gravel, dark yellowish brown and slightly calcareous. Laboratory and field tests have been performed in the lateglacial meltwater sand layers and below are the results summarized and depicted as a range and average in Table 5-3. Figure 5-1 presents an overview of the particle size distribution based on 1 test from lateglacial meltwater sand in borehole BH05.

Table 5-3: Laboratory and field test results of sand SAND, Mw, Lg

Test	Minimum measured value	Maximum measured value	Average value	Number of tests
Moisture content [%]	6,10	15,88	12,84	12
SPT [No.]	11	12	11,5	2
Particle size distribution [No]	-	-	-	1

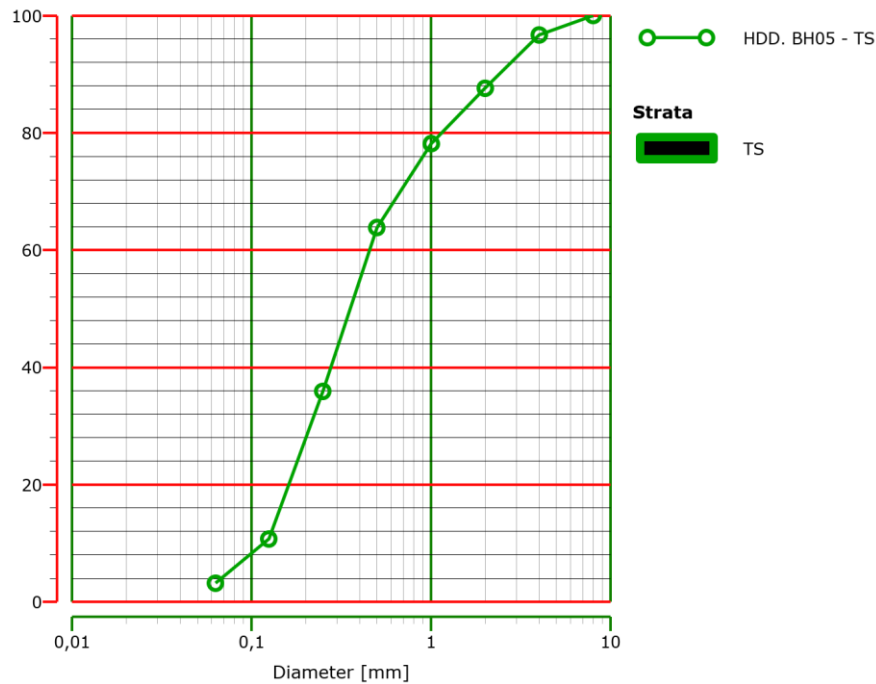


Figure 5-1: Particle size distribution of lateglacial meltwater sand in borehole BH05

5.1.1.3 GRAVEL, Mw, Gc

In borehole BH02 and BH04, glacial meltwater gravel, has been observed in the deeper layers as coarse, sandy, poorly graded, grey, and calcareous. Laboratory and field tests have been performed in the glacial meltwater gravel layers and below are the results summarized and depicted as a range and average in Table 5-4. Figure 5-2 presents an overview of the particle size distribution based on 3 tests from glacial meltwater gravel in borehole BH02 and BH04.

Table 5-4: Laboratory and field test results of GRAVEL, Mw, Gc

Test	Minimum measured value	Maximum measured value	Average value	Number of tests
Moisture content [%]	2,51	12,60	7,20	12
SPT [No.]	12	52	35	3
Particle size distribution [No]	-	-	-	3

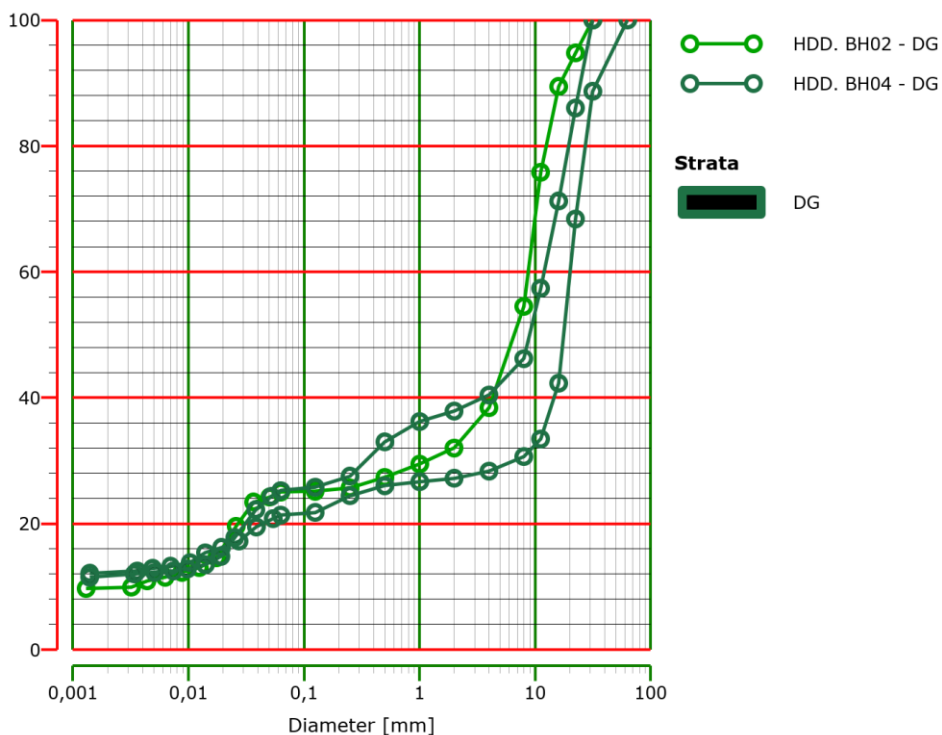


Figure 5-2: Particle size distribution of glacial meltwater gravel in borehole BH02 and BH04

5.1.1.4 SAND, Mw, Gc

In borehole BH01 and BH02, glacial meltwater sand has been observed in the deeper layers as fine – coarse, slightly gravelly, slightly silty, grey, and calcareous. In borehole BH03, BH04 and BH05, glacial meltwater sand has been observed in the upper layers close to the surface, as well as the deeper layers, as fine – medium, sorted, poorly graded, well graded, slightly silty, slightly clayey, dark yellowish brown, brownish grey, calcareous, and slightly calcareous. Laboratory and field tests have been performed in the glacial meltwater sand layers and below are the results summarized and depicted as a range and average in Table 5-5. To be noted, 5 shear vane tests has been performed in layers of glacial meltwater sand. Due to shear vane testing in frictional material, the results are not included to determine the strength or deformation of glacial meltwater sand.

Table 5-5: Laboratory and field test results of SAND, Mw, Gc

Test	Minimum measured value	Maximum measured value	Average value	Number of tests
Moisture content [%]	0	21,63	9,33	191
N _{SPT} [No.]	6	100	39	75
Shear Vane [kPa]	-	-	-	5
Particle size distribution [No]	-	-	-	23

Due to the relatively large number of performed SPT tests in glacial meltwater sand, a statistical approach is used to analyze the plane friction angle, whereby the N_{SPT} values from field tests in borehole BH01-BH05 are derived into plane friction angles in accordance with DS415 and DS/EN [3]. The friction angles represent a conservative estimate of the mean (which is hereafter referred to as the lower average), which represents the average of the values that fall within a 95% confidence interval.

The data population for glacial meltwater sand, can best be approximated by a log-normal distribution. To calculate a conservative estimate of the lower average value, a log-normal distribution is used.

As presented in Figure 5-3, the lower average value of the plane friction angle of glacial meltwater sand is derived to be $\varphi_{pl} = 39^\circ$.

To be noted, the glacial meltwater sand layers have generally been observed with no significant quantities of silt. Therefore, in accordance with DS415 and DS/EN, no deduction of the derived plane friction angle of glacial meltwater sand has been done.

Figure 5-4 presents an overview of the particle size distribution based on 23 tests from glacial meltwater sand layers in borehole BH01-BH05. As presented, BH01-BH05 has silt in its glacial meltwater sand deposits.

To examine the possible relation between depth and silt content in the layers of glacial meltwater sand, the data has been processed whereas particles from the 23 tests passing through 0,063 mm sieve are defined as silt (or clay).

Figure 5-5 presents an overview of the relation between depth and silt content of glacial meltwater sand in borehole BH01-BH05. As presented, the majority of the tests show a small content of silt, whereas no relative relation between depth and silt content were found. However, it should be noted that large amounts of silt were found in borehole BH04, as presented in Figure 5-5. Thus, in accordance with DS415 and DS/EN, it should be considered to deduct the derived plane friction angle in glacial meltwater sand according to the design purpose.

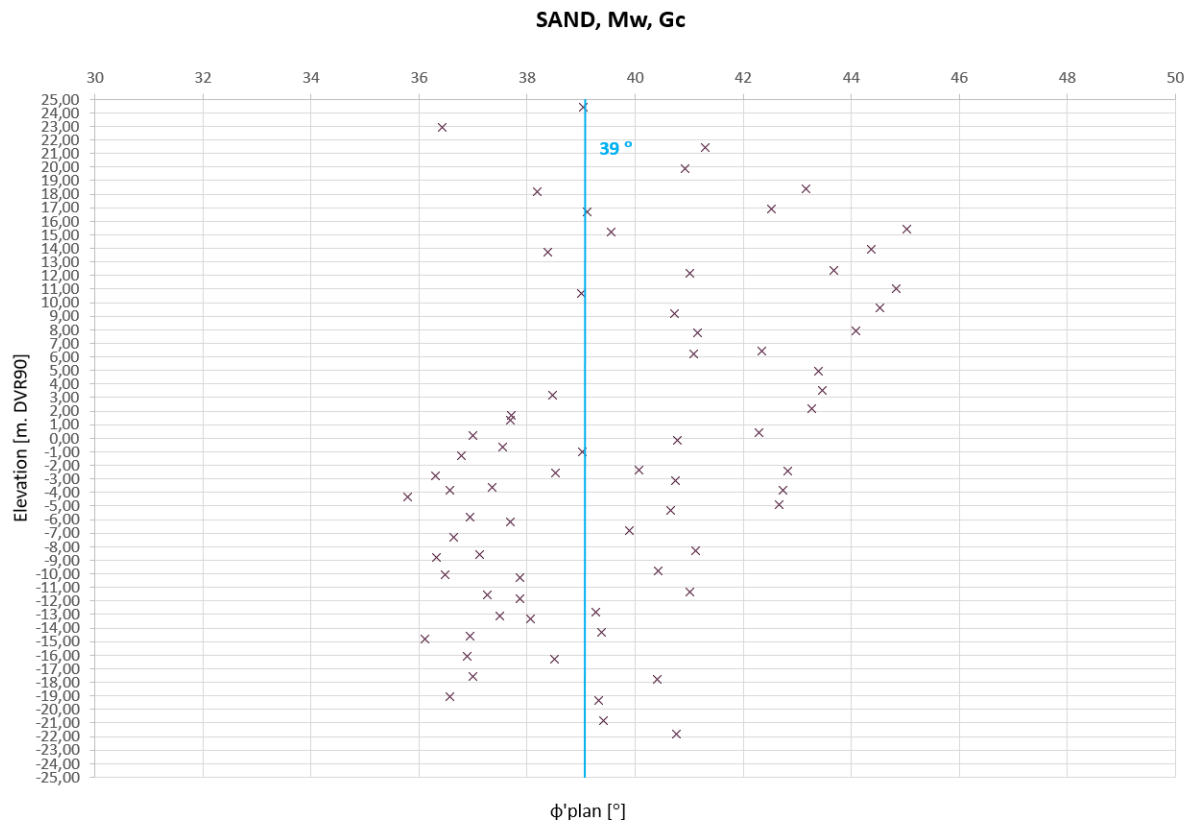


Figure 5-3: The lower average value of the plane friction angle of glacial meltwater sand

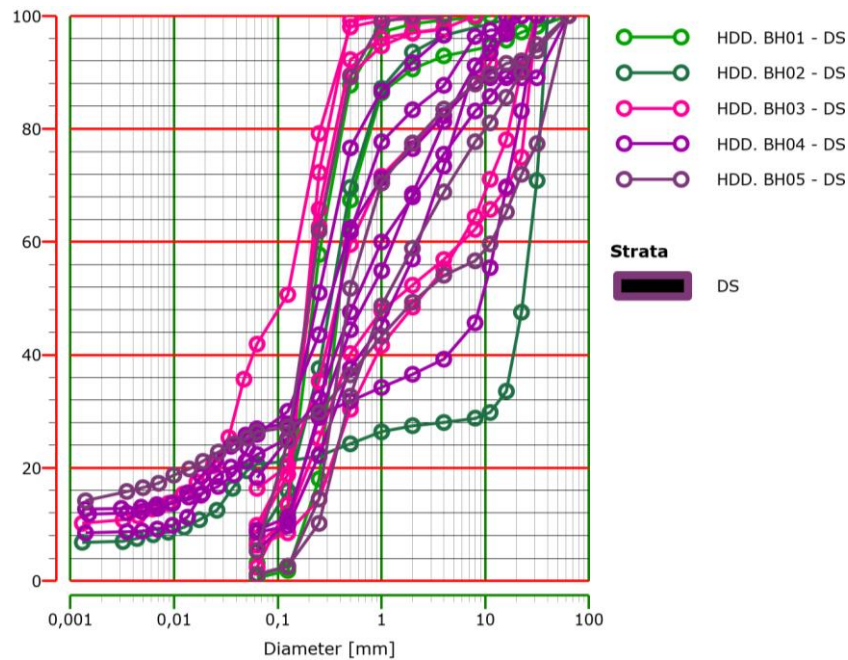


Figure 5-4: Particle size distribution of glacial meltwater sand in borehole BH01-BH05

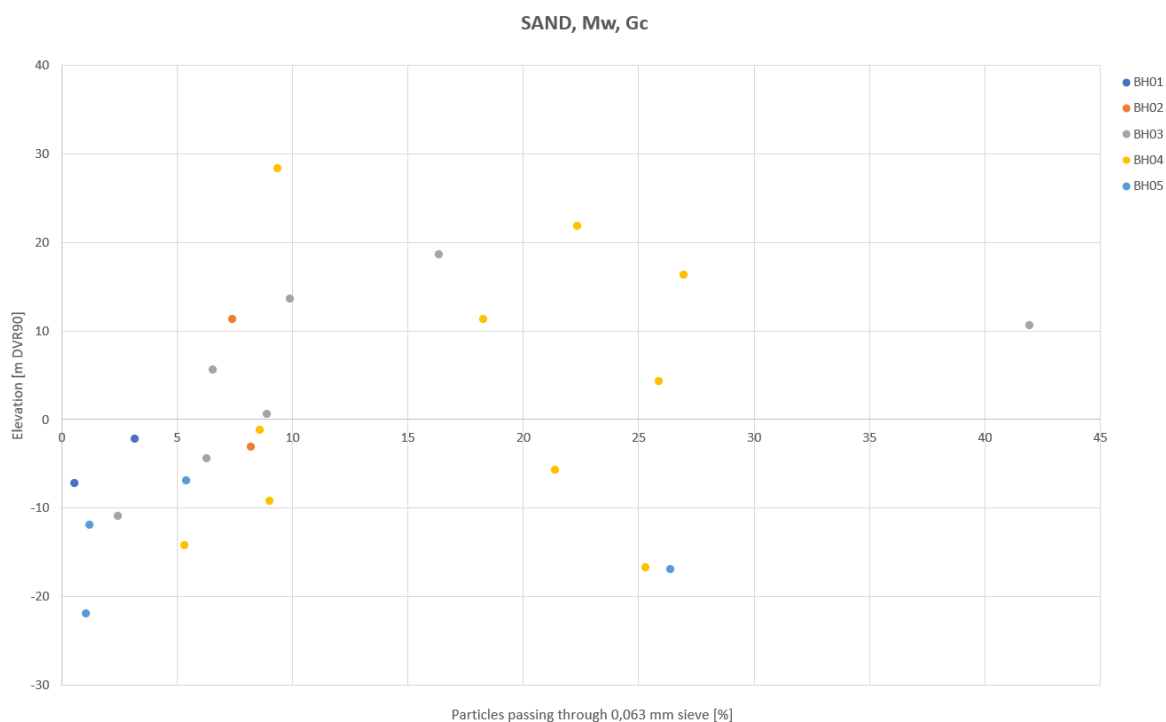


Figure 5-5: Particle size distribution of particles passing through 0,063 mm sieve of glacial meltwater sand in borehole BH01-BH05

5.1.1.5 GRAVEL TILL, GI, Gc

In borehole, BH02, glacial gravel till has been observed in the upper layer as well as the deeper layer as sandy, silty, grayish brown and calcareous. Laboratory and field tests have been performed in the glacial gravel till, layers and below are the results summarized and depicted as a range and average in Table 5-6. Figure 5-6 presents an overview of the particle size distribution based on 1 test from glacial gravel till in borehole BH02.

Table 5-6: Laboratory and field test results of GRAVEL TILL, GI, Gc

Test	Minimum measured value	Maximum measured value	Average value	Number of tests
Moisture content [%]	5,74	17,64	10,16	11
SPT [No.]	27	100	62	4
Particle size distribution [No]	-	-	-	1

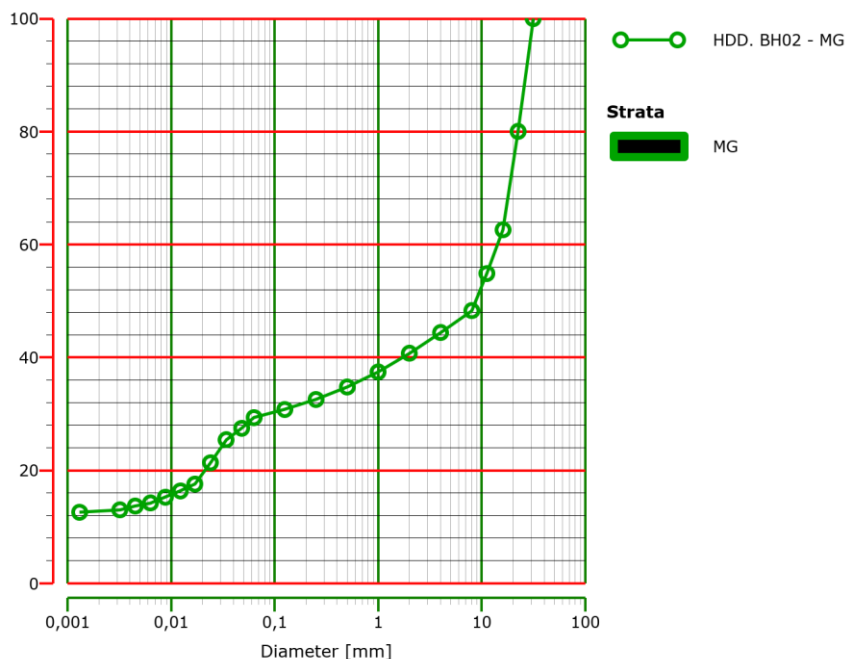


Figure 5-6: Particle size distribution of glacial gravel till in borehole BH02

5.1.1.6 SAND TILL, GI, Gc

In borehole BH01 and BH02, glacial sand till has been observed in the upper layers as well as the deeper layers as silty, gravelly, slightly clayey light yellowish brown, olive grey, not calcareous in the upper layers, however calcareous in the deeper layers. Laboratory and field tests have been performed in the glacial sand till layers and below are the results summarized and depicted as a range and average in Table 5-7.

Table 5-7: Laboratory and field test results of SAND TILL, GI, Gc

Test	Minimum measured value	Maximum measured value	Average value	Number of tests
Moisture content [%]	2,11	17,64	7,22	57
SPT [No.]	37	100	62	14
Particle size distribution [No]	-	-	-	3

Due to the relatively large number of performed SPT tests in glacial sand till, a statistical approach is used to analyze the plane friction angle, whereby the N_{SPT} values from field tests in borehole BH01-BH05 are derived into plane friction angles in accordance with DS415 and DS/EN [3]. The friction angles represent a conservative estimate of the mean (which is hereafter referred to as the lower average), which represents the average of the values that fall within a 95% confidence interval.

The data population for glacial sand till can best be approximated by a log-normal distribution. To calculate a conservative estimate of the lower average value, a log-normal distribution is used.

To be noted, glacial sand till, layers have been observed with smaller quantities of silt, and therefore it is assumed that the glacial sand till contains approximately 10% silt. Thus, in accordance with DS415 and DS/EN, 2 degrees is deducted from the derived plane friction angle of glacial sand till.

As presented in Figure 5-7, the lower average value of the plane friction angle of glacial sand till, is found to be $\phi_{pl} = 40^\circ$.

Figure 5-8 presents an overview of the particle size distribution based on 3 tests from glacial sand till in borehole BH01 and BH02.

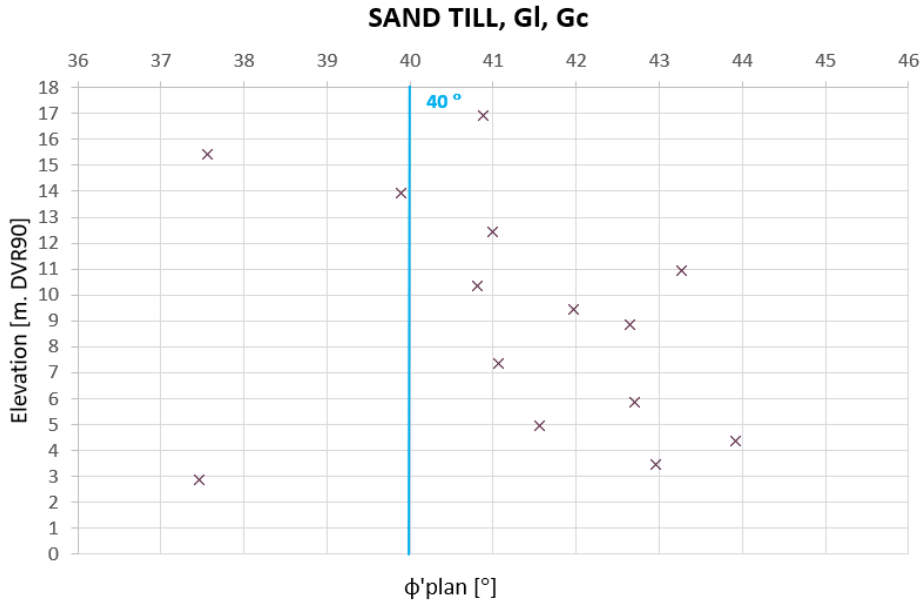


Figure 5-7: The lower average value of the plane friction angle of glacial sand till

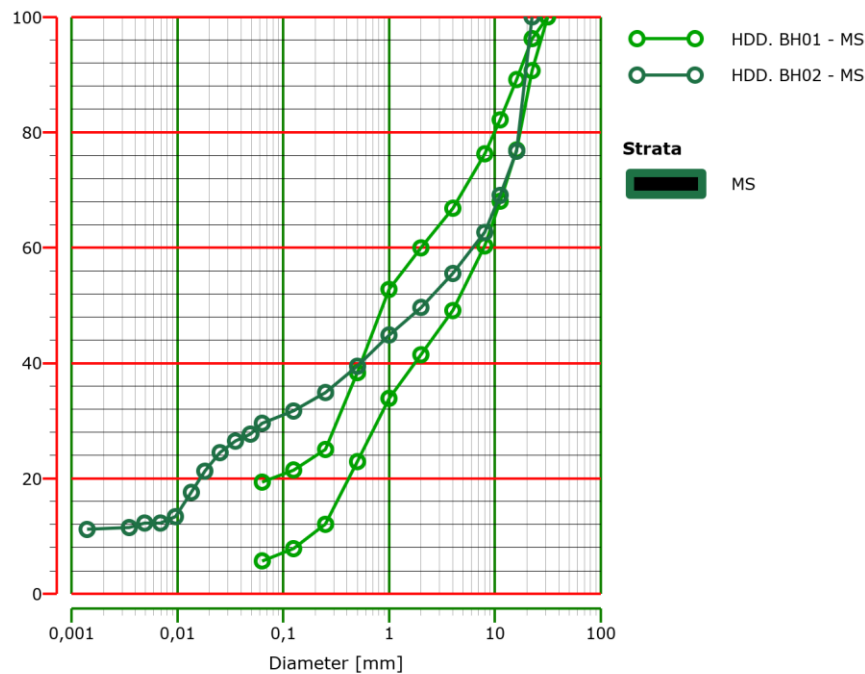


Figure 5-8: Particle size distribution of glacial sand till in borehole BH01 and BH02

5.1.1.7 CLAY TILL, GI, Gc

In borehole BH01, BH02 and BH03 glacial clay till has been observed in the upper layers as silty, very sandy, gravelly, with sand layers, grayish brown, not calcareous in the upper layers, however calcareous in the deeper layers. Laboratory and field tests have been performed in the glacial clay till, layers and below are the results summarized and depicted as a range and average in Table 5-8.

Table 5-8: Laboratory and field test results of CLAY TILL, GI, Gc

Test	Minimum measured value	Maximum measured value	Average value	Number of tests
Moisture content [%]	11,01	21,95	13,66	9
SPT [No.]	48	48	48	1
Shear Vane [kPa]	72	702	392	5
Particle size distribution [No]	-	-	-	0

Due to the relatively low number of performed shear vane tests, the strength- and deformation parameters in glacial clay till, must be determined on the basis of empirical knowledge and reference values.

To be noted, the five shear vane tests performed in glacial clay till, have been observed with a generous amount of sand in its deposit which can have an influence the shear vane test results.

The undrained shear strength is determined to match the average strength value, $c_u = 392$ kPa.

The effective cohesion, c' , is determined by the following expression: $c' = \frac{c_u}{10}$, whereas c' is limited to a maximum strength of 20 kPa. Hereby the effective cohesion, $c' = 20$ kPa.

The consolidation module is determined by the following expression that is based on the relation between the undrained shear strength, c_u , and the water content: $K = \frac{40}{w} \cdot c_u$. Hereby the consolidation module, $K = 115$ MPa.

5.1.1.8 Summary

Table 5-9 below summarizes the strength- and deformations parameters in the encountered soil types in borehole BH01-05. These parameters are determined on the basis of derived field-, and laboratory tests and on the basis of empirical knowledge and reference values.

Table 5-9: Summary of strength and deformation parameters of the encountered soil types in borehole BH01-05

Soil Type		γ/γ'	ϕ_k^1	c'	c_u	K
[-]	[Env., Age]	[kN/m ³]	[°]	[kPa]	[kPa]	[MPa]
FILL	Fi, Re	17/10	37	-	-	3-10
SAND	Mw, Lg	20/10	37	0	-	30
GRAVEL	Mw, Gc	21/10	37	0	-	40
SAND	Mw, Gc	20/10	39	0	-	40
GRAVEL TILL	GI, Gc	21/10	38	0	-	40
SAND TILL	GI, Gc	21/10	40	0	-	40
CLAY TILL	GI, Gc	21/10	30	20	392	115

¹⁾ In friction material the friction angle is plane, and I cohesive material the friction angle is triaxle

6. GEOPHYSICAL INVESTIGATIONS – MEP

The survey lines are called GIL-WEST and GIL-EAST are presented in Figure 6-1 below. Furthermore, details about the geophysical investigation and its survey lines are presented in Table 6-1.

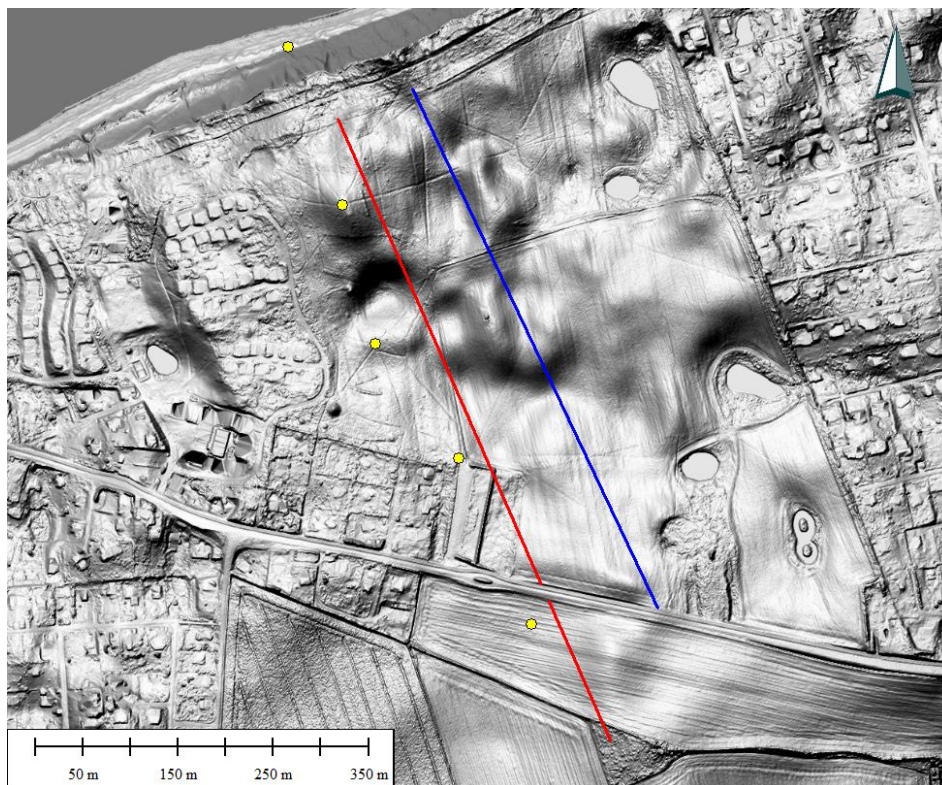


Figure 6-1. Overview of the survey site at Gilbjergghoved. Survey lines are presented in red (GIL-WEST) and blue (GIL-EAST). Boreholes are presented in yellow.

Table 6-1: Details of the geotechnical investigations and its survey lines

Survey Line	Colour	Surface Distance	Acquisition date	X	Y
[-]	[-]	[m]	[YYYYMMDD]	[UTM32 ETRS89]	[UTM32 ETRS89]
GIL-WEST_N	Red	530	2022-04-12	North 703228.478	North 6224903.984
				South 703440.338	South 6224419.421
GIL-WEST_S	Red	160	2022-04-12	North 703448.694	North 6224401.101
				South 703513.215	South 6224254.842

GIL-EAST	Blue	600	2022-04-11	North 703306.329	North 6224936.127
				South 703562.323	South 6224394.279

The MEP data has been processed in the software RES2DINV and Aarhus Workbench. The resistivity measurements have been cleaned for unusually low and high resistivities and afterwards inverted with topography included. The topography has been extracted from the Danish Digital Terrain Model (0,4 m grid) from SDFE. During the data processing both single- and multi-layered 1D interpretations are made as well as 2D interpretations.

The results from the geoelectrical mapping have been correlated with the boreholes extracted from GeoGIS to investigate the soil condition between the boreholes. In the technical drawings the boreholes are orthogonally placed on the profiles labeled with an offset distance.

The MEP profiles are shown in colours representing resistivities in ohm.m according to the logarithmic colour scale presented in Figure 6-2 below.

The MEP Profiles are presented in Figure 6-3 and Figure 6-4 and in Appendix 2.1 and Appendix 2.2 and are oriented north to south.

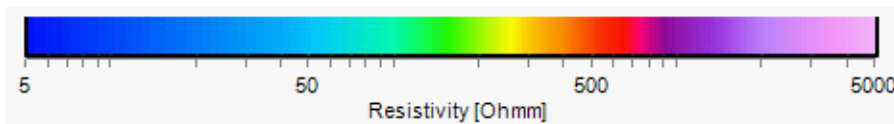


Figure 6-2. Logarithmic colour scale representing resistivities in ohm.m.

GIL-WEST

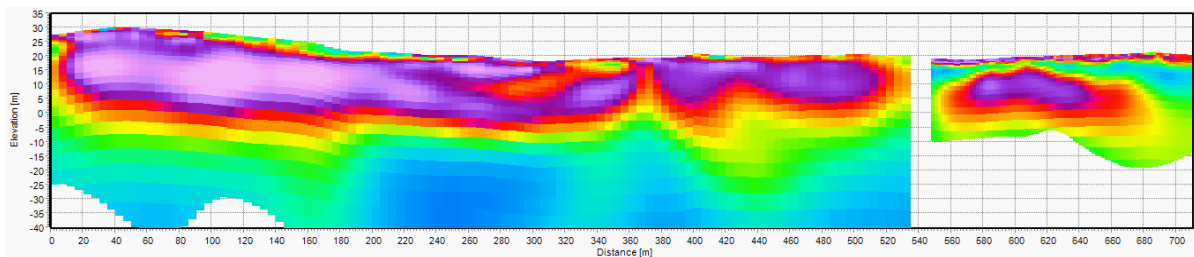


Figure 6-3. MEP profile GIL-WEST oriented north to south.

The profile is divided at the road crossing at 540 meters along the profile. The electrode spacing is 5 m north of the road and 2 m spacing south of the road. The difference is evident with a shallower penetration but with a higher resolution when 2 m spacing is used.

The sharp transition from high resistivities to low resistivities are related to the water table, thus it marks the boundary between unsaturated and saturated sediments. The very low resistivities (dark blue) will normally be associated with clays, however this cannot be confirmed from the boreholes. It would not be surprising to find clays at the deepest part of the profile (-40 m), however it has not been interpreted.

According to the LER-database the profile is crossing a cable at approximately 370 meters along the profile. Undulating resistivity data correlate with position of 3rd party power cable.

From the boreholes the geology is mainly composed of sand and gravel throughout the profile but with mixed-in clay particles in the southern part. The resistivities are correlating with the lab-interpreted geology, however a distinction between sand a gravel with or without mixed-in clay particles cannot be made from the resistivities.

North of Tinkerup Strandvej there are areas with clay till as seen in the low resistivities (greenish blue). This correlates with the boreholes. South of Tinkerup Strandvej the profile is situated in an agricultural field. The upper high resistivities are related to the agricultural soil. Below is a layer of clay till varying in thickness from approximately 1-10 m.

GIL-EAST

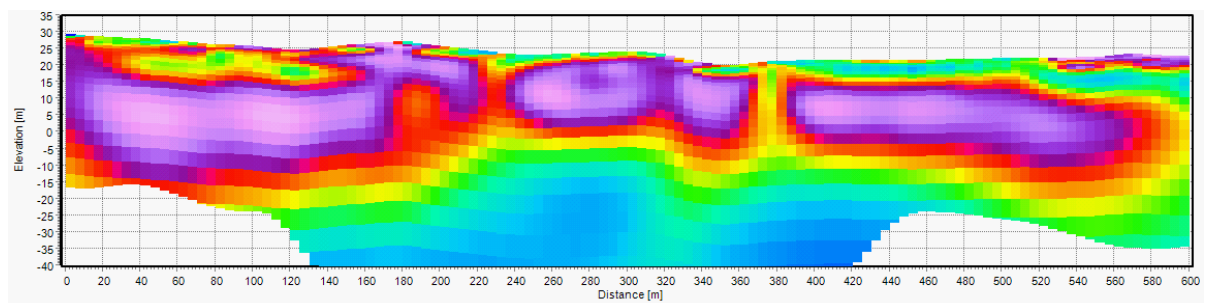


Figure 6-4. MEP profile GIL-EAST oriented north to south.

The profile is only acquired north of the road with an electrode spacing of 5 m.

The same sharp transition from high resistivities to low resistivities is present marking the boundary between unsaturated and saturated sediments. There are also very low resistivities in the deepest part of the profile normally associated with clays, however, as with the previous profile, it has not been interpreted as it could not be confirmed from the boreholes.

In the northern part of the profile there are areas of clay till as seen in the low resistivities (greenish blue). In the southern part of the profile a layer of clay till is interpreted with low resistivities and sharp boundaries to the unsaturated sediment below. In the southernmost part of the profile an unsaturated sediment is interpreted with high resistivities overlying the interpreted clay till.

The boreholes are further away and correlation becomes more uncertain with distance, however the resistivities correlate well with the lab-interpreted geology and there is a high correlation between the two profiles. It is however evident that the eastern profile has lower resistivities in the upper part which indicate a greater presence of clay till. This correlates well with the geological map (jordartskort 1:25000) from GEUS as presented in Figure 2-4. The brown colour is glacial clay till and the purple colour is glacial meltwater sand and gravel.

According to the LER-database the profile is crossing a cable at approximately 380 meters along the profile. Undulating resistivity data correlate with position of 3rd party power cable.

7. RISK ASSESMENT

The scope of this section is to establish a risk profile for the horizontal directional drillings. The purpose is to identify risks towards the contractor’s successful completion of the project on time. Focus is on soil related risks.

Risks have been identified and evaluated in advance by geotechnical engineers as well as geologists and discussed and clarified in a workshop with Energinet. Although all efforts have been made to identify all relevant risk and evaluate them, no guarantees are given that all risk scenarios are covered and that risks are correctly assessed.

Risks are evaluated on the impact they will have on the project objective - time. The probability of occurrence is evaluated on a six-point scale ranging from Theoretical (<1%) to Often (>50%). Consequence on time is also evaluated on a six-point scale calibrated to a project with a relatively short duration, see Figure 7-1.

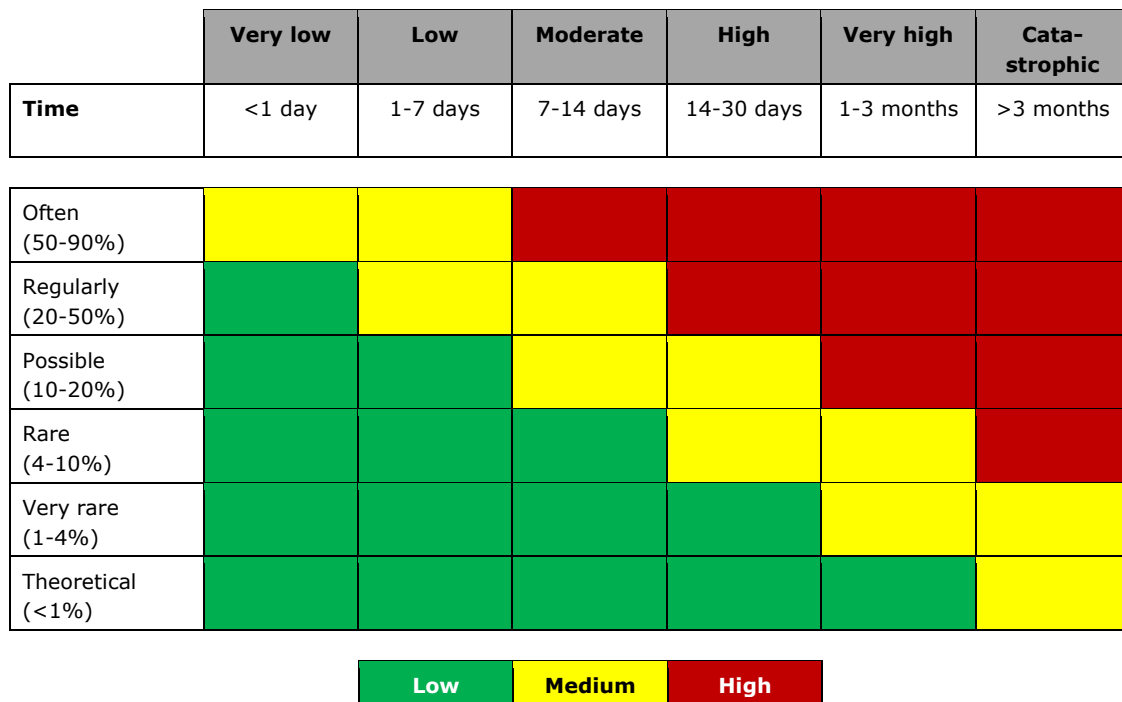


Figure 7-1. Risk matrices for evaluating impact on project time.

In Figure 7-2, the results are plotted in the risk matrix above.

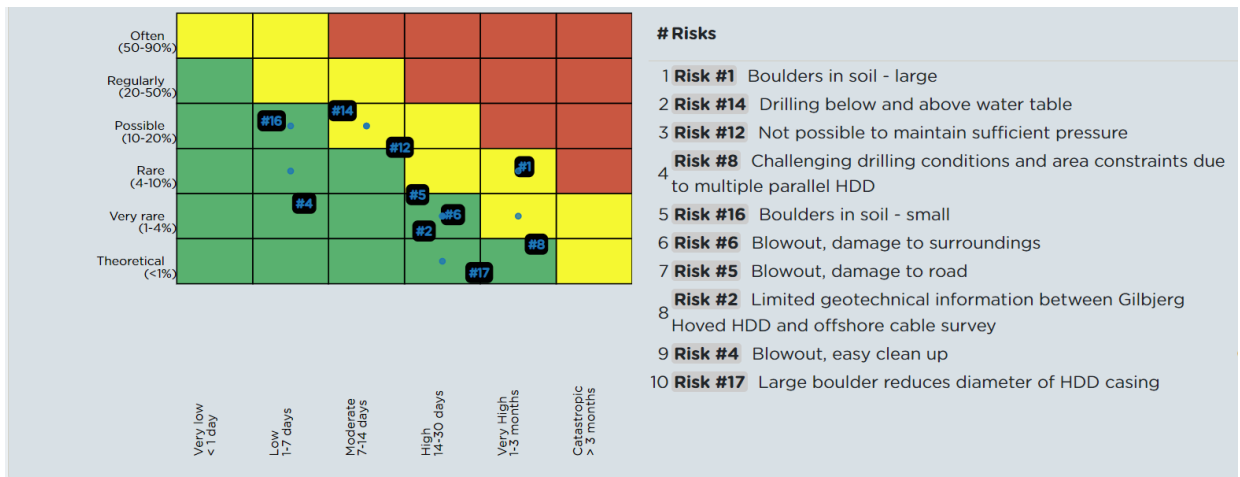






Figure 7-2. Risks plotted in risk matrix.

Below is an overview of the identified risks and the risk level. The risks are ranked with the highest risk first.

In Appendix 7.1 the risks, the effects and possible mitigation measures are described in more details.

No.	Description	Risk level
1	Boulders in soil - large	
12	Not possible to maintain sufficient pressure	
14	Drilling below and above water table	
8	Challenging drilling conditions and area constraints due to multiple parallel HDD	
16	Boulders in soil - small	
2	Limited geotechnical information between Gilbjerg Hoved HDD and offshore cable survey	
5	Blowout, damage to road	
6	Blowout, damage to surroundings	
4	Blowout, easy clean up	




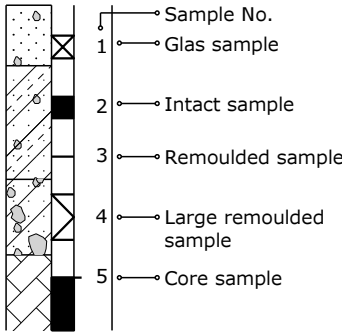
























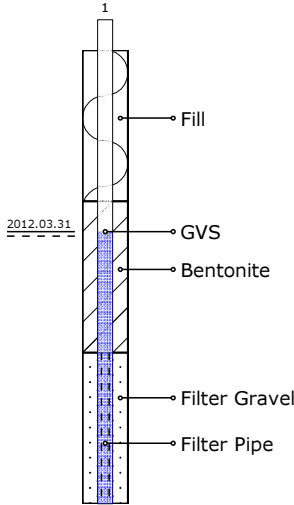
17	Large boulder reduces diameter of HDD casing	
11	Risk of friction during drilling	
15	Crossing of high voltage cable.	
10	Interference with roots	

8. REFERENCES

- [1] Danish Geotechnical Society Bulletin 1, revision 2, A guide to engineering geological description. 2021.
- [2] DS/EN 1997-1 DK NA:2021, Eurocode 7: Geotechnical design, Part 1.
- [3] Fundering, Dansk Standard, DS415, 3. Edition. 1984.
- [4] Geologi og Landskaber i Nationalpark Kongernes Nordsjælland, M. Houmark-Nielsen. 2019.
- [5] DS/EN 1997-2 DK NA:2013, Eurocode 7: Geotechnical design, Part 2.

APPENDIX 1.1 – LEGEND AND DEFINITIONS

Test Results

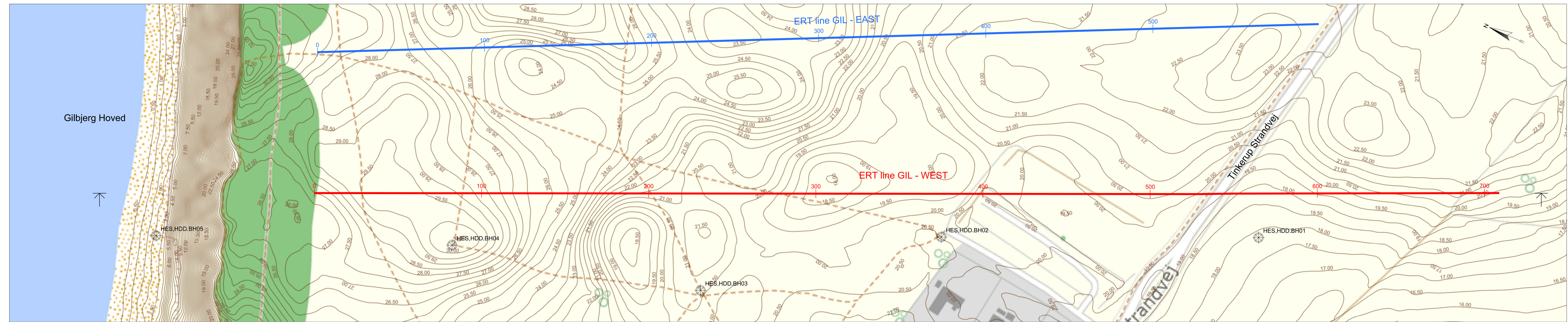
Geology		Plan	Borehole Log																																																														
 FILL	 SAND TILL	 LB 10																																																															
 MULL	 SILT TILL	 Pumping well																																																															
 MULL, sandy	 CLAY TILL	 Monitoring well																																																															
 SAND, org. content	 LIMESTONE (CHALK)	 Simple borehole																																																															
 SAND, lumps of organic material	 ROCK	 Borehole with sampling																																																															
 STONE	 GYTTJA	 Geotech. borehole incl. insitu tests																																																															
 GRAVEL	 SHELLS	 Penetration tests																																																															
 SAND	 PEAT																																																																
 SILT	 PEATY MUD																																																																
 CLAY	 PLANT REMNANTS																																																																
		Geological Abbreviations	Stand Pipe																																																														
		<table border="0"> <thead> <tr> <th>Environment</th> <th>Age</th> </tr> </thead> <tbody> <tr><td>Br</td><td>Brackish Water</td><td>Pg</td><td>Post Glacial</td></tr> <tr><td>Fw</td><td>Freshwater</td><td>Lg</td><td>Late Glacial</td></tr> <tr><td>Ss</td><td>Solifluction Soil</td><td>Al</td><td>Allerød</td></tr> <tr><td>Gl</td><td>Gletscher</td><td>Gc</td><td>Glacial</td></tr> <tr><td>Ma</td><td>Marine</td><td>Ig</td><td>Interglacial</td></tr> <tr><td>Wd</td><td>Wash Down</td><td>Is</td><td>Interstadial</td></tr> <tr><td>Ts</td><td>Top Soil</td><td>Pl</td><td>Pliocene</td></tr> <tr><td>Ls</td><td>Land Slide</td><td>Mi</td><td>Miocene</td></tr> <tr><td>Mw</td><td>Meltwater</td><td>Oi</td><td>Oligocene</td></tr> <tr><td>Ae</td><td>Aeolian</td><td>Eo</td><td>Eocene</td></tr> <tr><td>Vu</td><td>Vulcanic</td><td>Pl</td><td>Palæocene</td></tr> <tr><td></td><td></td><td>Se</td><td>Selandien</td></tr> <tr><td></td><td></td><td>Da</td><td>Danien</td></tr> <tr><td></td><td></td><td>Ct</td><td>Cretaceous</td></tr> <tr><td></td><td></td><td>Se</td><td>Senon</td></tr> </tbody> </table>	Environment	Age	Br	Brackish Water	Pg	Post Glacial	Fw	Freshwater	Lg	Late Glacial	Ss	Solifluction Soil	Al	Allerød	Gl	Gletscher	Gc	Glacial	Ma	Marine	Ig	Interglacial	Wd	Wash Down	Is	Interstadial	Ts	Top Soil	Pl	Pliocene	Ls	Land Slide	Mi	Miocene	Mw	Meltwater	Oi	Oligocene	Ae	Aeolian	Eo	Eocene	Vu	Vulcanic	Pl	Palæocene			Se	Selandien			Da	Danien			Ct	Cretaceous			Se	Senon	
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Definitions

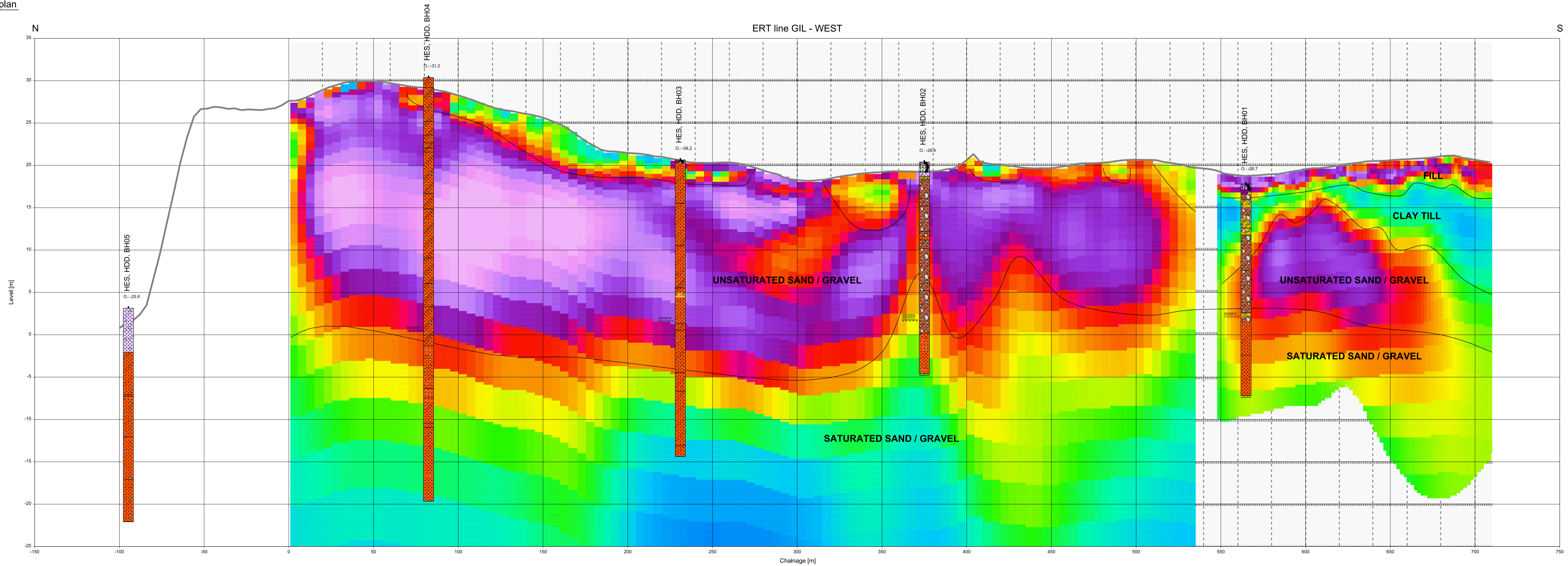
Legend	Topic	Abbr.	Unit	Definition
○	Moisture Content	W	%	Water as % of dry weight
—	Liquid limit	WL	%	Water content at liquid limit
—	Plasticity limit	WP	%	Water content at plastic limit
— —	Plasticity index	IP	%	WL - WP
▽	Bulk Weight	g	kN/m ³	Total weight of total volume
×	Loss of Ignition	gl	%	Loss of ignition as % of dry weight
×	Loss of Ignition, reduced	glr	%	gl - ka
⊕	Carbonate content	ka	%	Weight of CaCo ₃ as % of dry weight
-/(+)/+//+	Chalk Sample	kp	-	HCl Reaction: - not calcareous, (+) slightly calcareous, + calcareous, ++ very calcareous
++/+/(+)	Frost			++ Freezing hazard under all conditions + Freezing problems, even during short periods of frost (+) Freezing problems, during long periods of frost - No Freezing problems -- Absolutely no freezing hazard ? Freezing hazard cannot be evaluated -?/+? Freezing hazard is difficult to evaluate
●	Vane shear strength, intact	cvf	kN/m ²	Undrained shear strength - Vane test in intact soil
○	Vane shear strength, remoulded	cvr	kN/m ²	Undrained shear strength - Vane test in remoulded soil
	Penetration Test:			
	- Weight Sounding Test	WST	N200	Number of half rotations per. 200 mm penetration
	- Light Sounding Test	LST	N200	Number of blows per 200 mm penetration
	- Light Dynamic Penetrometer	LDP	N200	Number of blows per 200 mm penetration
	- SPT, closed/open	SPT	N300	Number of blows per 300 mm penetration

APPENDIX 2.1 – LOCATION MAP

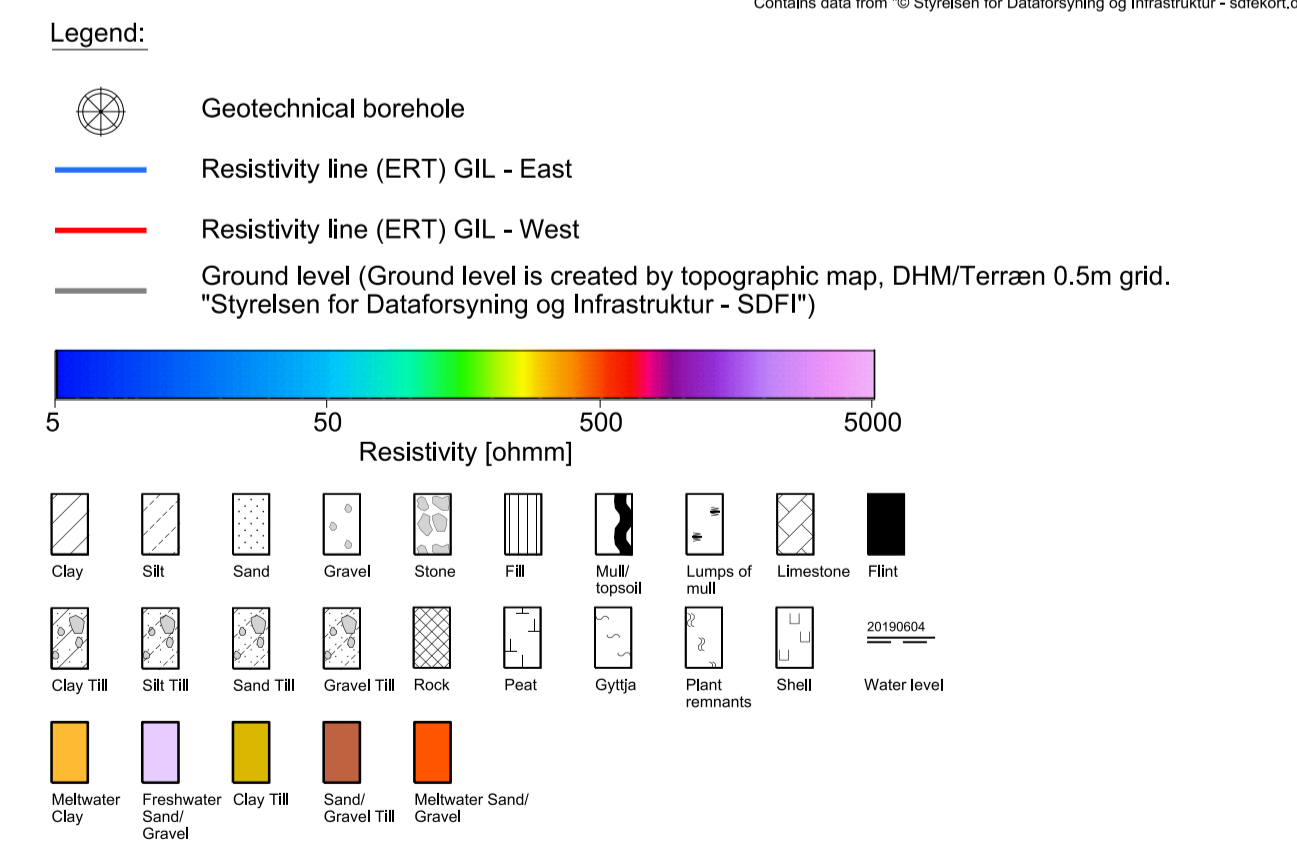
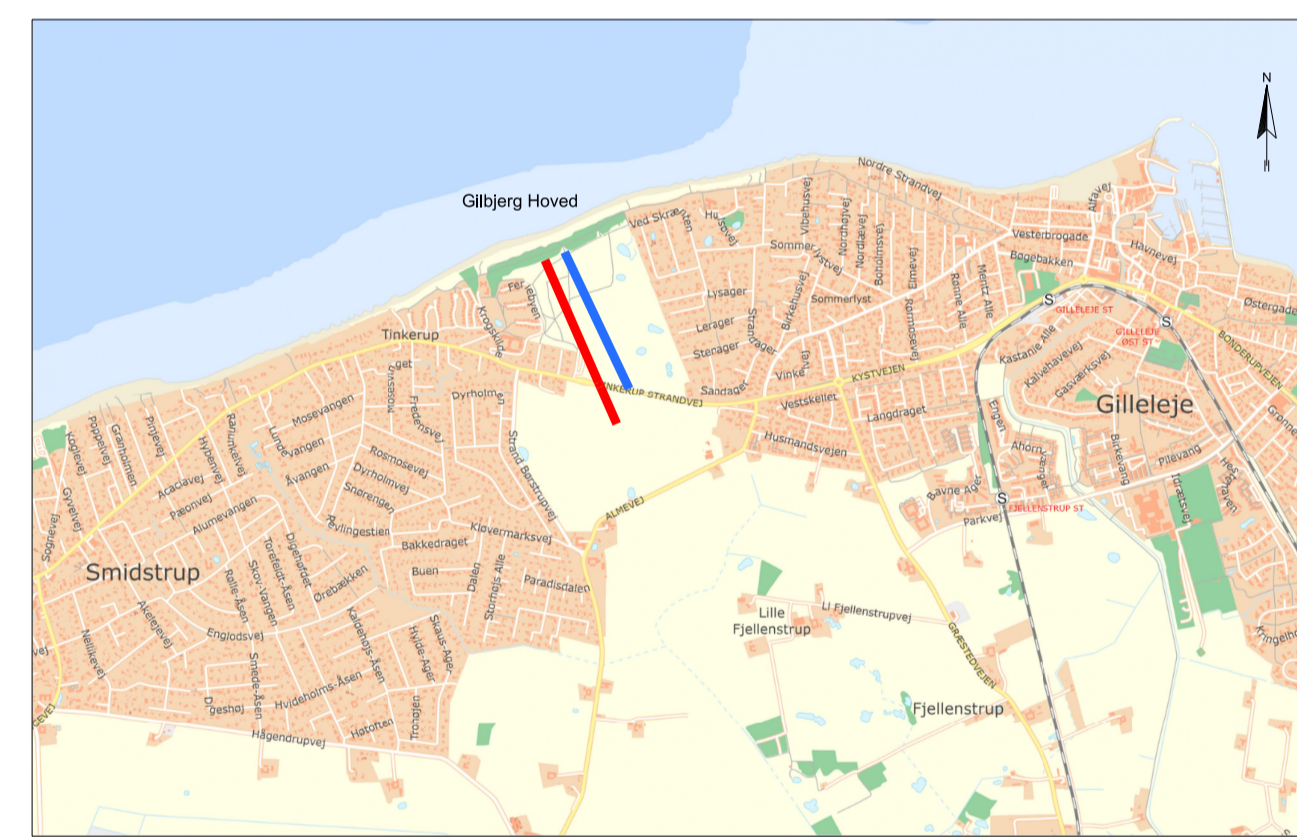
APPENDIX 3.1-3.4 – GEOTECHNICAL AND GEOPHYSICAL LONGITUDINAL PROFILES



Site plan
Scale: 1:1000



Longitudinal profile
Scale: 1:1000



Coordinate system: ETRS89 UTM32N, Elevation DVR90
Format: 594x1260

Rev.	Date	Signature	Checked	Approved
	2022-06-17	JMN	CRTA	RMH

Project no. 1100051481 Scale: 1:1000; 1:200

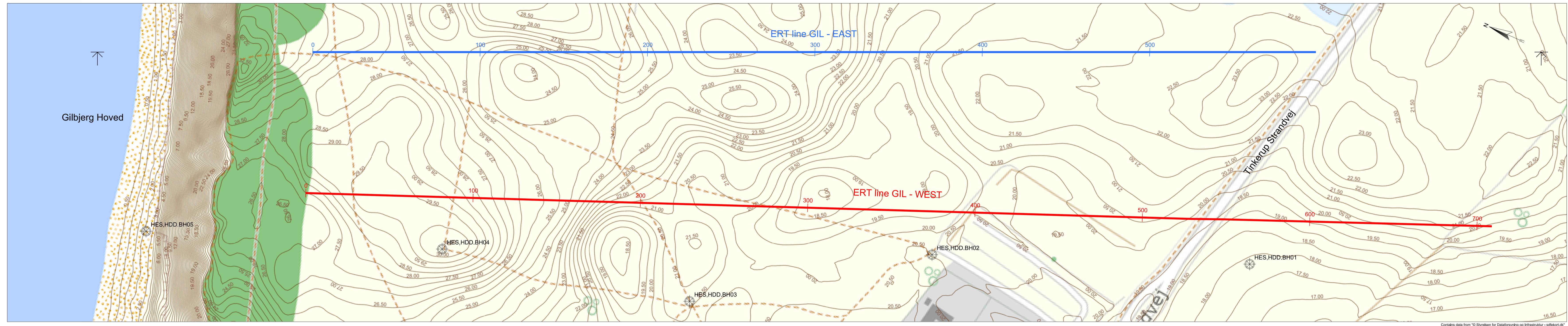
HESSELØFFSHORE WINDFARM
Onshore DK. HDD site investigations

Gilbjerg Hoved. HDD GIL - West. Resistivity (ERT)
Geotechnical and geophysical longitudinal profile

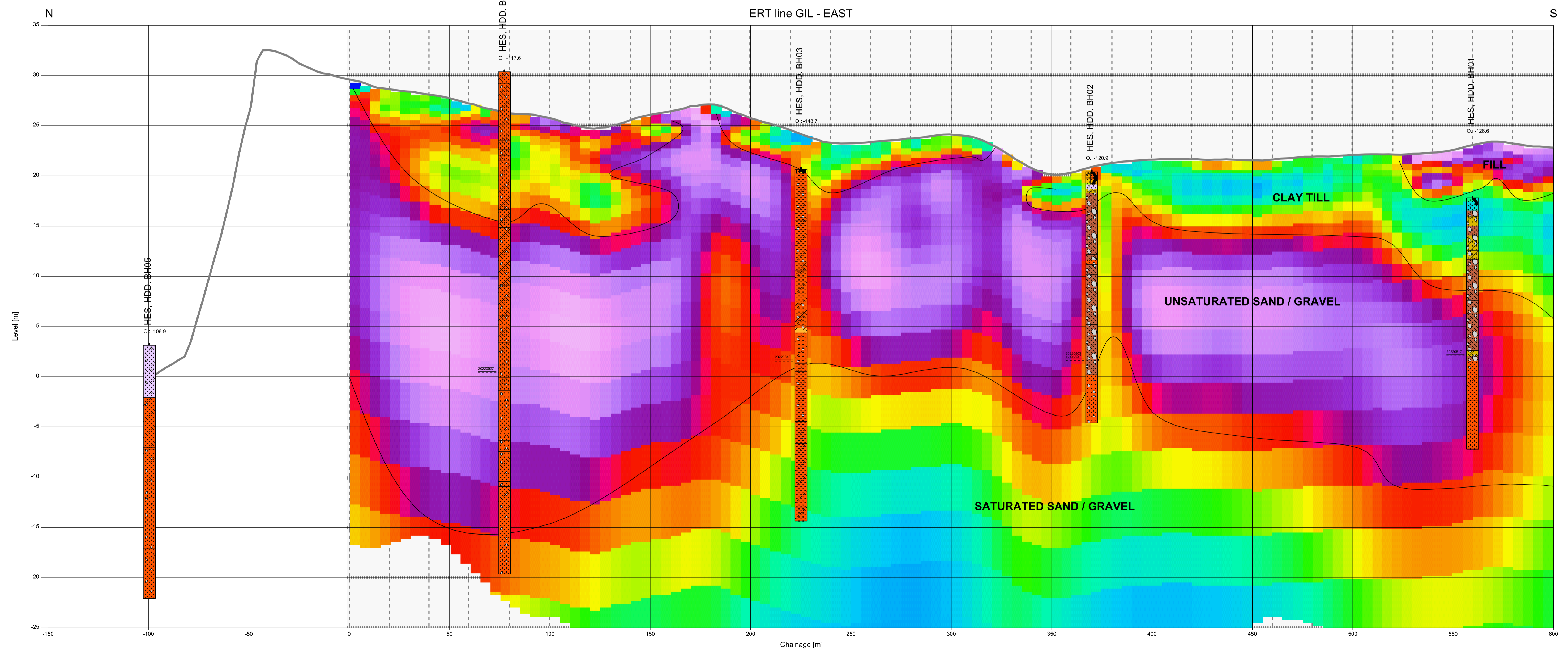
RAMBOLL
Hørmannsgade 53
DK-2300 København S
Tlf. +45 5161 1000
Fax +45 5161 1001
www.ramboll.com

ENERGINET
www.energinet.dk

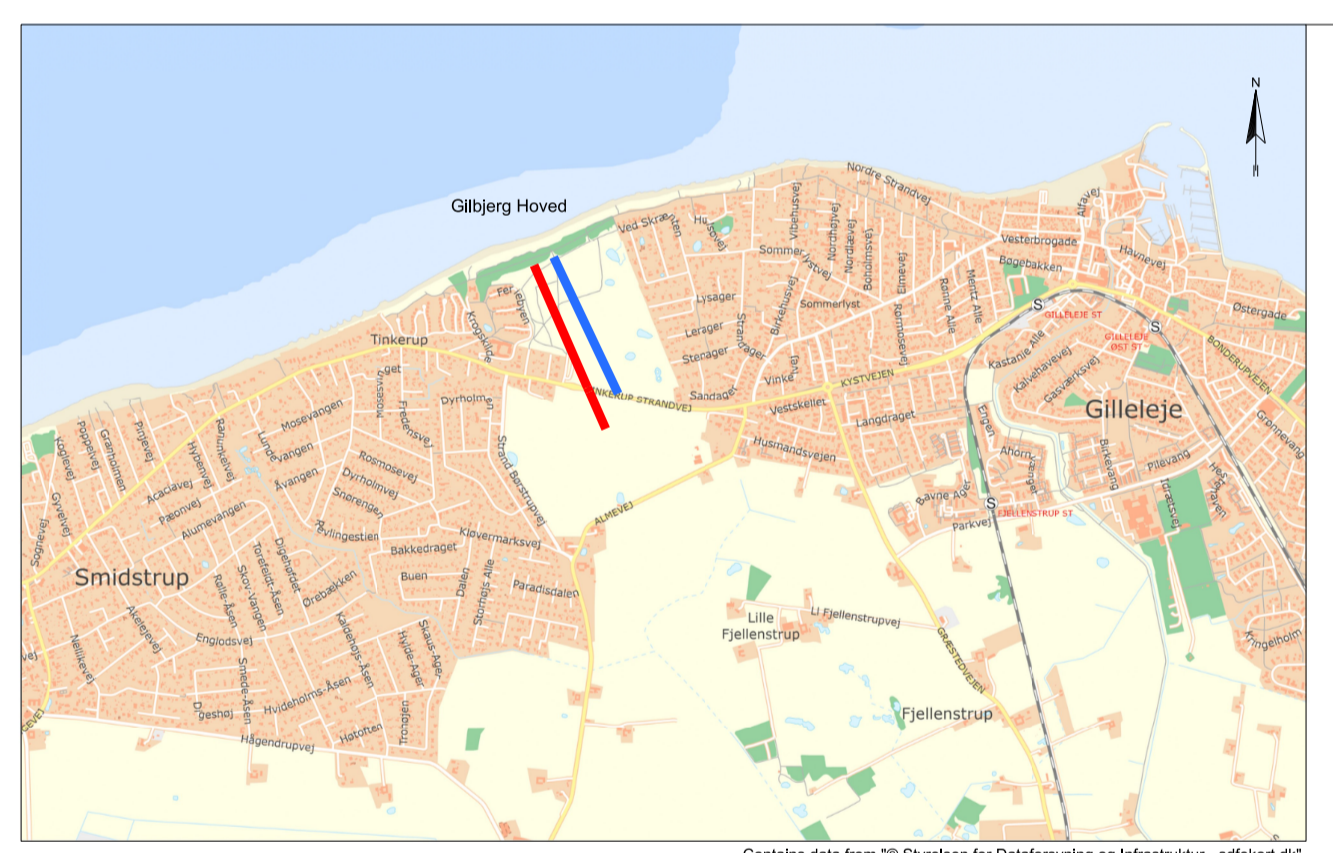
Drawing no. Rev.
2.1 1



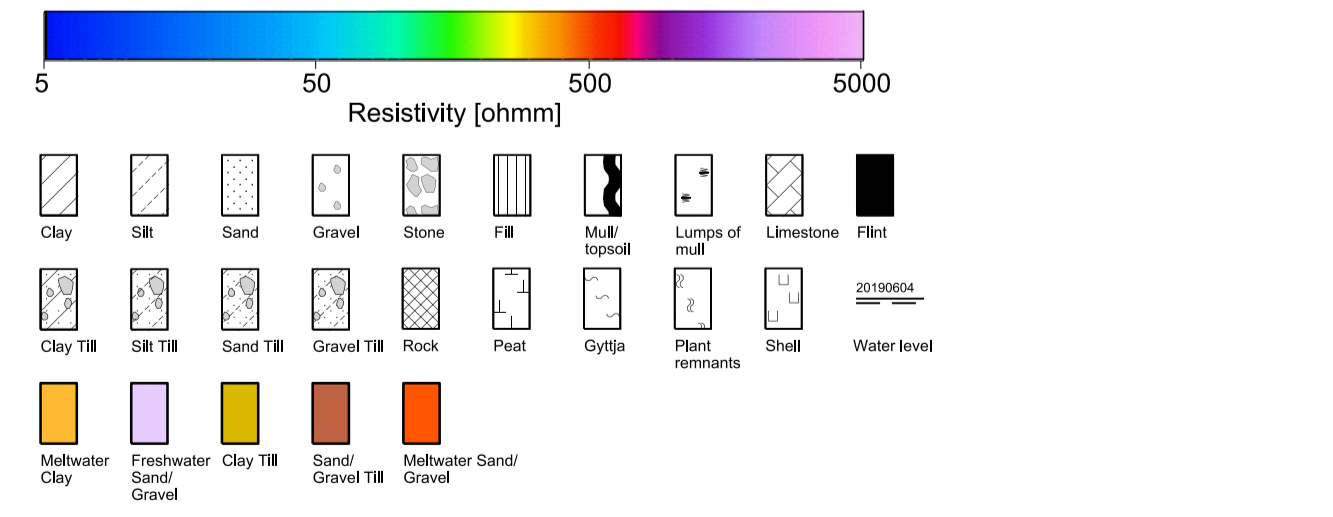
Site plan
Scale: 1:1000



Longitudinal profile
Title scale: 1:200
Venn scale: 1:200



- Legend:
- Geotechnical borehole
 - Resistivity line (ERT) GIL - East
 - Resistivity line (ERT) GIL - West
 - Ground level (Ground level is created by topographic map, DHM/Terræn 0.5m grid. *Styrelsen for Dataforsyning og Infrastruktur - SDFI*)



Coordinate system: ETRS89 UTM32N, Elevation DVR90
Format: 594x1260

Rev.	Date	Signature	Checked	Approved
	2022-06-17	JMN	CRTA	RMH

Project no. 1100051481 Scale: 1:1000; 1:200

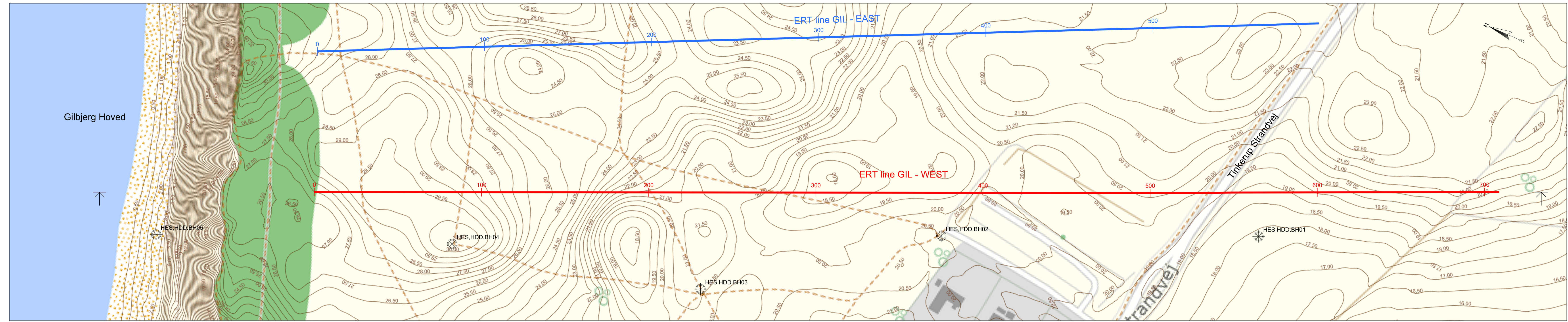
HESSELØ OFFSHORE WINDFARM
Onshore DK. HDD site investigations

Gilbjerg Hoved. HDD GIL - East. Resistivity (ERT)
Geotechnical and geophysical longitudinal profile

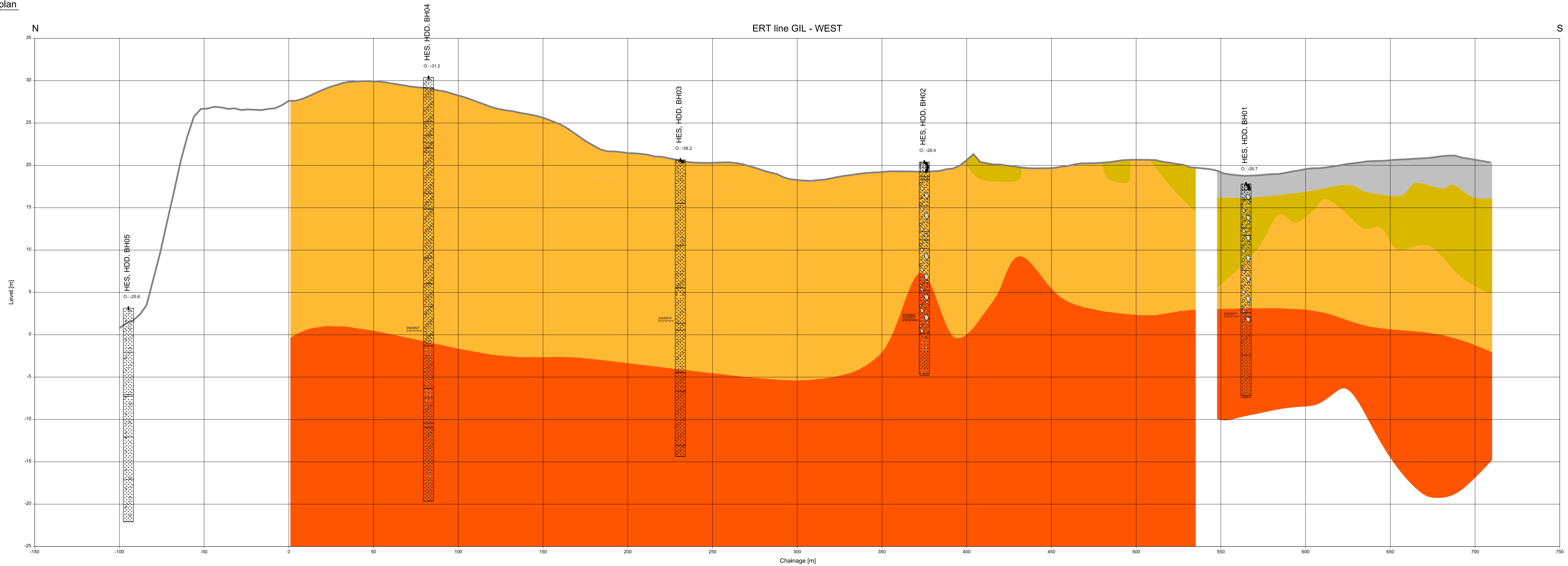
RAMBOLL
Hannemanns Allé 53
DK-2300 København S
Tlf. +45 5161 1000
Fax +45 5161 1001
www.ramboll.com

ENERGINET
www.energinet.dk

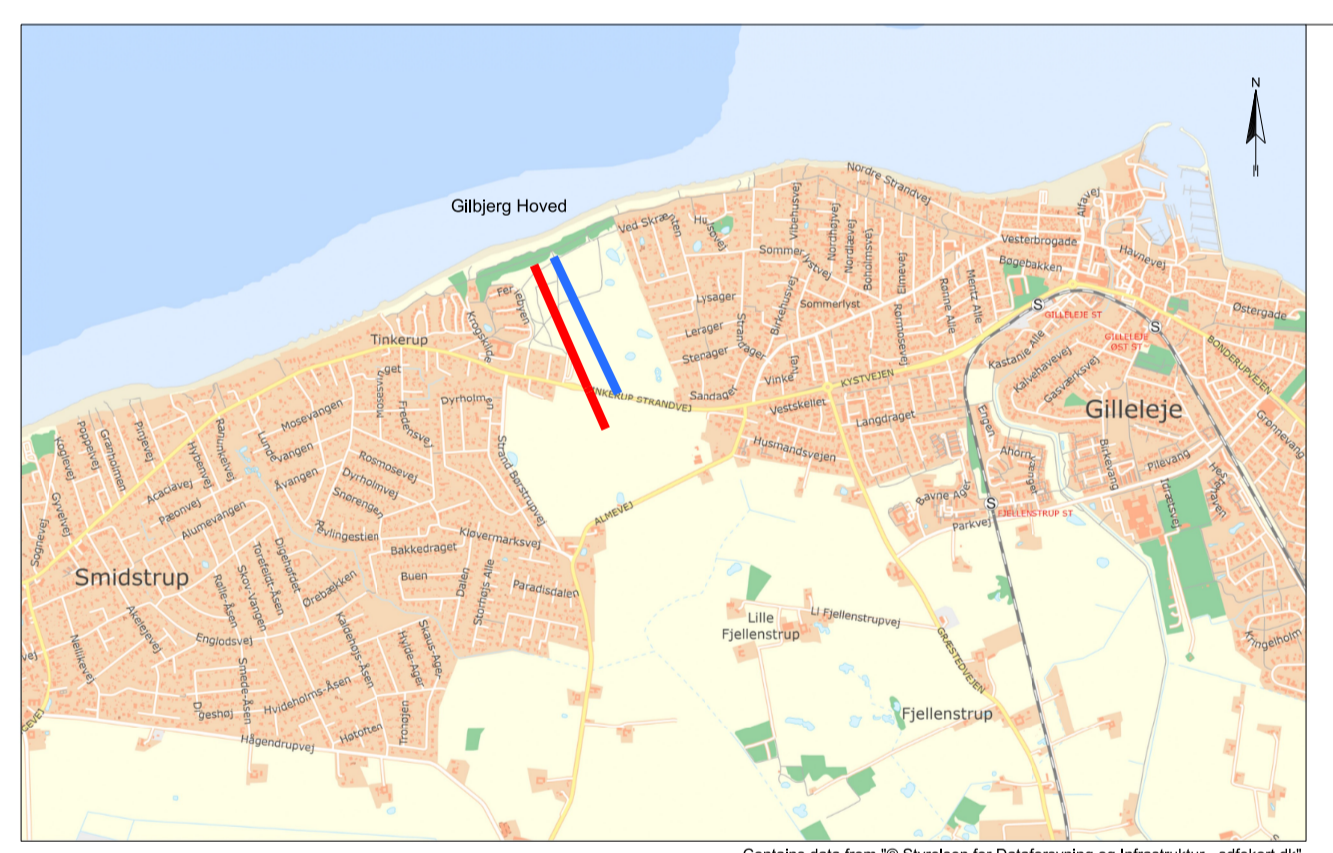
Drawing no. Rev. 2.2 1



Site plan
Scale: 1:1000



Longitudinal profile
Title scale: 1:200
Plan scale: 1:200



- Legend:
- Geotechnical borehole
 - Resistivity line (ERT) GIL - East
 - Resistivity line (ERT) GIL - West
 - Ground level (Ground level is created by topographic map, DHM/Terræn 0.5m grid, "Statens for Dataforsyning og Infrastruktur - SDFI")

- | | | | | |
|--|--|--|--|--|
| | | | | |
| | | | | |
| | | | | |

Coordinate system: ETRS89 UTM32N, Elevation DVR90
Format: 594x1260

Rev.	Date	Signature	Checked	Approved
	2022-07-06	JMN	MSHE	RMH

Project no. 1100051481 Scale: 1:1000; 1:200

HESSELØ OFFSHORE WINDFARM
Onshore DK. HDD site investigations

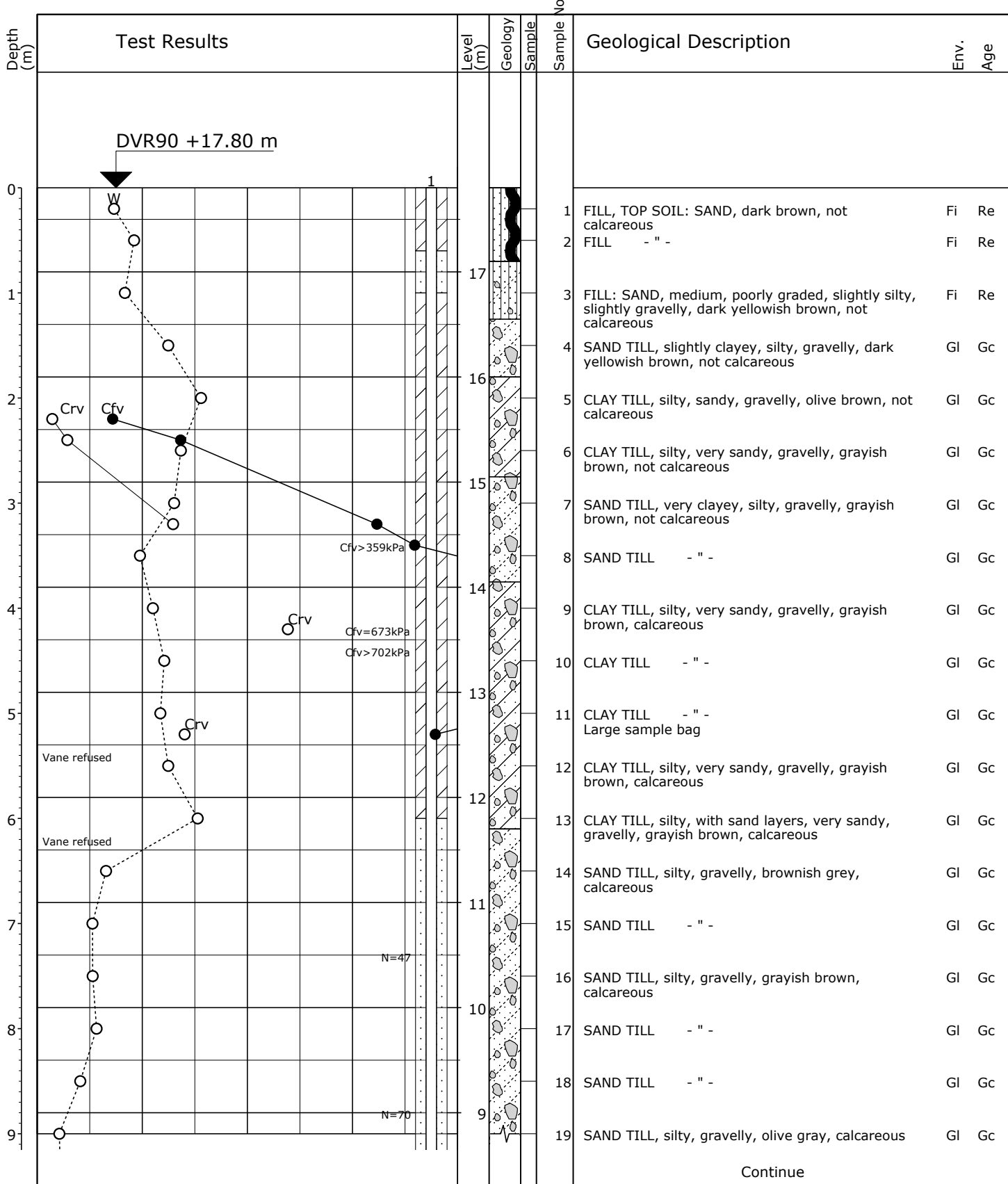
Gilbjerg Hoved. HDD GIL - West.
Geotechnical and geophysical longitudinal profile

RAMBOLL
Hørmannsgade 53
DK-2300 København S
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Drawing no. Rev. 3.1 0

APPENDIX 4.1-4.5 – BOREHOLE LOGS



Continue

○	10	20	30	W (%)
●	100	200	300	Crv, Cfv (kPa)
▼	10	20	30	N (Blows/30 cm)

Glacial deposits may contain cobbles and boulders

Stand Pipe: 1: ø25 - Top Level: 17.80 m

Method: Cased Shell & Auger 6'
 Projection: UTM32E89
 X: 703431 (m) Y: 6224376 (m) Plan: 2.101

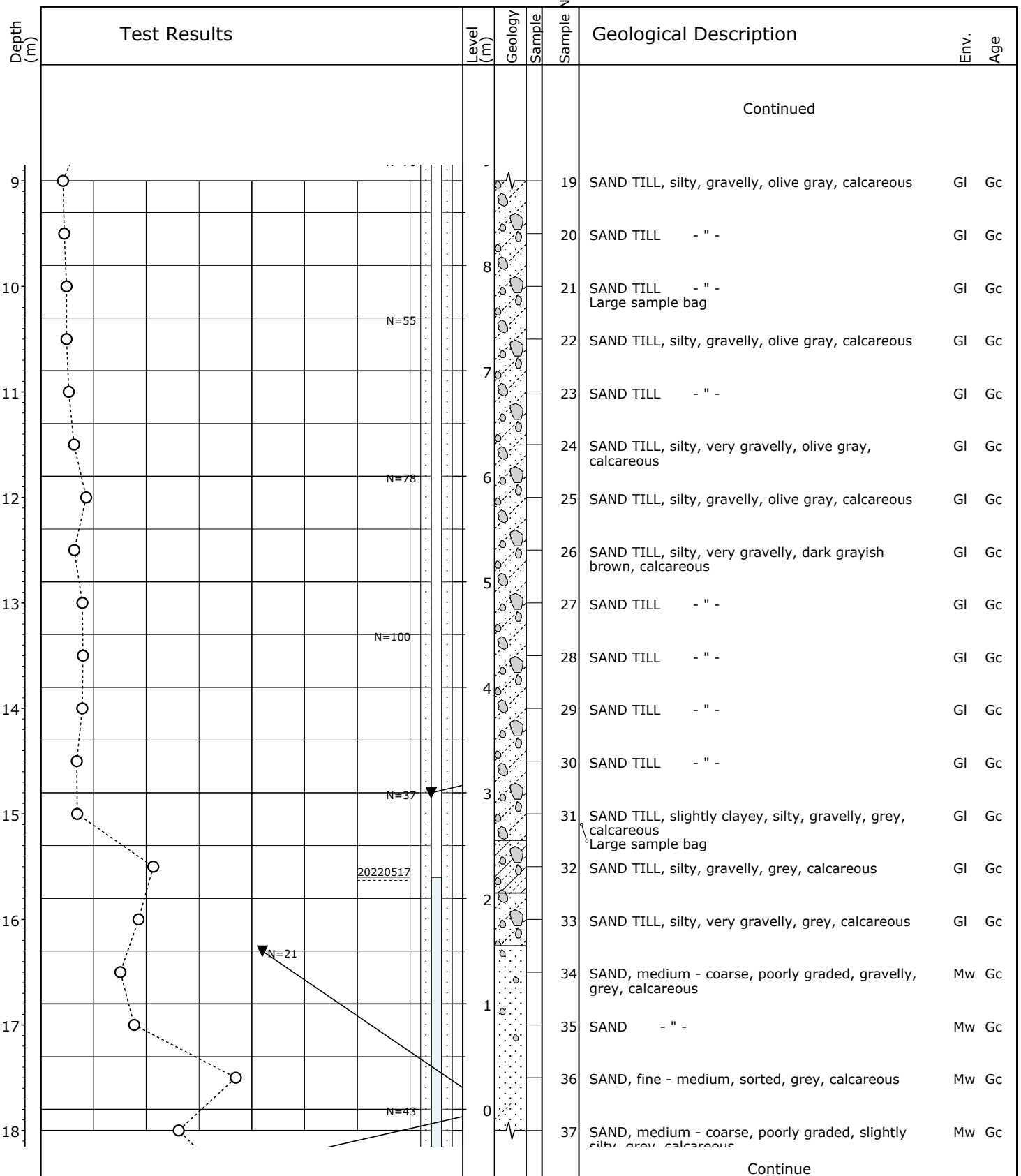
Project: 1100051481 Gilbjerg Hoved, HDD

Drilled by: PAA RJ/PB Date: 2022.05.17 Geologist: LSCH Public No.: Borehole: HDD. BH01

Prepared by: LSCH Checked by: RMH Approved by: RMH Date: 2022.06.10 Encl. No.: P. 1/3



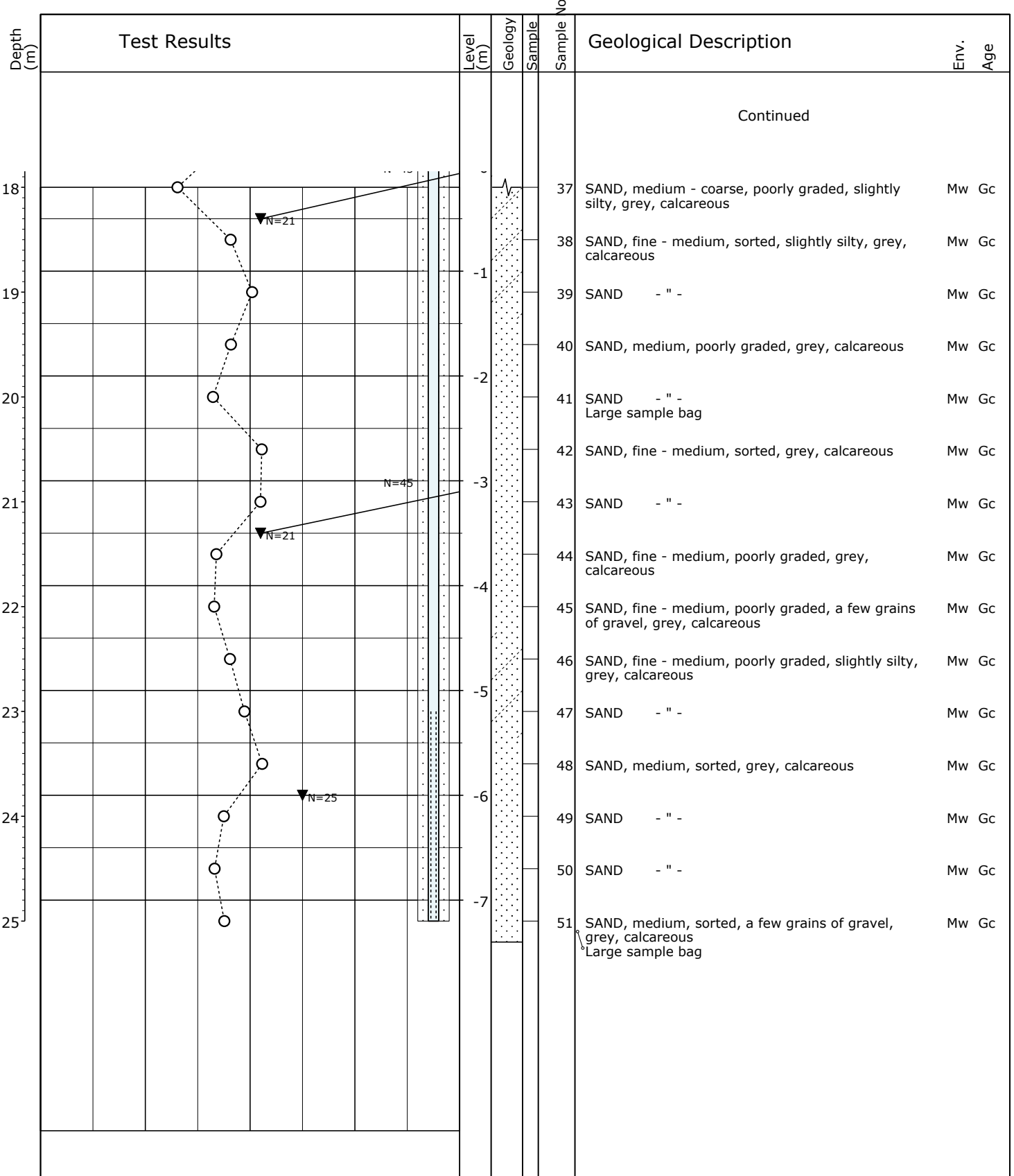
Borehole Log



○	10	20	30	W (%)	Glacial deposits may contain cobbles and boulders
●	100	200	300	Crv, Cfv (kPa)	
▼	10	20	30	N (Blows/30 cm)	
Method: Cased Shell & Auger 6'					Stand Pipe: 1: ø25 - Top Level: 17.80 m
Projection: UTM32E89					
X: 703431 (m) Y: 6224376 (m) Plan: 2.101					

Project: 1100051481 Gilbjerg Hoved, HDD
 Drilled by: PAA RJ/PB Date: 2022.05.17 Geologist: LSCH Public No.: Borehole: HDD. BH01
 Prepared by: LSCH Checked by: RMH Approved by: RMH Date: 2022.06.10 Encl. No.: P. 2/3

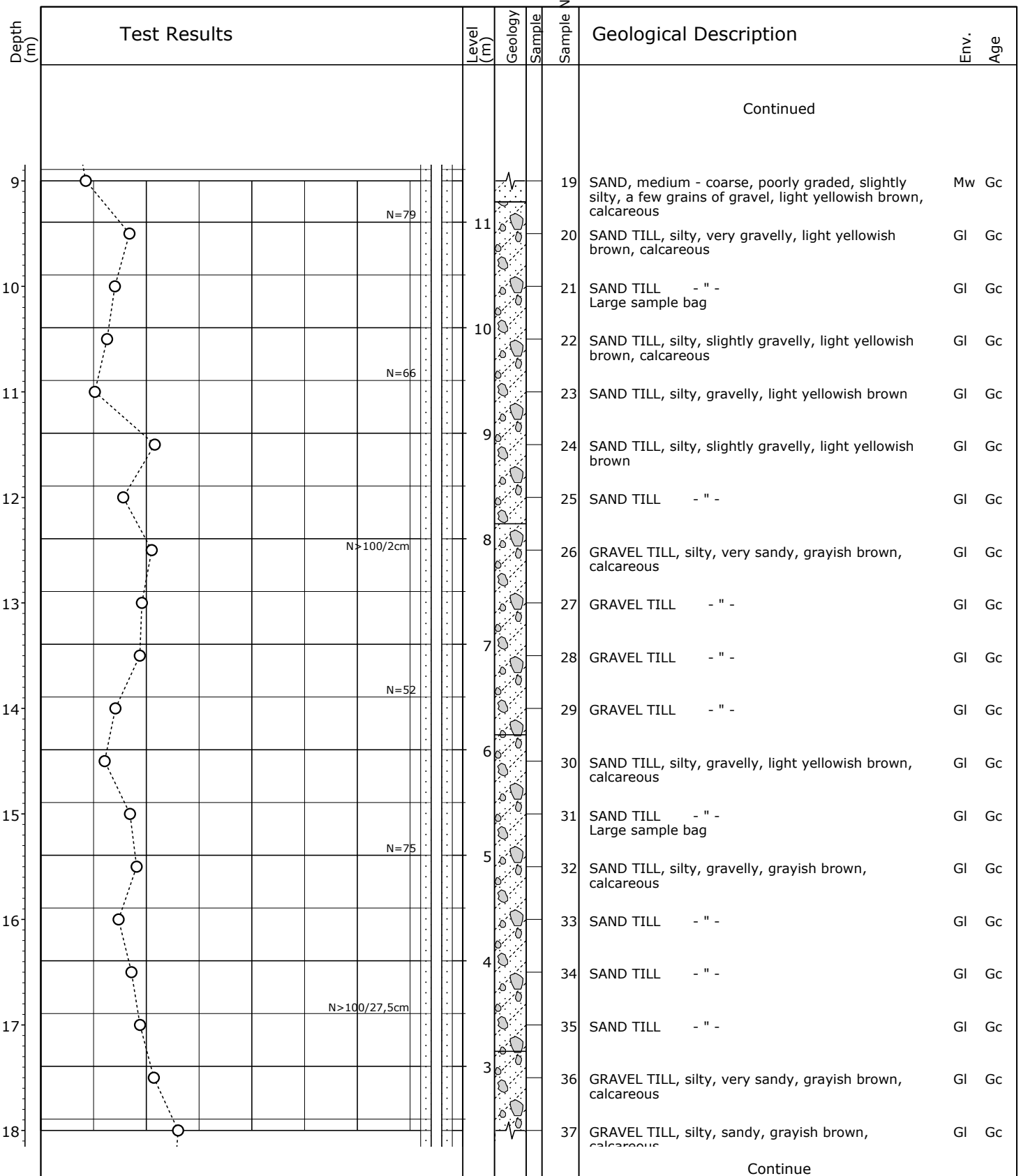
GeoGIS2020 20.03.81 PSTGUK 04-07-2022 12:28:36



○	10	20	30	W (%)	Glacial deposits may contain cobbles and boulders
○●	100	200	300	Crv, Cfv (kPa)	
▼	10	20	30	N (Blows/30 cm)	
					Stand Pipe: 1: ø25 - Top Level: 17.80 m
					Method: Cased Shell & Auger 6'
					Projection: UTM32E89
					X: 703431 (m) Y: 6224376 (m) Plan: 2.101

Project: 1100051481 Gilbjerg Hoved, HDD
 Drilled by: PAA RJ/PB Date: 2022.05.17 Geologist: LSCH Public No.: Borehole: HDD. BH01
 Prepared by: LSCH Checked by: RMH Approved by: RMH Date: 2022.06.10 Encl. No.: P. 3/3

GeoGIS2020 20.03.81 PSTGUK 04-07-2022 12:28:36



○	10	20	30	W (%)
○●	100	200	300	Crv, Cfv (kPa)
▼	10	20	30	N (Blows/30 cm)

Glacial deposits may contain cobbles and boulders
Excavated by hand to 1, 5 m b.g.
Stand Pipe: 1: ø25 - Top Level: 20.39 m

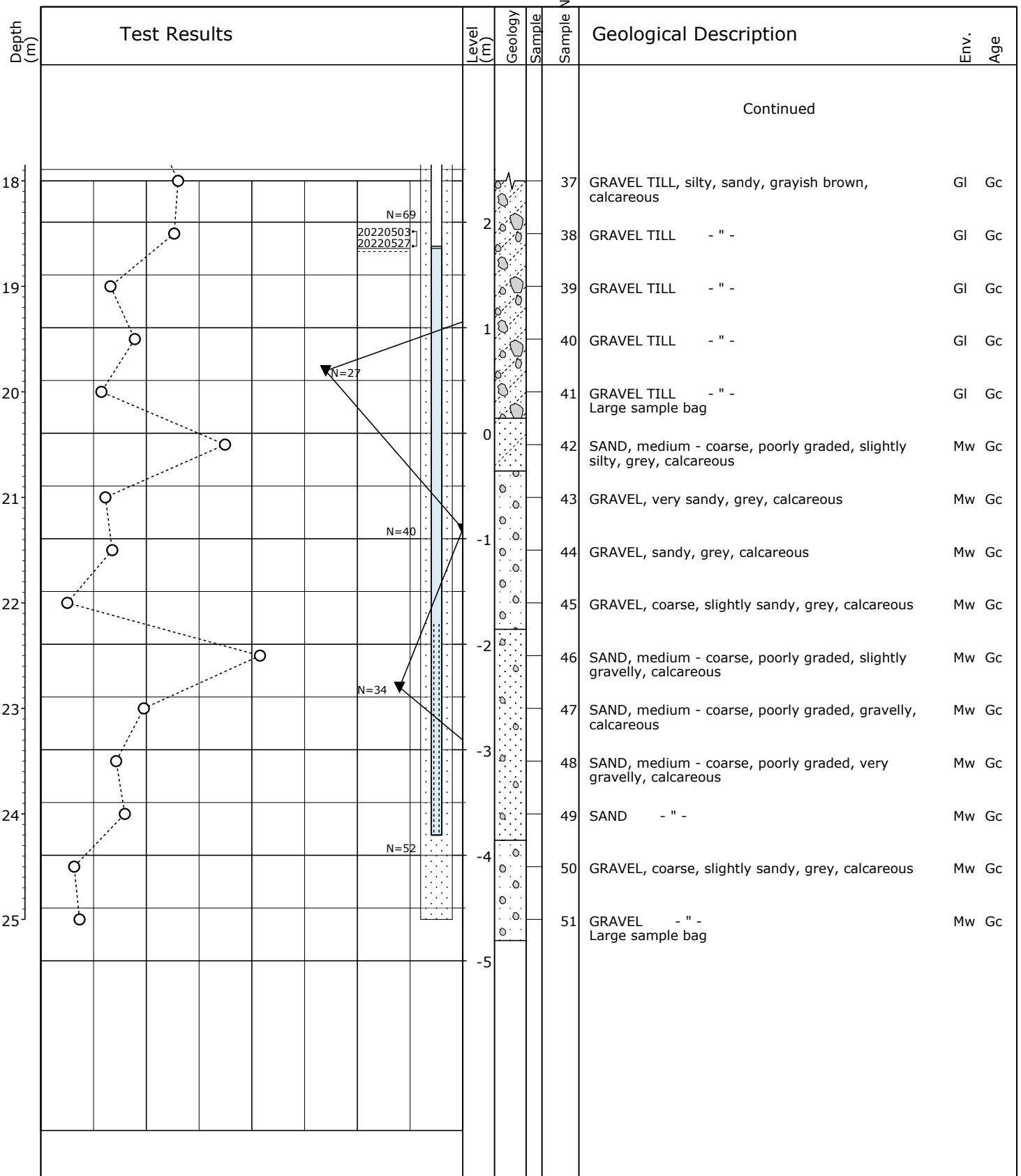
Method: Cased Shell & Auger 6'
Projection: UTM32E89
X: 703355 (m) Y: 6224550 (m) Plan: 2.101

Project: 1100051481 Gilbjerg Hoved, HDD

Drilled by: PAA VLJ/PB Date: 2022.05.03 Geologist: LSCH Public No.: Borehole: HDD. BH02

Prepared by: LSCH Checked by: RMH Approved by: RMH Date: 2022.06.10 Encl. No.: P. 2/3

GeoGIS2020 20.03.81 PSTGUK 04-07-2022 12:29:22



○	10	20	30	W (%)
●	100	200	300	Crv, Cfv (kPa)
▼	10	20	30	N (Blows/30 cm)

Glacial deposits may contain cobbles and boulders
 Excavated by hand to 1, 5 m b.g.
 Stand Pipe: 1: ø25 - Top Level: 20.39 m

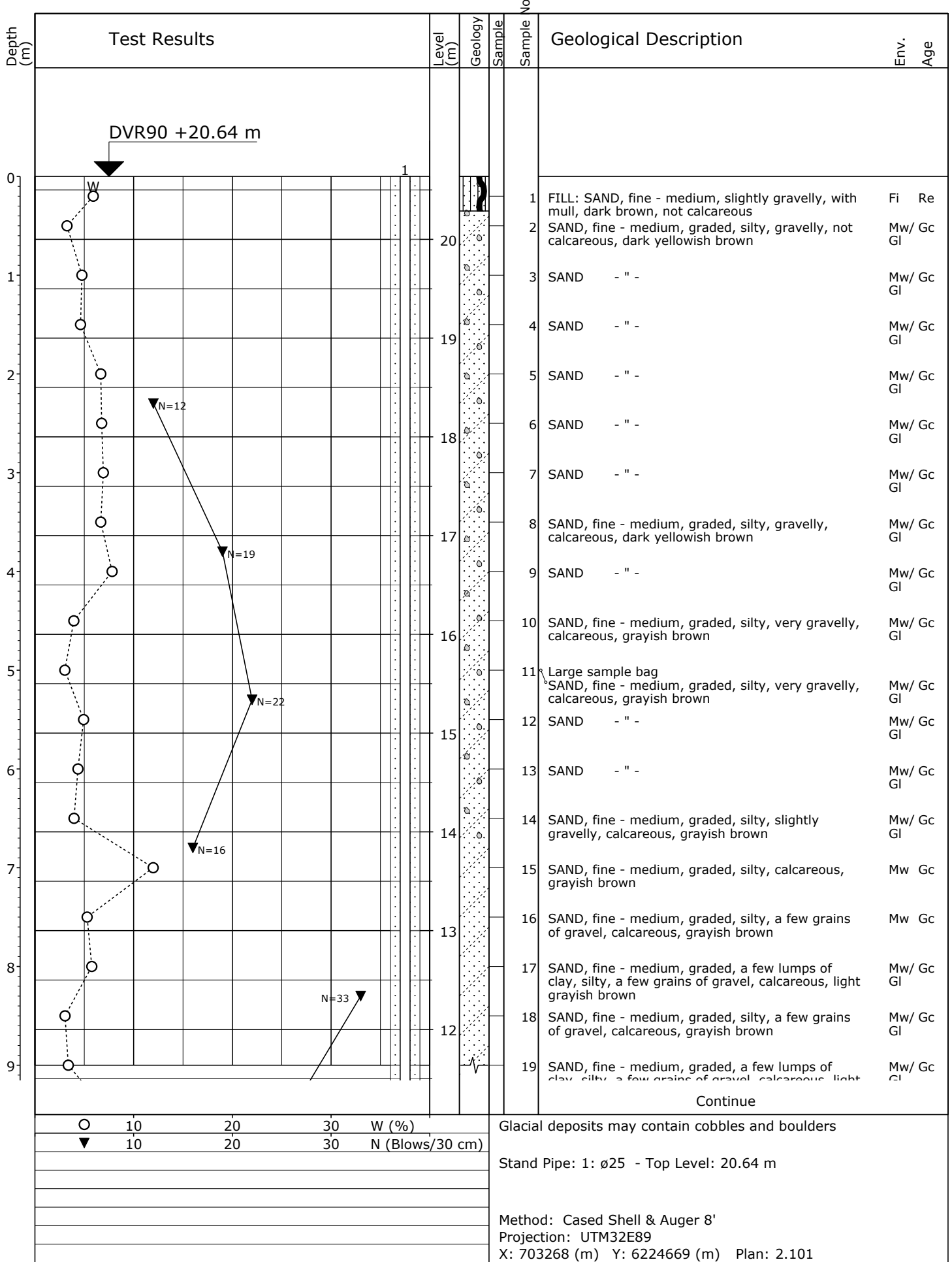
Method: Cased Shell & Auger 6'
 Projection: UTM32E89
 X: 703355 (m) Y: 6224550 (m) Plan: 2.101

Project: 1100051481 Gilbjerg Hoved, HDD

Drilled by: PAA VLJ/PB Date: 2022.05.03 Geologist: LSCH Public No.: Borehole: HDD. BH02

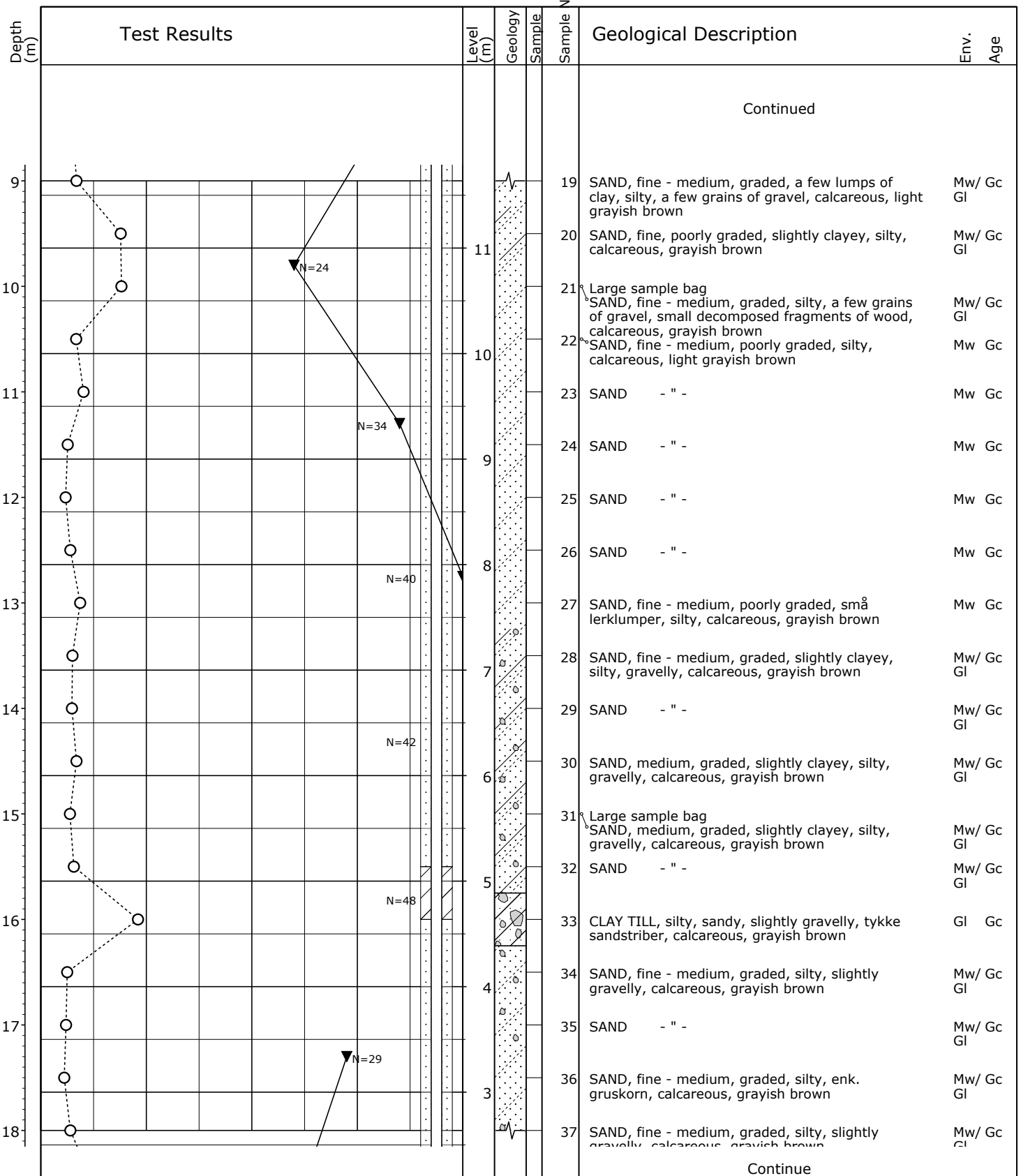
Prepared by: LSCH Checked by: RMH Approved by: RMH Date: 2022.06.10 Encl. No.: P. 3/3

GeoGIS2020 20.03.81 PSTGUK 04-07-2022 12:29:22



Project: 1100051481 Gilbjerg Hoved, HDD
 Drilled by: PAA RJ/PB Date: 2022.05.31 Geologist: LSCH Public No.: Borehole: HDD. BH03
 Prepared by: LSCH Checked by: RMH Approved by: RMH Date: 2022.06.10 Encl. No.: P. 1/4

GeoGIS2020 20.03.81 PSTGUK 04-07-2022 12:30:30

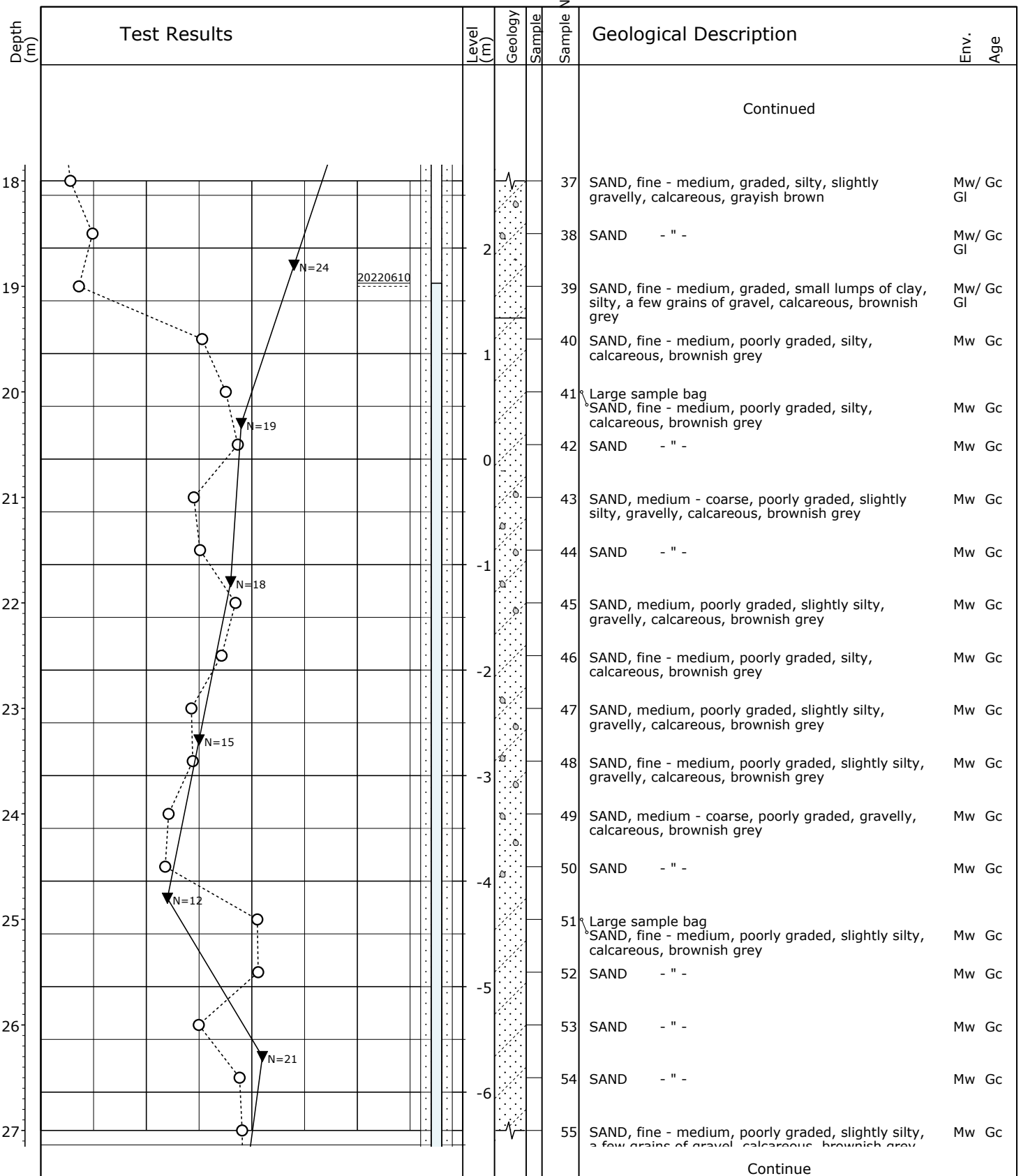


○ 10 20 30 W (%)
 ▼ 10 20 30 N (Blows/30 cm)

Glacial deposits may contain cobbles and boulders
 Stand Pipe: 1: ø25 - Top Level: 20.64 m
 Method: Cased Shell & Auger 8'
 Projection: UTM32E89
 X: 703268 (m) Y: 6224669 (m) Plan: 2.101

Project: 1100051481 Gilbjerg Hoved, HDD
 Drilled by: PAA RJ/PB Date: 2022.05.31 Geologist: LSCH Public No.: Borehole: HDD. BH03
 Prepared by: LSCH Checked by: RMH Approved by: RMH Date: 2022.06.10 Encl. No.: P. 2/4

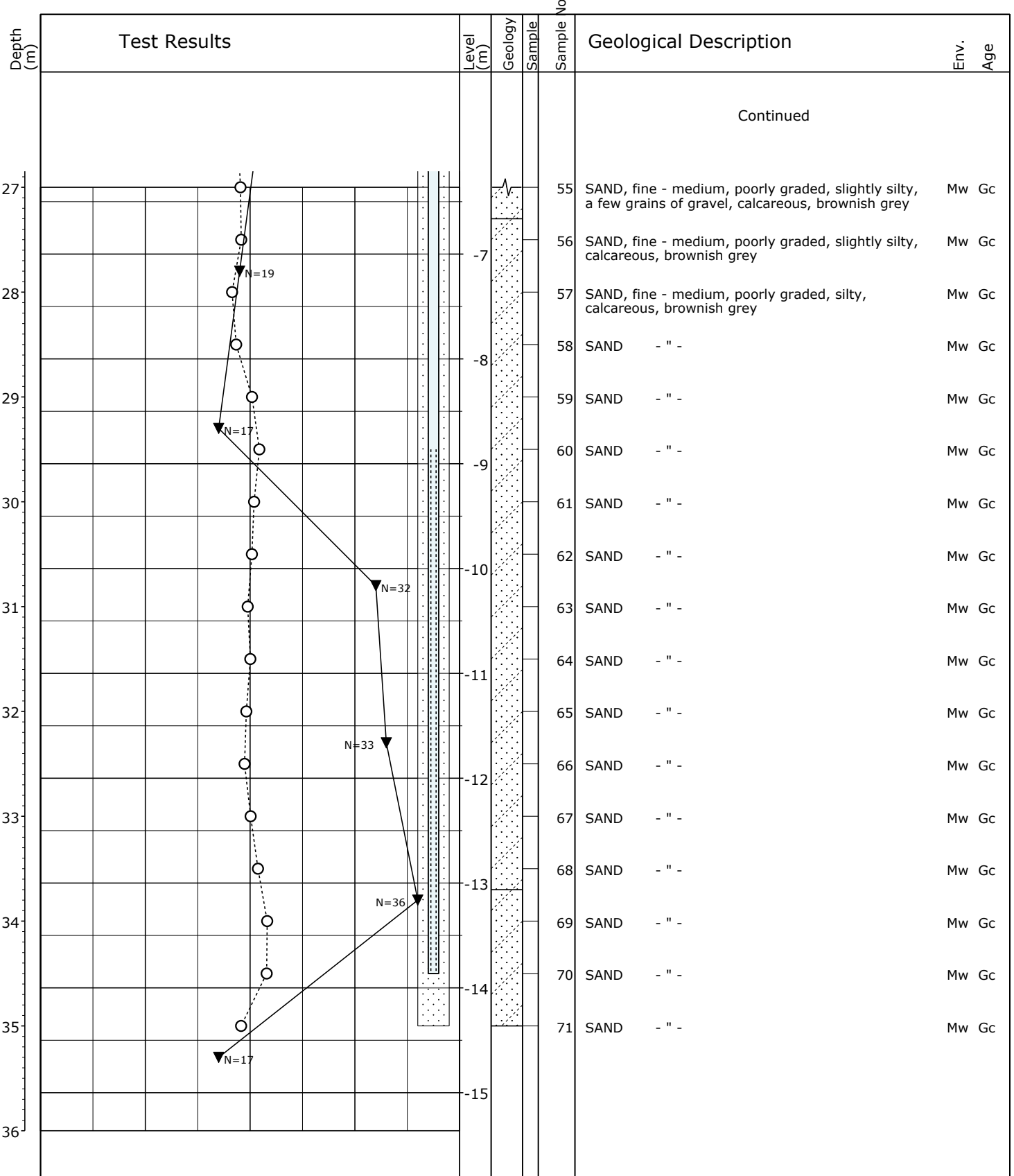
GeoGIS2020 20.03.81 PSTGUK 04-07-2022 12:30:30



○	10	20	30	W (%)	Glacial deposits may contain cobbles and boulders
▼	10	20	30	N (Blows/30 cm)	
					Stand Pipe: 1: ø25 - Top Level: 20.64 m
					Method: Cased Shell & Auger 8'
					Projection: UTM32E89
					X: 703268 (m) Y: 6224669 (m) Plan: 2.101

Project: 1100051481 Gilbjerg Hoved, HDD
 Drilled by: PAA RJ/PB Date: 2022.05.31 Geologist: LSCH Public No.: Borehole: HDD. BH03
 Prepared by: LSCH Checked by: RMH Approved by: RMH Date: 2022.06.10 Encl. No.: P. 3/4

GeoGIS2020 20.03.81 PSTGUK 04-07-2022 12:30:30

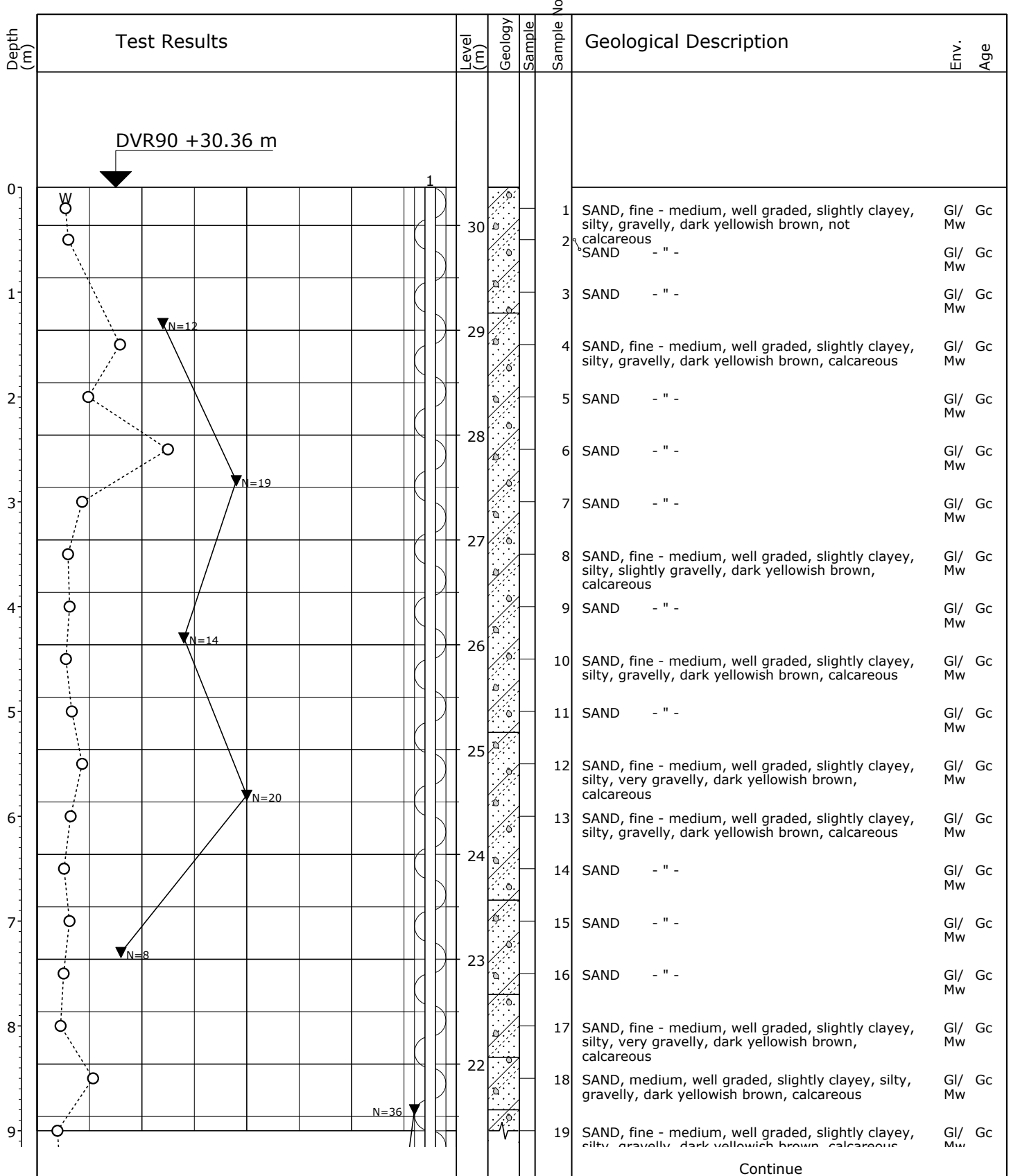


○ 10 20 30 W (%)
 ▼ 10 20 30 N (Blows/30 cm)

Glacial deposits may contain cobbles and boulders
 Stand Pipe: 1: ø25 - Top Level: 20.64 m
 Method: Cased Shell & Auger 8'
 Projection: UTM32E89
 X: 703268 (m) Y: 6224669 (m) Plan: 2.101

Project: 1100051481 **Gilbjerg Hoved, HDD**
 Drilled by: PAA RJ/PB Date: 2022.05.31 Geologist: LSCH Public No.: Borehole: HDD. BH03
 Prepared by: LSCH Checked by: RMH Approved by: RMH Date: 2022.06.10 Encl. No.: P. 4/4

GeoGIS2020 20.03.81 PSTGUK 04-07-2022 12:30:30

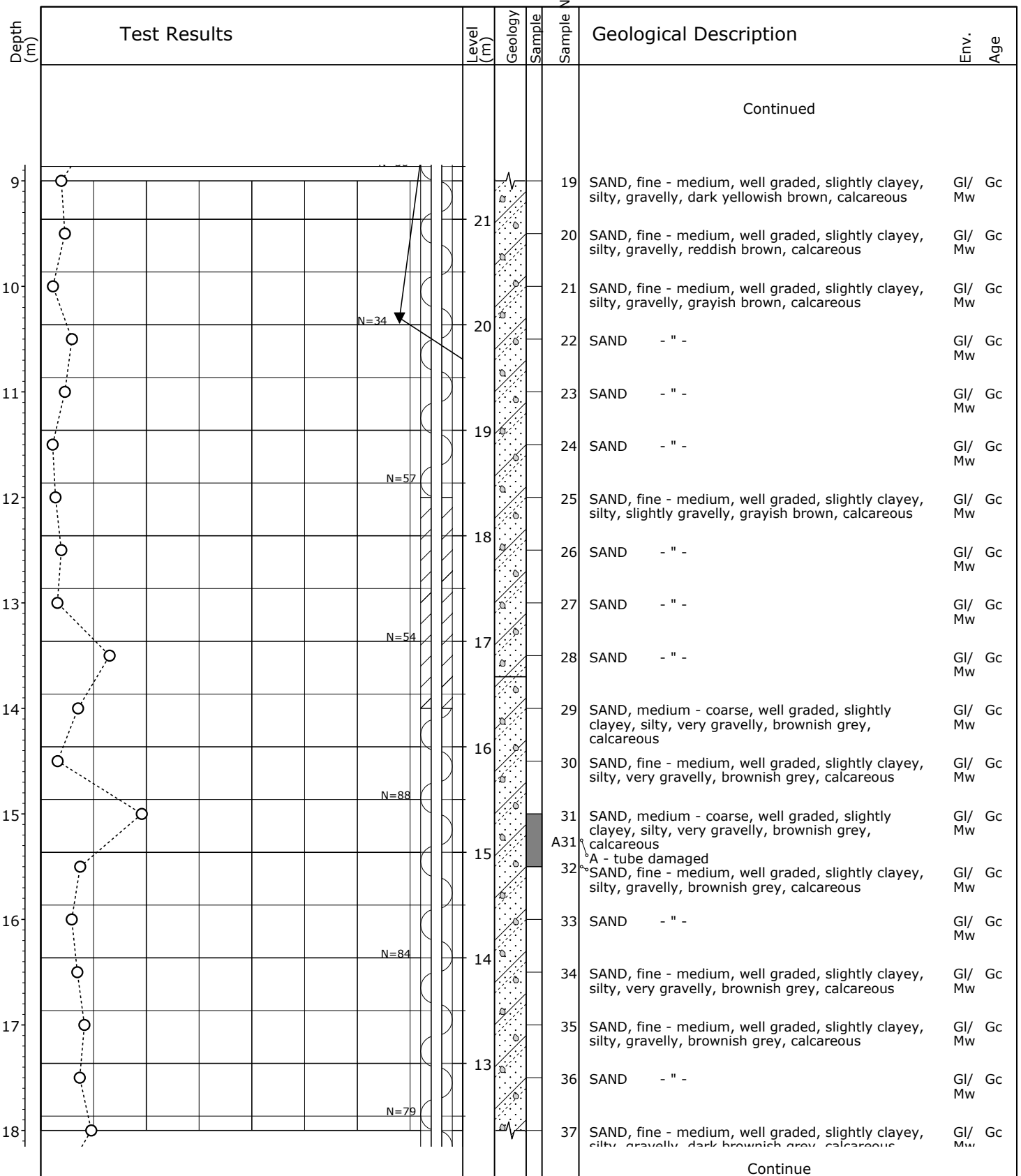


Continue

○	10	20	30	W (%)	Glacial deposits may contain cobbles and boulders
▼	10	20	30	N (Blows/30 cm)	Stand Pipe: 1: ø25 - Top Level: 30.36 m
					Method: Cased Shell & Auger 8'
					Projection: UTM32E89
					X: 703233 (m) Y: 6224816 (m) Plan: 2.101

Project: 1100051481 Gilbjerg Hoved, HDD
 Drilled by: PAA SS/KG Date: 2022.05.23 Geologist: LSCH Public No.: Borehole: HDD. BH04
 Prepared by: LSCH Checked by: RMH Approved by: RMH Date: 2022.06.10 Encl. No.: P. 1/6

GeoGIS2020 20.03.81 PSTGUK 04-07-2022 12:26:40



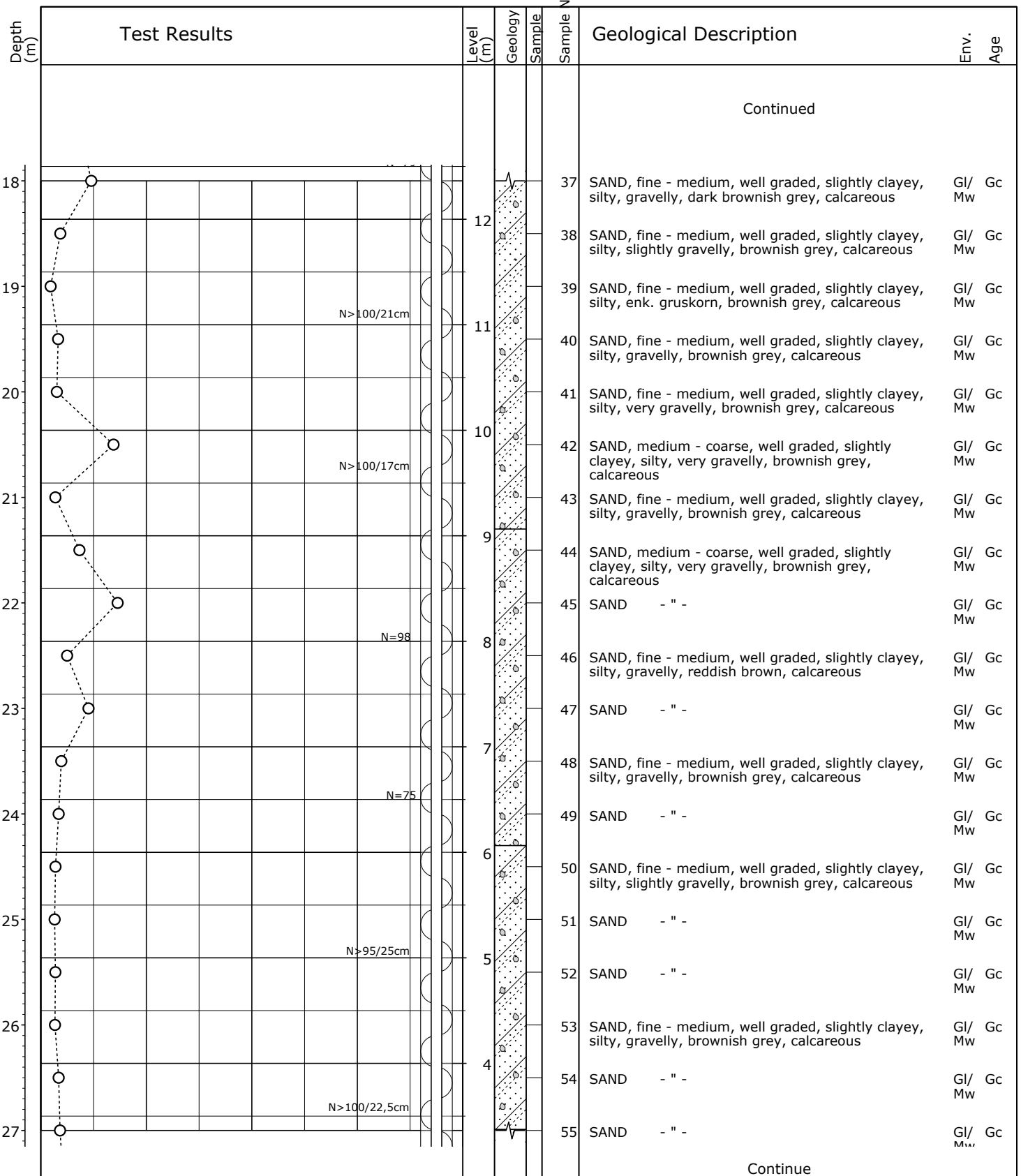
○	10	20	30	W (%)	Glacial deposits may contain cobbles and boulders
▼	10	20	30	N (Blows/30 cm)	
					Stand Pipe: 1: ø25 - Top Level: 30.36 m
					Method: Cased Shell & Auger 8'
					Projection: UTM32E89
					X: 703233 (m) Y: 6224816 (m) Plan: 2.101

Project: 1100051481 Gilbjerg Hoved, HDD

Drilled by: PAA SS/KG Date: 2022.05.23 Geologist: LSCH Public No.: Borehole: HDD. BH04

Prepared by: LSCH Checked by: RMH Approved by: RMH Date: 2022.06.10 Encl. No.: P. 2/6

GeoGIS2020 20.03.81 PSTGUK 04-07-2022 12:26:40

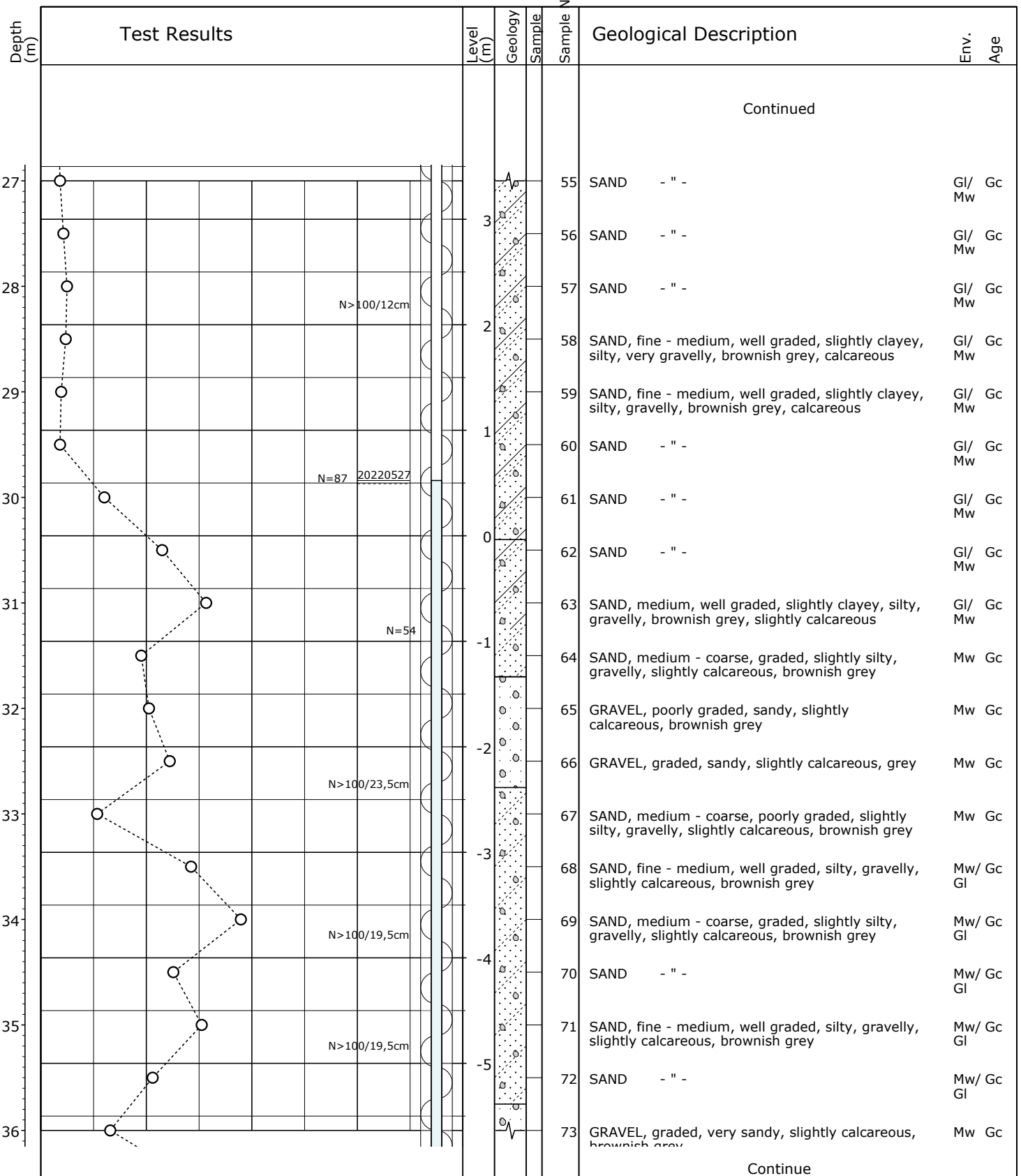


○ 10 20 30 W (%)
 ▼ 10 20 30 N (Blows/30 cm)

Glacial deposits may contain cobbles and boulders
 Stand Pipe: 1: ø25 - Top Level: 30.36 m
 Method: Cased Shell & Auger 8'
 Projection: UTM32E89
 X: 703233 (m) Y: 6224816 (m) Plan: 2.101

Project: 1100051481 Gilbjerg Hoved, HDD
 Drilled by: PAA SS/KG Date: 2022.05.23 Geologist: LSCH Public No.: Borehole: HDD. BH04
 Prepared by: LSCH Checked by: RMH Approved by: RMH Date: 2022.06.10 Encl. No.: P. 3/6

GeoGIS2020 20.03.81 PSTGUK 04-07-2022 12:26:40



Continued

Continue

○	10	20	30	W (%)
▼	10	20	30	N (Blows/30 cm)

Glacial deposits may contain cobbles and boulders

Stand Pipe: 1: ø25 - Top Level: 30.36 m

Method: Cased Shell & Auger 8'

Projection: UTM32E89

X: 703233 (m) Y: 6224816 (m) Plan: 2.101

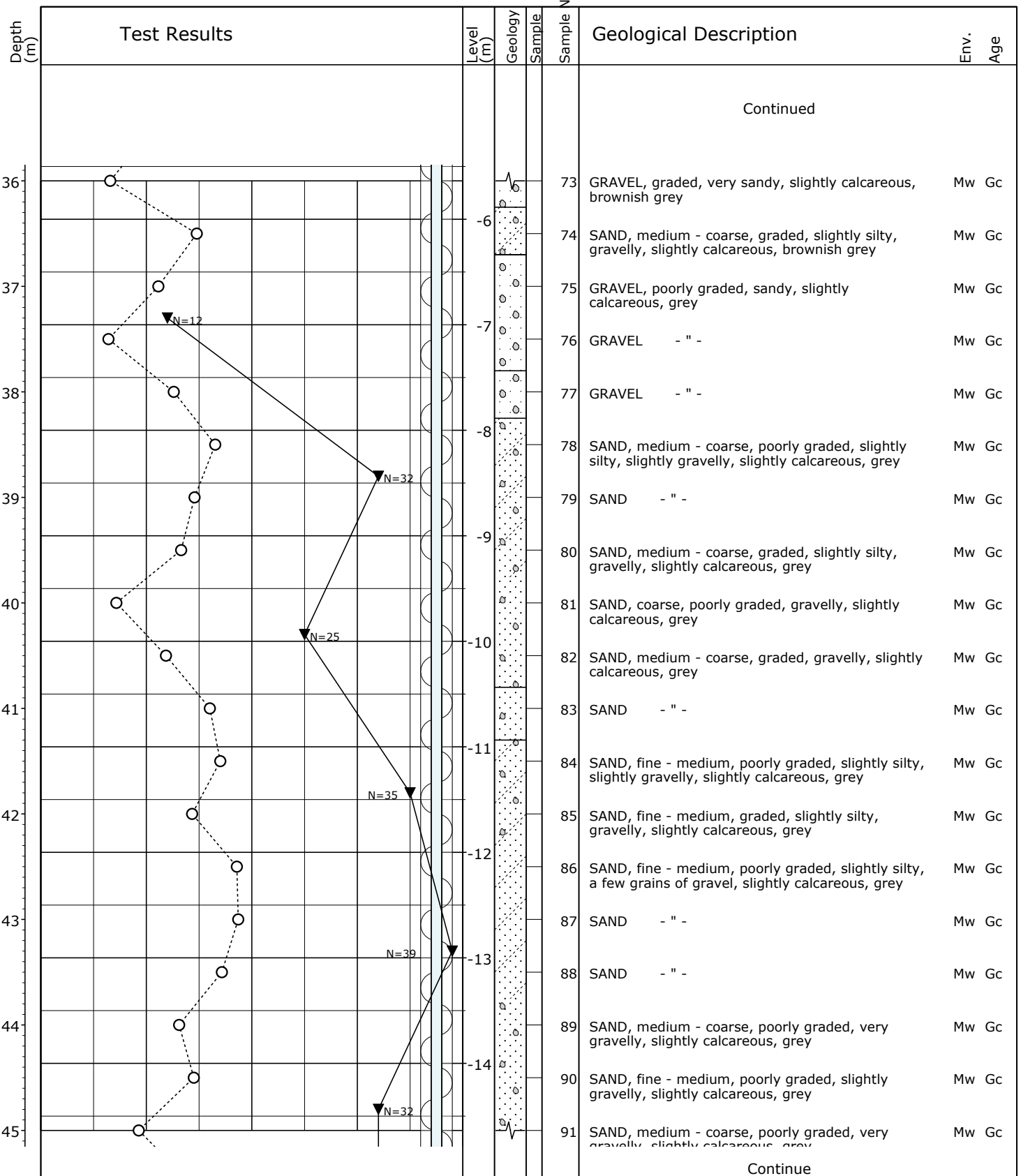
Project: 1100051481 Gilbjerg Hoved, HDD

Drilled by: PAA SS/KG Date: 2022.05.23 Geologist: LSCH Public No.: Borehole: HDD. BH04

Prepared by: LSCH Checked by: RMH Approved by: RMH Date: 2022.06.10 Encl. No.: P. 4/6



Borehole Log

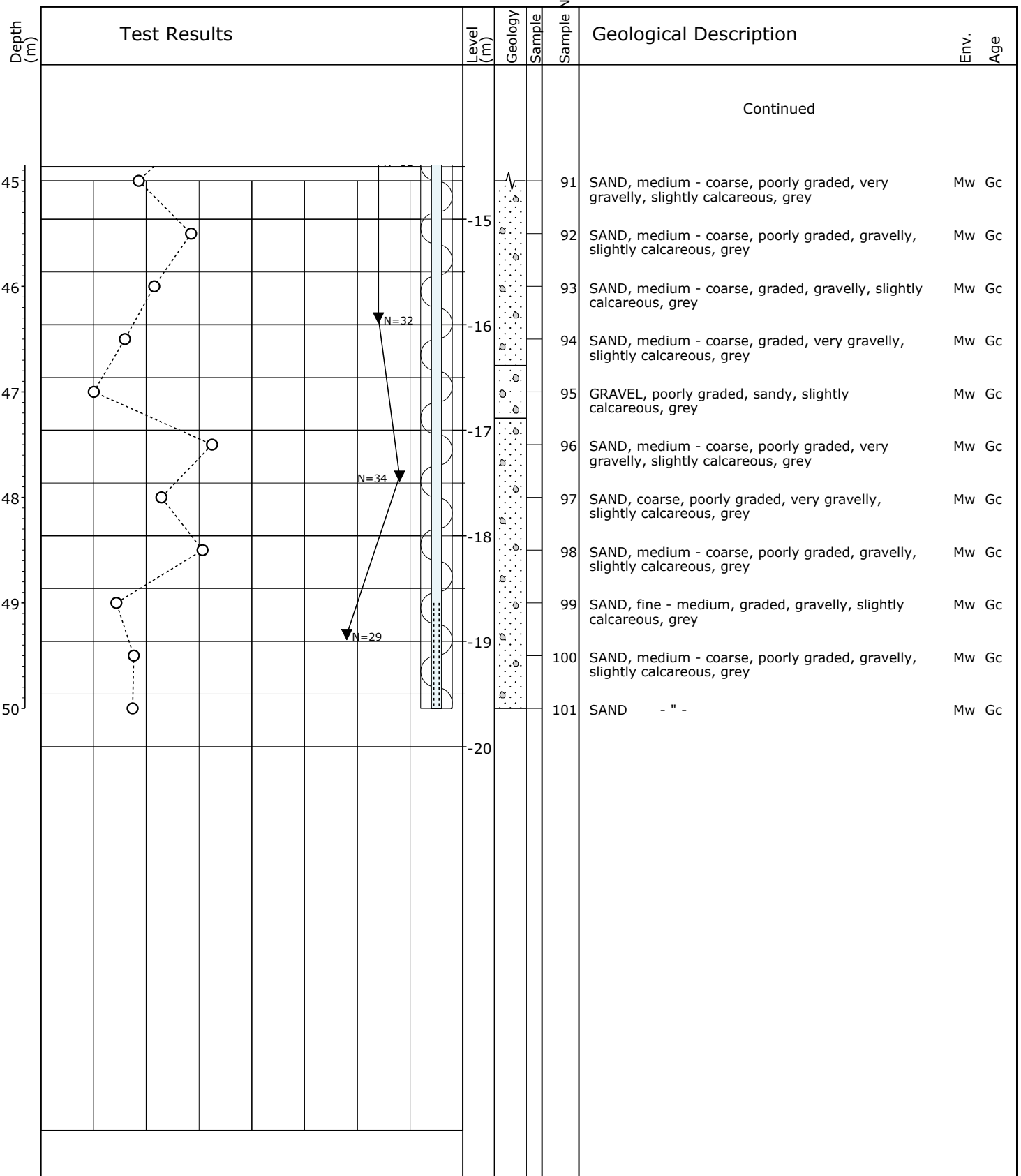


○ 10 20 30 W (%)
 ▼ 10 20 30 N (Blows/30 cm)

Continue
 Glacial deposits may contain cobbles and boulders
 Stand Pipe: 1: ø25 - Top Level: 30.36 m
 Method: Cased Shell & Auger 8'
 Projection: UTM32E89
 X: 703233 (m) Y: 6224816 (m) Plan: 2.101

Project: 1100051481 Gilbjerg Hoved, HDD
 Drilled by: PAA SS/KG Date: 2022.05.23 Geologist: LSCH Public No.: Borehole: HDD. BH04
 Prepared by: LSCH Checked by: RMH Approved by: RMH Date: 2022.06.10 Encl. No.: P. 5/6

GeoGIS2020 20.03.81 PSTGUK 04-07-2022 12:26:40

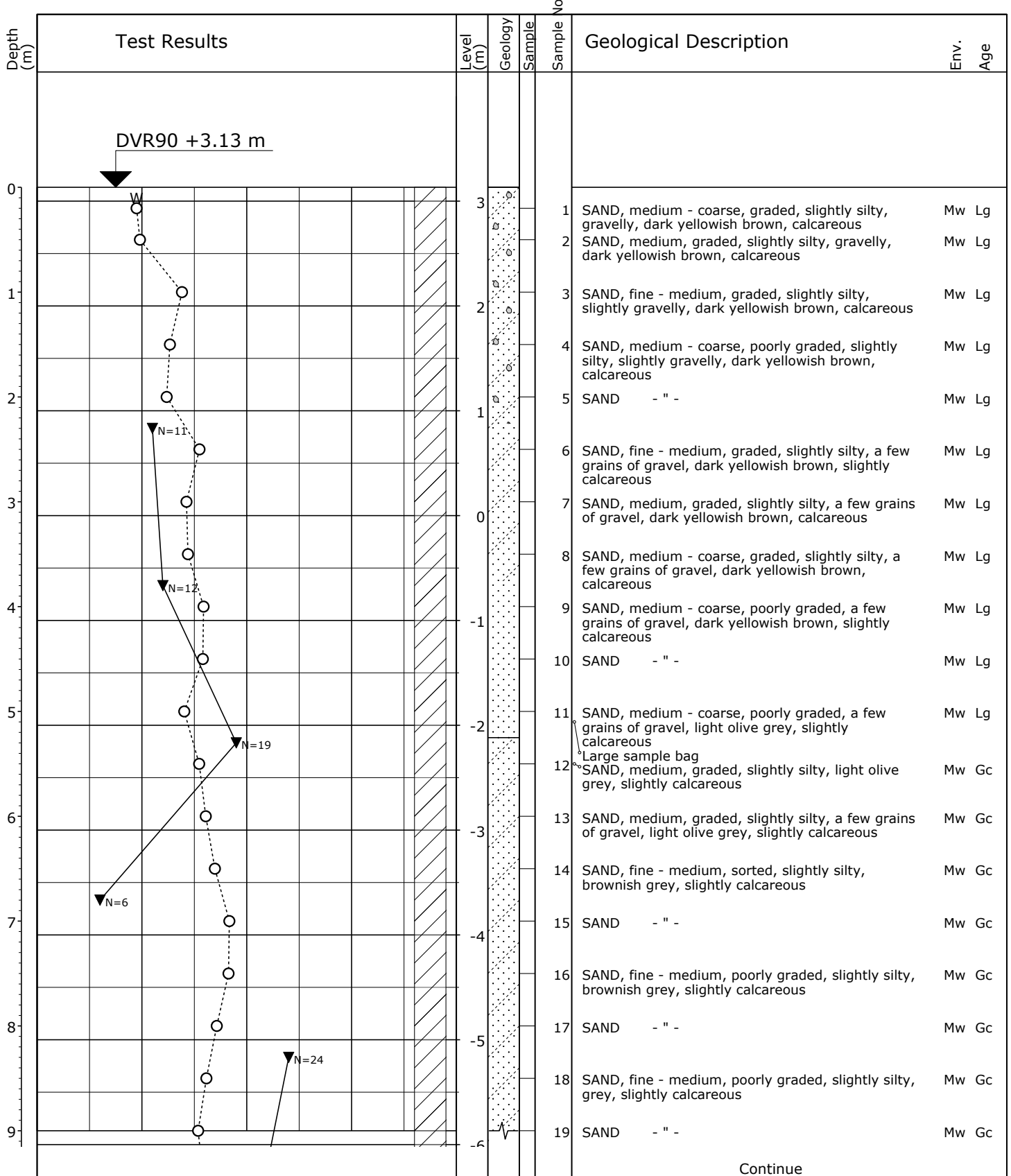


○ 10 20 30 W (%)
 ▼ 10 20 30 N (Blows/30 cm)

Glacial deposits may contain cobbles and boulders
 Stand Pipe: 1: ø25 - Top Level: 30.36 m
 Method: Cased Shell & Auger 8'
 Projection: UTM32E89
 X: 703233 (m) Y: 6224816 (m) Plan: 2.101

Project: 1100051481 Gilbjerg Hoved, HDD
 Drilled by: PAA SS/KG Date: 2022.05.23 Geologist: LSCH Public No.: Borehole: HDD. BH04
 Prepared by: LSCH Checked by: RMH Approved by: RMH Date: 2022.06.10 Encl. No.: P. 6/6

GeoGIS2020 20.03.81 PSTGUK 04-07-2022 12:26:40



Continue

○	10	20	30	W (%)
▼	10	20	30	N (Blows/30 cm)

Glacial deposits may contain cobbles and boulders

Method: Cased Shell & Auger 6'
 Projection: UTM32E89
 X: 703167 (m) Y: 6224980 (m) Plan: 2.101

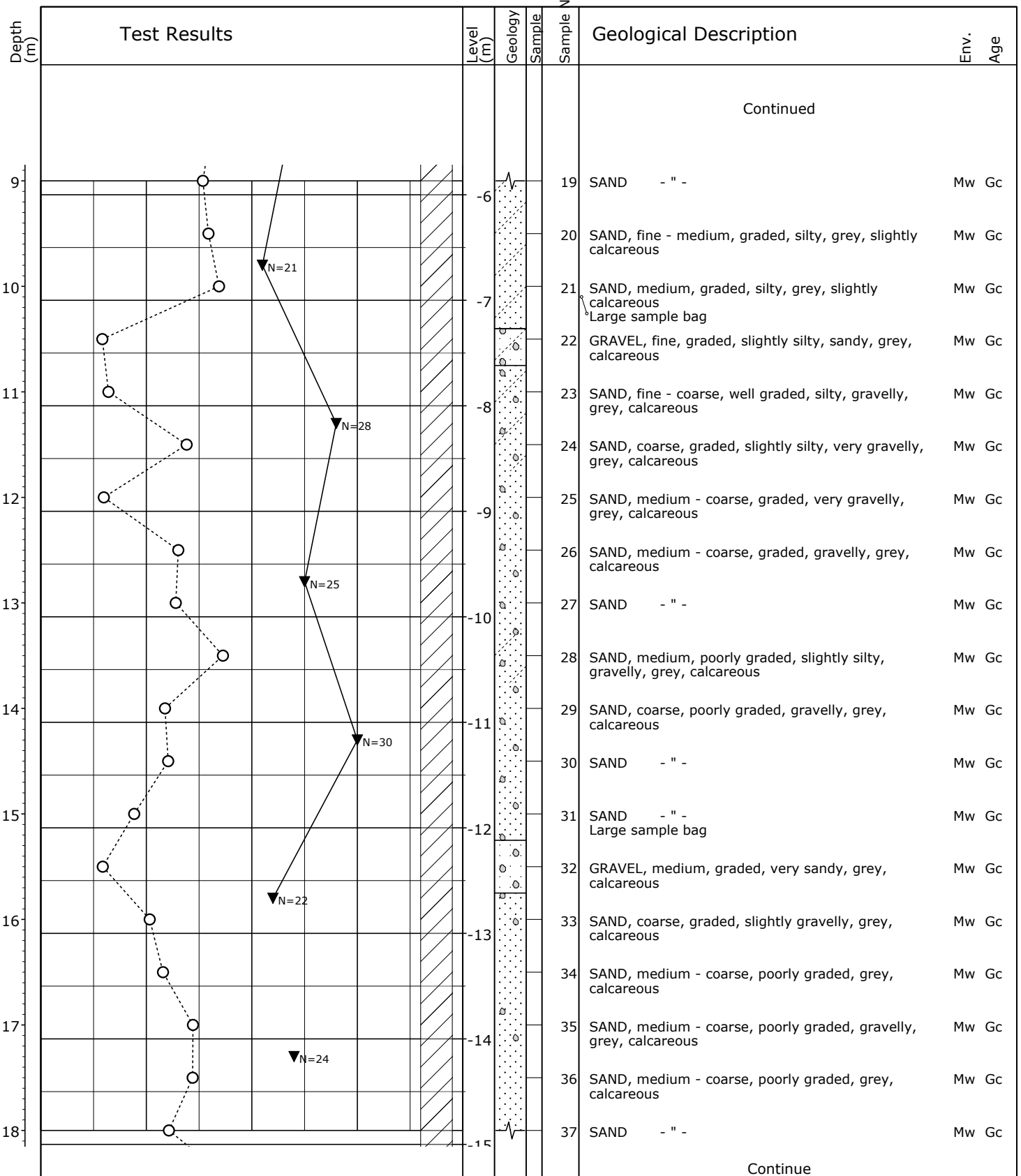
Project: 1100051481 Gilbjerg Hoved, HDD

Drilled by: PAA VLJ/PB Date: 2022.04.25 Geologist: LSCH Public No.: Borehole: HDD. BH05

Prepared by: LSCH Checked by: RMH Approved by: RMH Date: 2022.06.10 Encl. No.: P. 1/3



Borehole Log



Continued

Continue

○ 10 20 30 W (%)
 ▼ 10 20 30 N (Blows/30 cm)

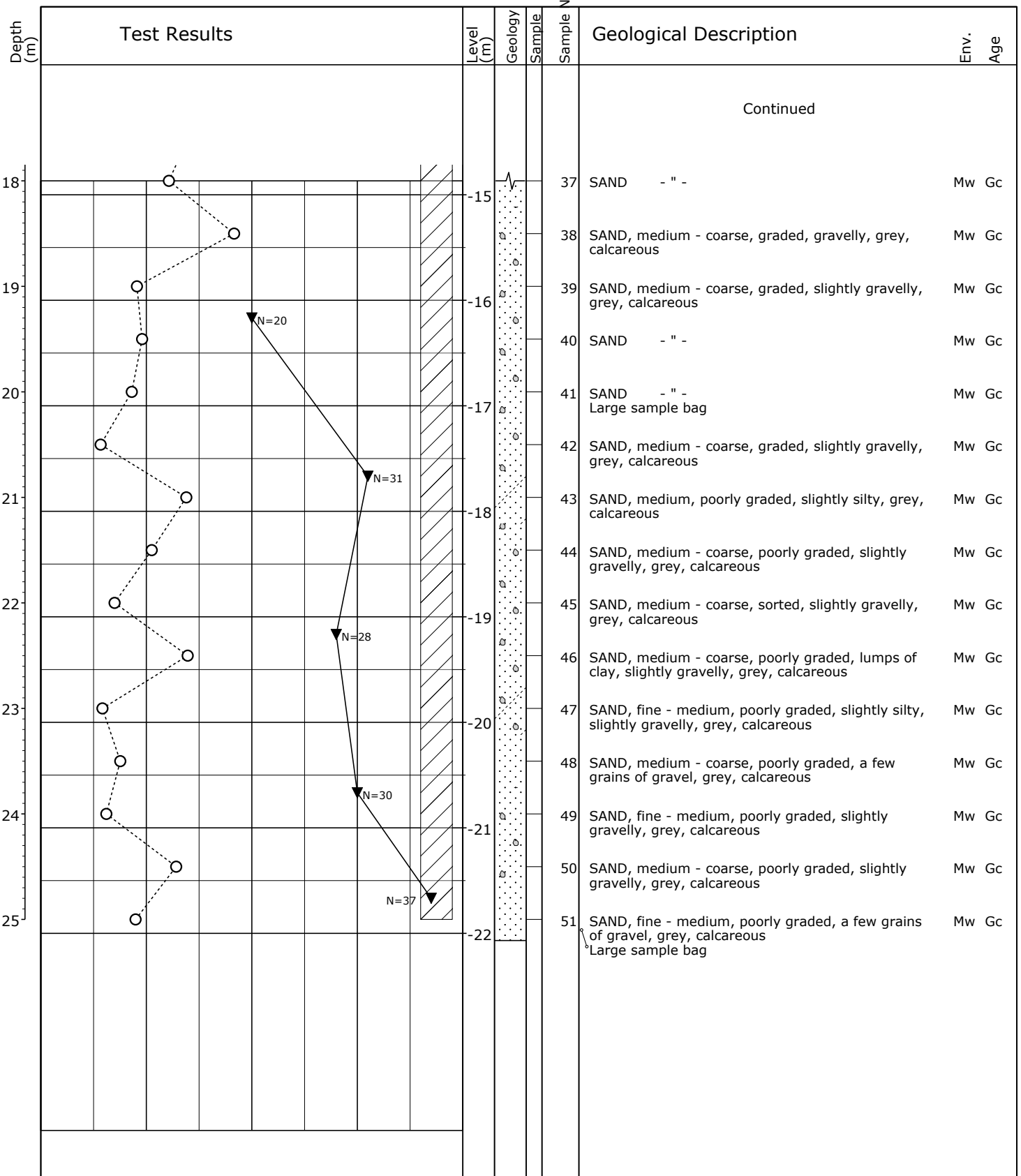
Glacial deposits may contain cobbles and boulders

Method: Cased Shell & Auger 6'
 Projection: UTM32E89
 X: 703167 (m) Y: 6224980 (m) Plan: 2.101

Project: 1100051481 Gilbjerg Hoved, HDD
 Drilled by: PAA VLJ/PB Date: 2022.04.25 Geologist: LSCH Public No.: Borehole: HDD. BH05
 Prepared by: LSCH Checked by: RMH Approved by: RMH Date: 2022.06.10 Encl. No.: P. 2/3



Borehole Log



○ 10 20 30 W (%)
 ▼ 10 20 30 N (Blows/30 cm)

Glacial deposits may contain cobbles and boulders

Method: Cased Shell & Auger 6'
 Projection: UTM32E89
 X: 703167 (m) Y: 6224980 (m) Plan: 2.101

Project: 1100051481 Gilbjerg Hoved, HDD
 Drilled by: PAA VLJ/PB Date: 2022.04.25 Geologist: LSCH Public No.: Borehole: HDD. BH05
 Prepared by: LSCH Checked by: RMH Approved by: RMH Date: 2022.06.10 Encl. No.: P. 3/3



Borehole Log

APPENDIX 5.1-5.5 – PARTICLE SIZE DISTRIBUTION

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

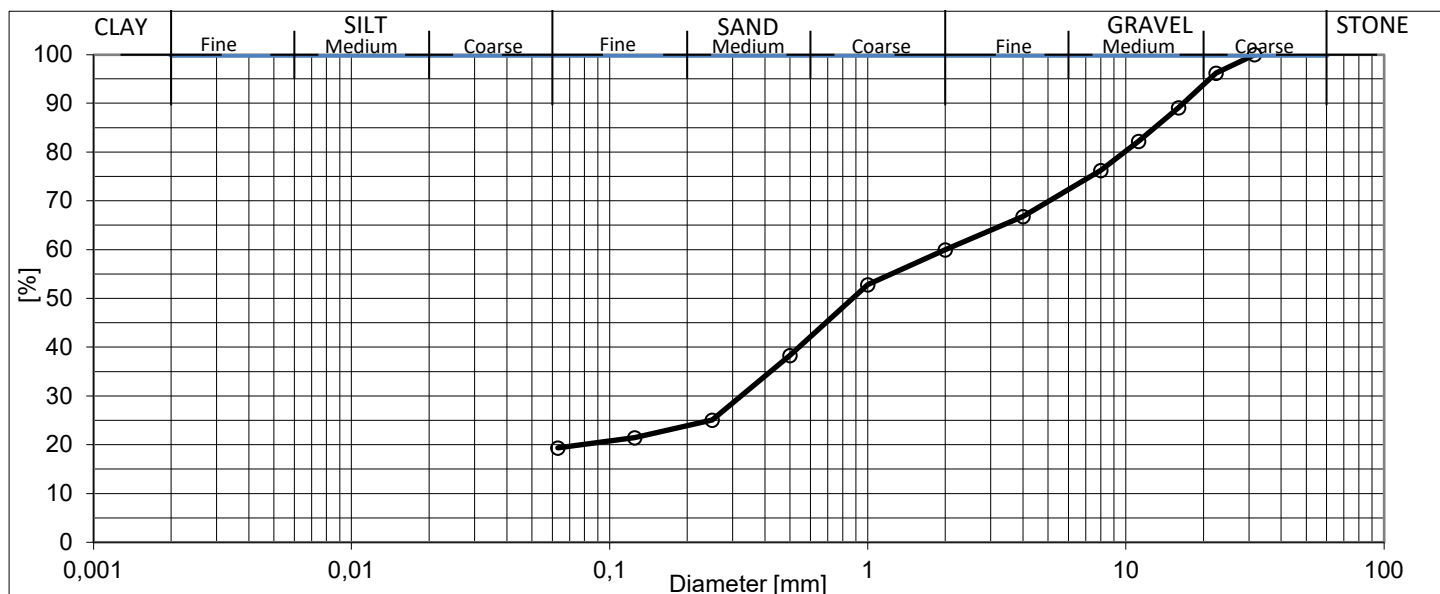
Inspection Section	BH01-S17-8,0
Sample Description	Sand, fine-medium
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	16. jun 2022

Sieving	
Sieve size [mm]	Passing %
31,5	100,0
22,4	96,2
16	89,1
11,2	82,2
8	76,3
4	66,8
2	60,0
1	52,8
0,5	38,3
0,25	25,0
0,125	21,4
0,063	19,4

Results	
D ₈₅	12,93
D ₆₀	2,00
D ₅₀	0,87
D ₁₅	
D ₁₀	

Coefficient of uniformity	
D ₆₀ /D ₁₀	



Made By: THAND

Checked By: CVZ

Date: 17. jun 2022

Date: 17. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

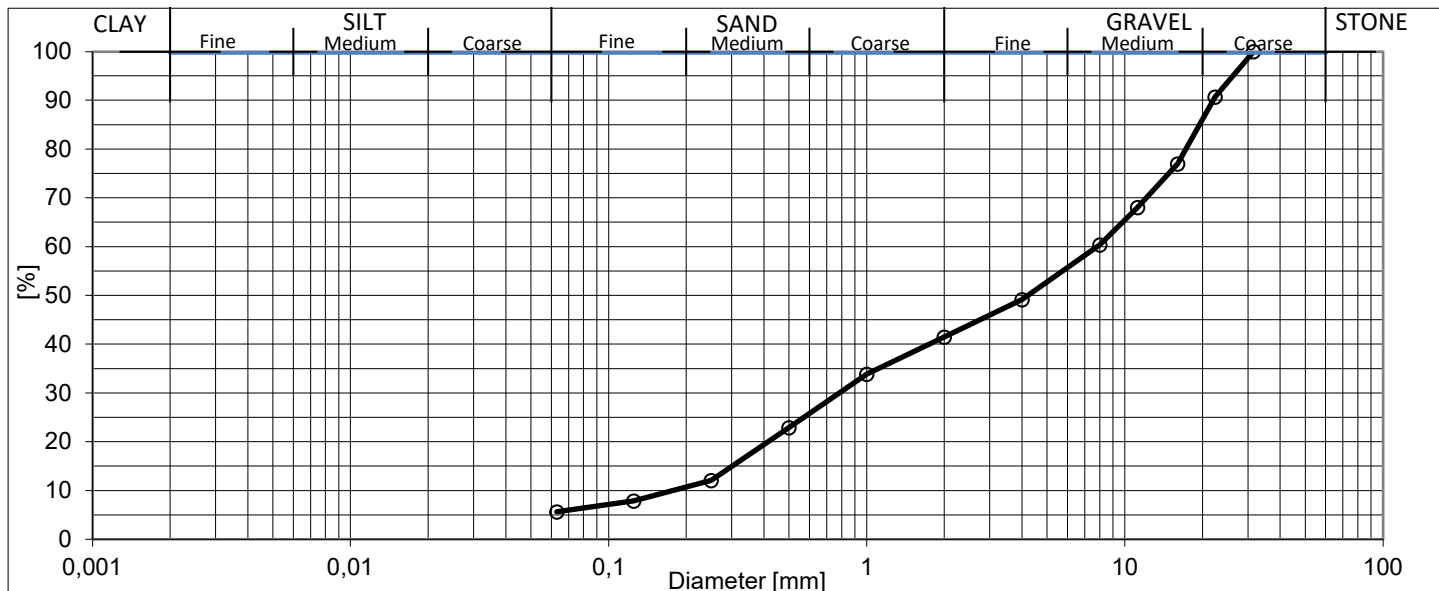
Inspection Section	BH01-S28-13,5
Sample Description	Sand, fine - medium
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	14. jun 2022

Sieving	
Sieve size [mm]	Passing %
31,5	100,0
22,4	90,7
16	76,9
11,2	68,0
8	60,3
4	49,1
2	41,5
1	33,9
0,5	22,9
0,25	12,1
0,125	7,9
0,063	5,7

Results	
D ₈₅	19,49
D ₆₀	7,83
D ₅₀	4,22
D ₁₅	0,30
D ₁₀	0,18

Coefficient of uniformity	
D ₆₀ /D ₁₀	44,12



Made By: MALT / THAND

Checked By: CVZ

Date: 14-06 / 16-06-2022

Date: 17. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

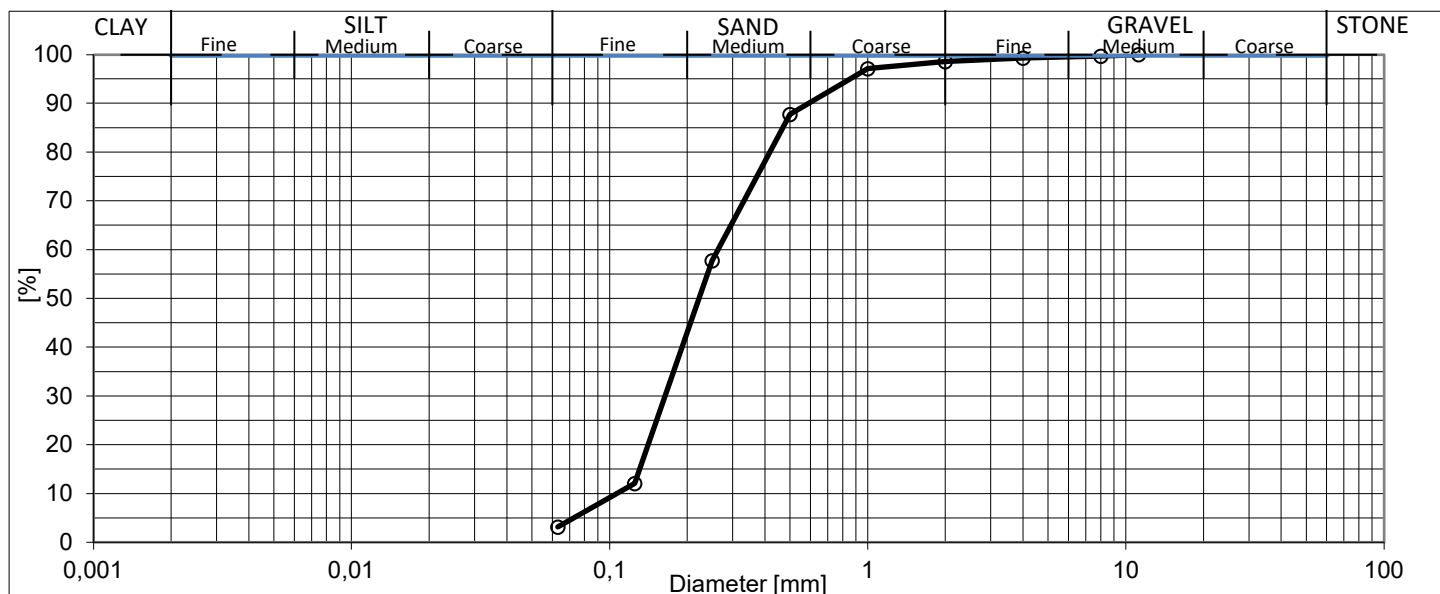
Inspection Section	BH01-S41-20
Sample Description	Sand, medium
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	20. jun 2022

Sieving	
Sieve size [mm]	Passing %
11,2	100,0
8	99,7
4	99,3
2	98,6
1	97,1
0,5	87,8
0,25	57,7
0,125	12,1
0,063	3,2

Results	
D ₈₅	0,47
D ₆₀	0,26
D ₅₀	0,22
D ₁₅	0,13
D ₁₀	0,11

Coefficient of uniformity	
D ₆₀ /D ₁₀	2,48



Made By: THAND

Checked By: CVZ

Date: 20. jun 2022

Date: 20. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

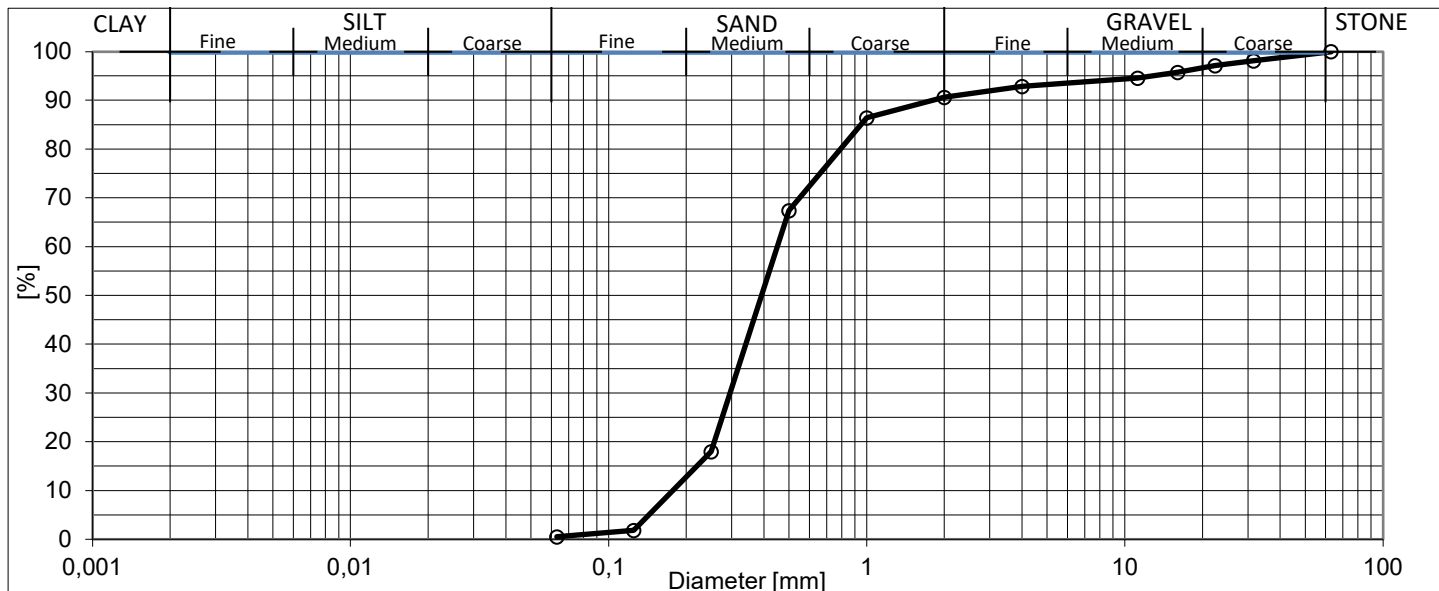
Inspection Section	BH01-S51-25
Sample Description	Sand, medium
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	20. jun 2022

Sieving	
Sieve size [mm]	Passing %
63	100,0
31,5	98,1
22,4	97,1
16	95,7
11,2	94,6
4	92,9
2	90,6
1	86,4
0,5	67,4
0,25	18,0
0,125	1,8
0,063	0,5

Results	
D ₈₅	0,95
D ₆₀	0,45
D ₅₀	0,39
D ₁₅	0,22
D ₁₀	0,18

Coefficient of uniformity	
D ₆₀ /D ₁₀	2,54



Made By: THAND

Checked By: CVZ

Date: 20. jun 2022

Date: 20. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

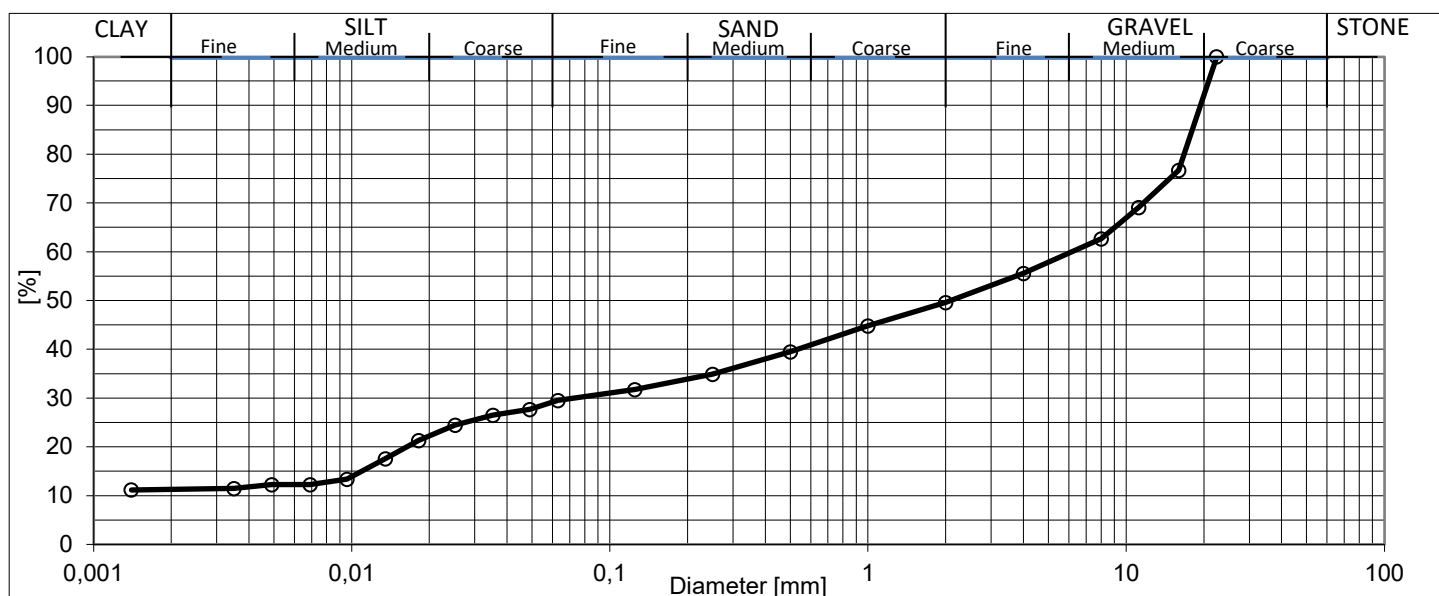
Inspection Section	BH02-S11-5
Sample Description	Sand, fine - medium
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	17. jun 2022

Sieving	
Sieve size [mm]	Passing %
22,4	100,0
16	76,7
11,2	69,1
8	62,7
4	55,6
2	49,6
1	44,8
0,5	39,5
0,25	34,9
0,125	31,7
0,063	29,6
0,049	27,7
0,0353	26,5
0,0252	24,5
0,0182	21,3
0,0135	17,6
0,0096	13,4
0,0069	12,3
0,0049	12,3
0,0035	11,5
0,0014	11,2

Results	
D ₈₅	18,03
D ₆₀	6,16
D ₅₀	2,09
D ₁₅	0,012
D ₁₀	

Coefficient of uniformity	
D ₆₀ /D ₁₀	



Made By: THME

Checked By: CVZ

Date: 17. jun 2022

Date: 21. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

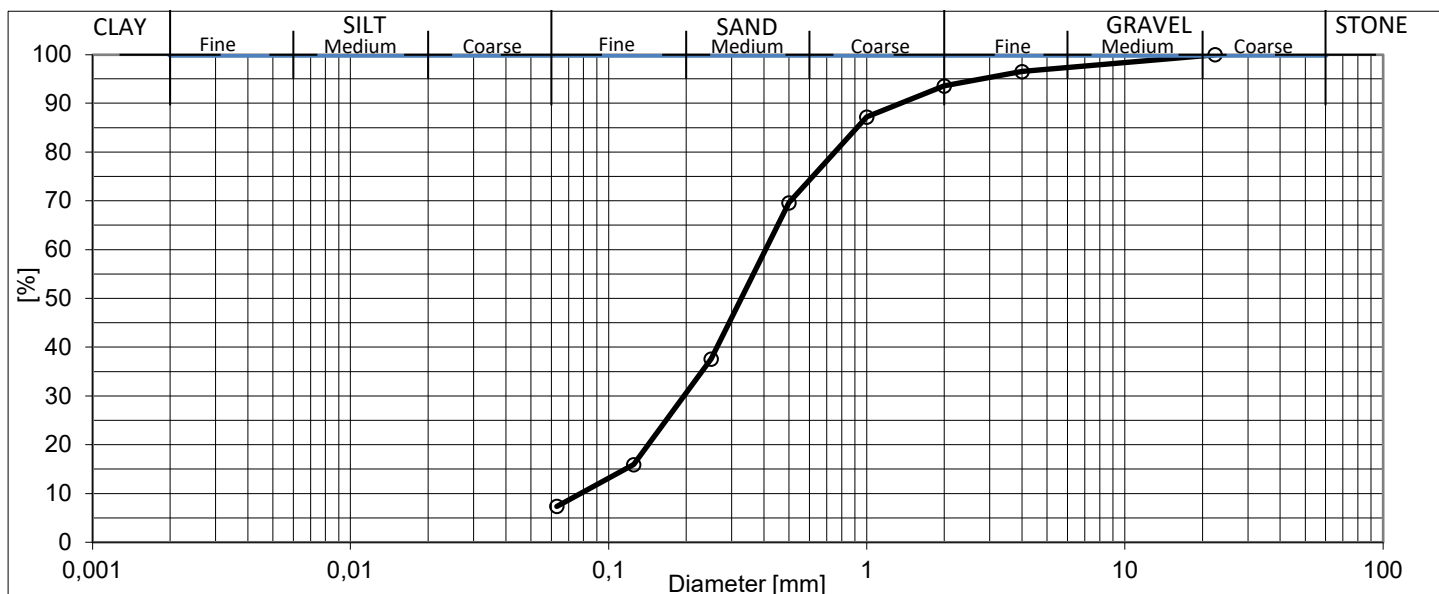
Inspection Section	BH02-S19-9
Sample Description	Sand, medium -coarse
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	16. jun 2022

Sieving	
Sieve size [mm]	Passing %
22,4	100,0
4	96,5
2	93,6
1	87,2
0,5	69,6
0,25	37,6
0,125	15,9
0,063	7,4

Results	
D ₈₅	0,92
D ₆₀	0,41
D ₅₀	0,33
D ₁₅	0,12
D ₁₀	0,08

Coefficient of uniformity	
D ₆₀ /D ₁₀	5,23



Made By: THME

Checked By: CVZ

Date: 17. jun 2022

Date: 17. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

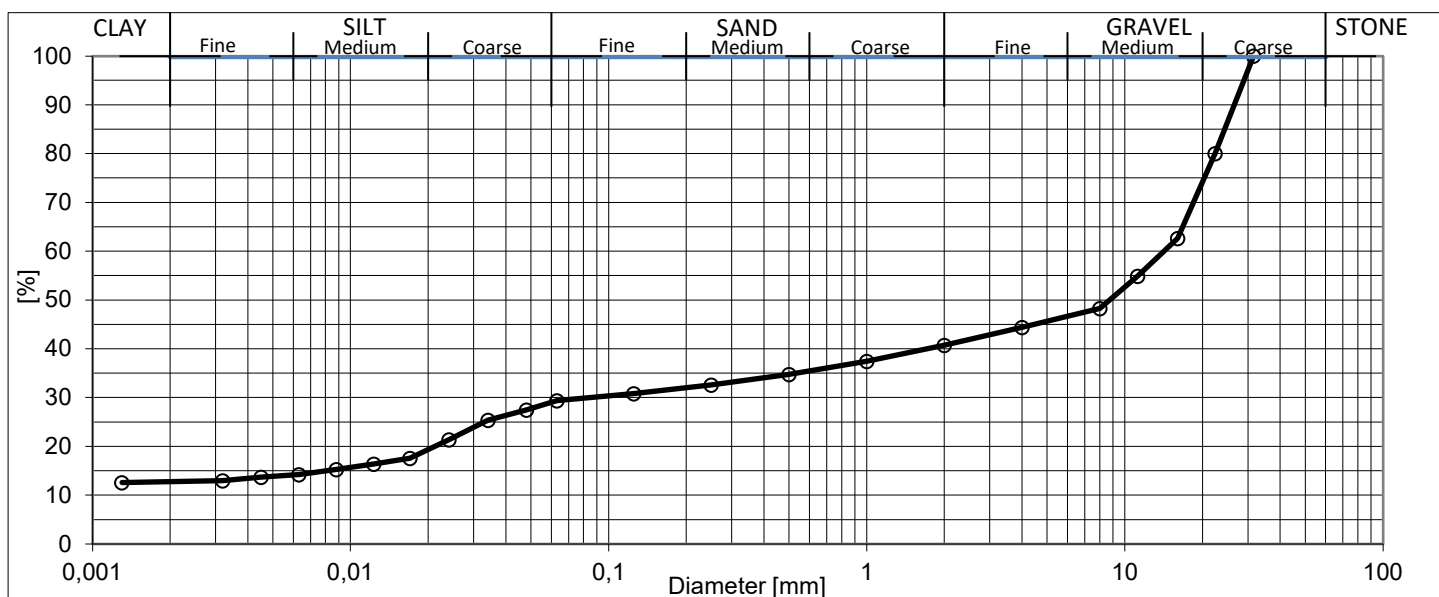
Inspection Section	BH02-S29-14
Sample Description	Gravel
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	17. jun 2022

Sieving	
Sieve size [mm]	Passing %
31,5	100,0
22,4	80,0
16	62,6
11,2	54,9
8	48,3
4	44,4
2	40,7
1	37,4
0,5	34,8
0,25	32,6
0,125	30,8
0,063	29,4
0,0481	27,5
0,0341	25,4
0,0241	21,4
0,017	17,6
0,0123	16,4
0,0088	15,3
0,0063	14,2
0,0045	13,7
0,0032	13,0
0,0013	12,6

Results	
D ₈₅	24,39
D ₆₀	14,19
D ₅₀	8,74
D ₁₅	0,008
D ₁₀	

Coefficient of uniformity	
D ₆₀ /D ₁₀	



Made By: THME

Checked By: CVZ

Date: 17. jun 2022

Date: 21. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

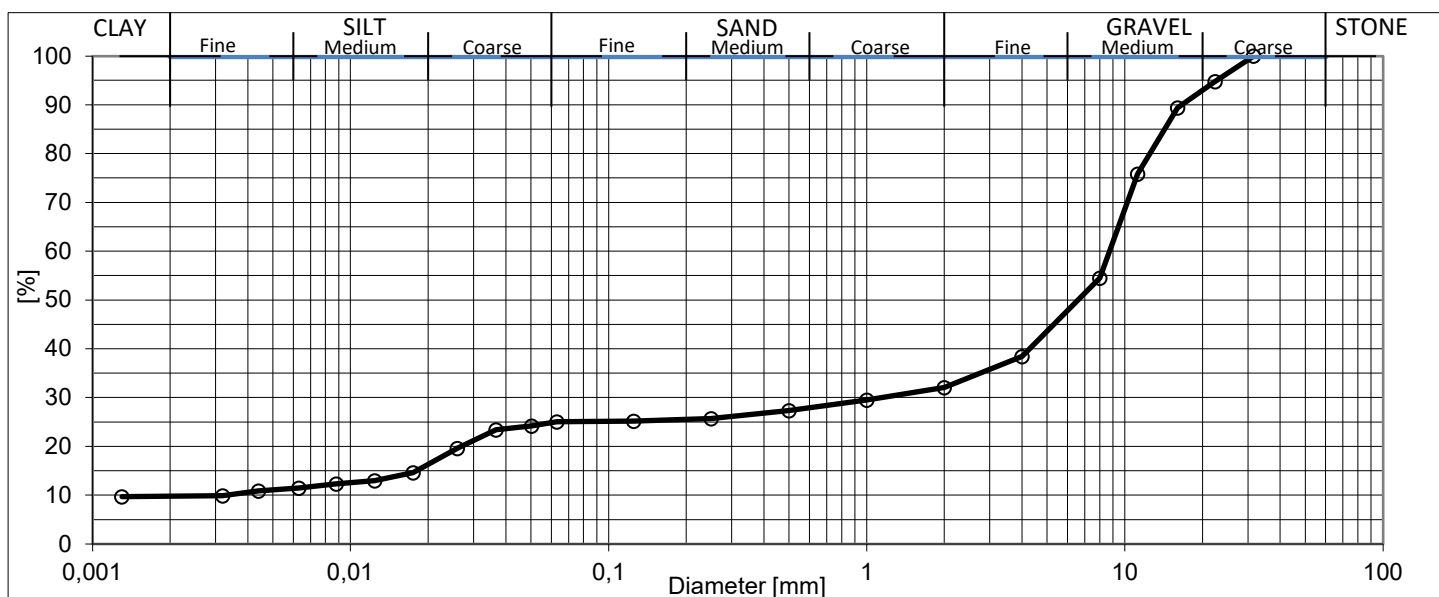
Inspection Section	BH02-S43-21
Sample Description	Gravel, sandy
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	16. jun 2022

Sieving	
Sieve size [mm]	Passing %
31,5	100,0
22,4	94,8
16	89,4
11,2	75,8
8	54,5
4	38,4
2	32,0
1	29,5
0,5	27,4
0,25	25,7
0,125	25,2
0,063	25,0
0,0503	24,2
0,0366	23,4
0,0259	19,6
0,0175	14,6
0,0124	13,0
0,0088	12,3
0,0063	11,5
0,0044	10,9
0,0032	9,9
0,0013	9,7

Results	
D ₈₅	14,25
D ₆₀	8,72
D ₅₀	6,58
D ₁₅	0,02
D ₁₀	0,003

Coefficient of uniformity	
D ₆₀ /D ₁₀	



Made By: THME

Checked By: CVZ

Date: 17. jun 2022

Date: 21. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

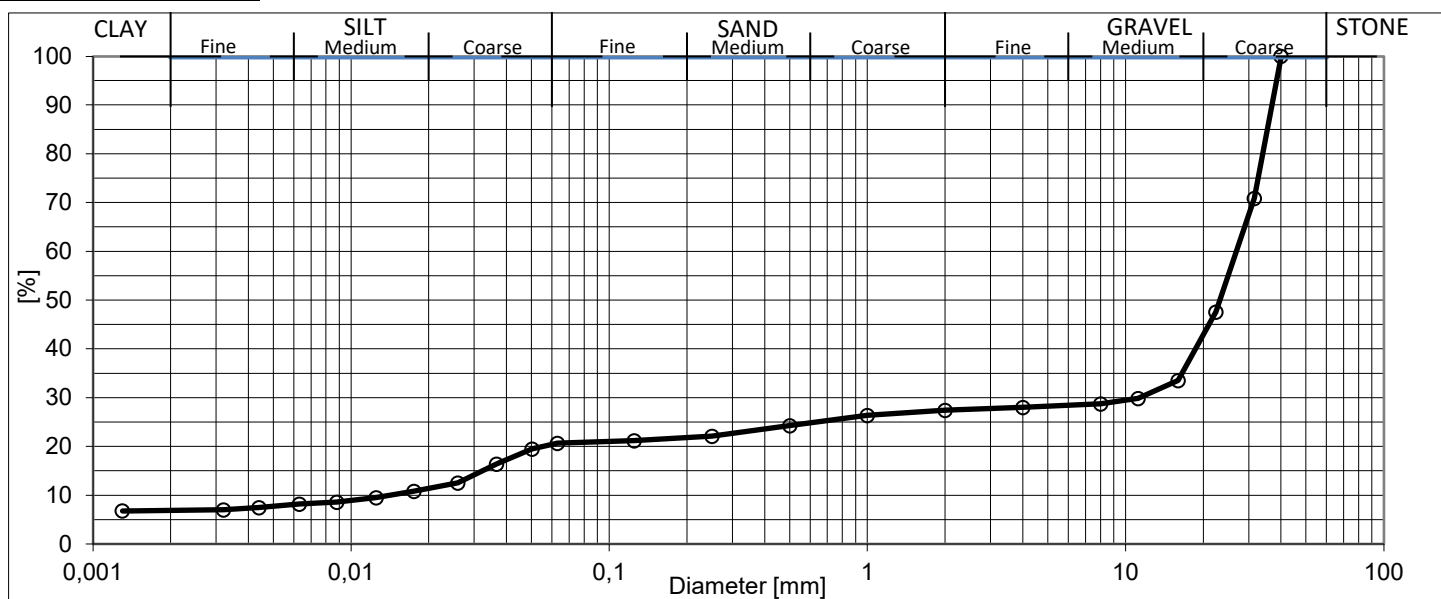
Inspection Section	BH02-S48-23,5
Sample Description	Sand, medium - coarse
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	16. jun 2022

Sieving	
Sieve size [mm]	Passing %
40	100,0
31,5	70,8
22,4	47,6
16	33,6
11,2	29,8
8	28,7
4	28,0
2	27,4
1	26,4
0,5	24,3
0,25	22,1
0,125	21,2
0,063	20,7
0,0503	19,5
0,0366	16,4
0,0259	12,5
0,0175	10,8
0,0125	9,5
0,0088	8,6
0,0063	8,2
0,0044	7,5
0,0032	7,0
0,0013	6,8

Results	
D ₈₅	35,37
D ₆₀	26,88
D ₅₀	23,22
D ₁₅	0,028
D ₁₀	0,017

Coefficient of uniformity	
D ₆₀ /D ₁₀	



Made By: THAND

Checked By: CVZ

Date: 17. jun 2022

Date: 21. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

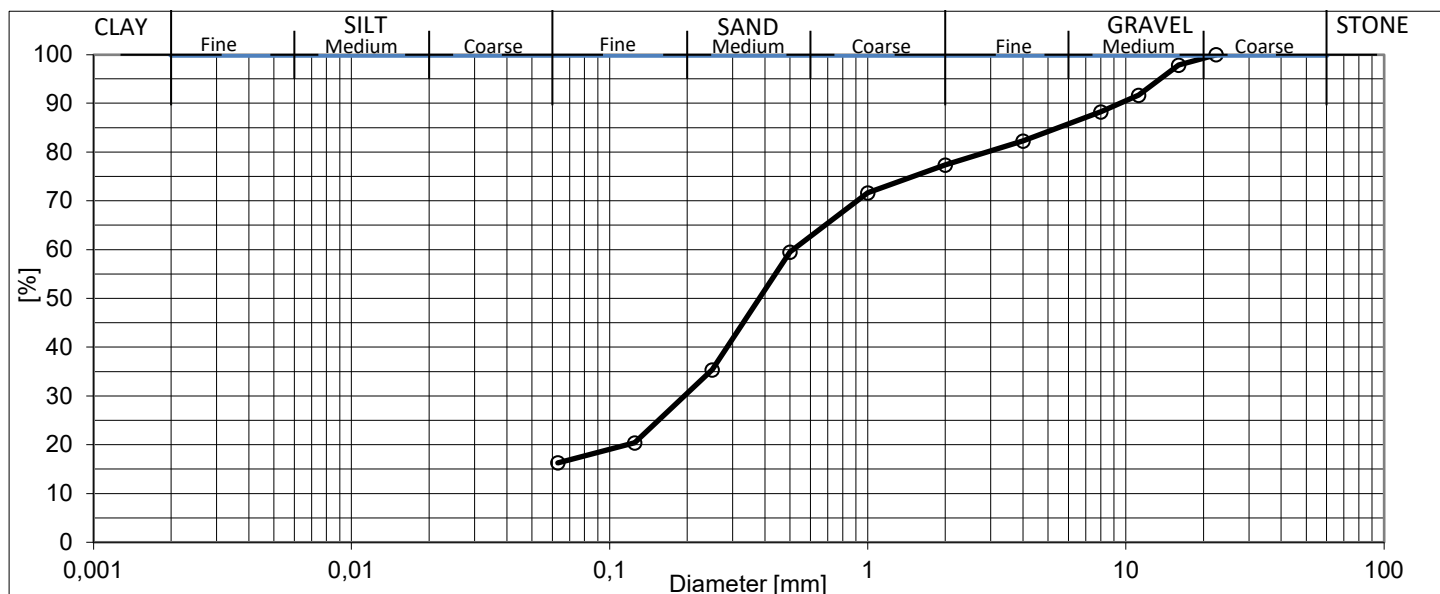
Inspection Section	BH03-S5-2
Sample Description	Sand, fine - medium
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	15. jun 2022

Sieving	
Sieve size [mm]	Passing %
22,4	100,0
16	97,9
11,2	91,7
8	88,3
4	82,3
2	77,3
1	71,7
0,5	59,5
0,25	35,3
0,125	20,4
0,063	16,3

Results	
D ₈₅	5,49
D ₆₀	0,51
D ₅₀	0,38
D ₁₅	
D ₁₀	

Coefficient of uniformity	
D ₆₀ /D ₁₀	



Made By: THAND

Checked By: CVZ

Date: 16. jun 2022

Date: 16. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

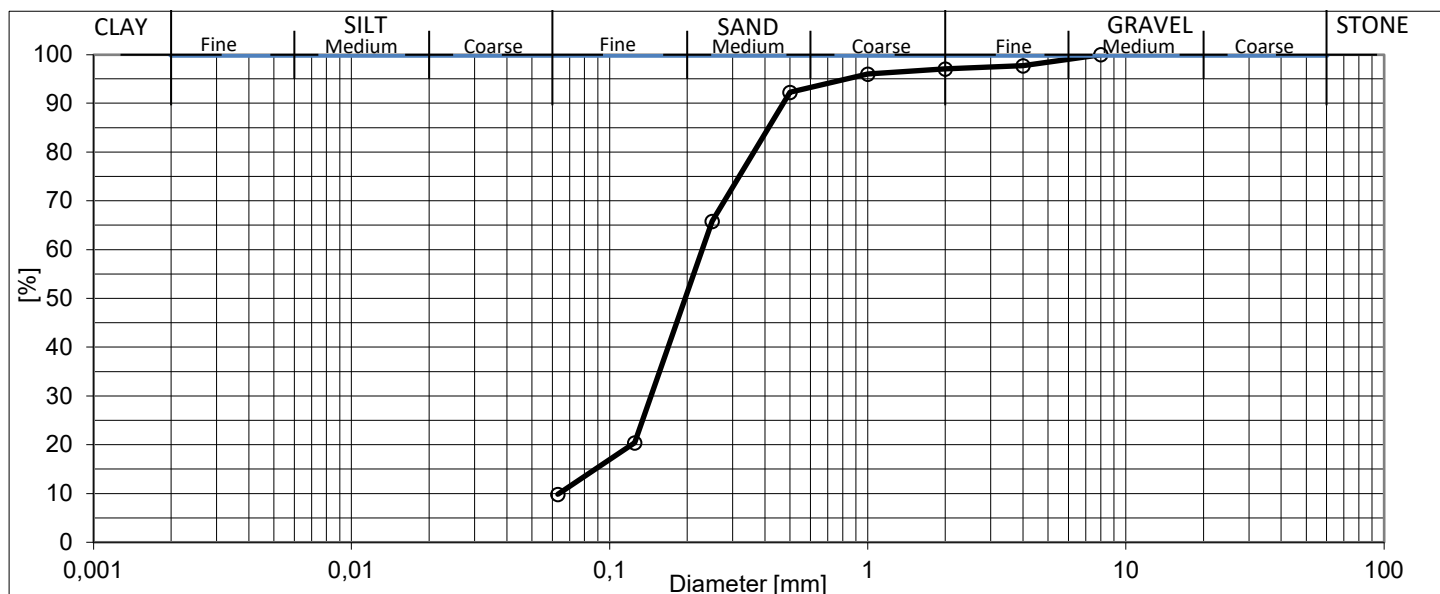
Inspection Section	BH03-S15-7
Sample Description	Sand, fine - medium
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	15. jun 2022

Sieving	
Sieve size [mm]	Passing %
8	100,0
4	97,7
2	97,1
1	96,0
0,5	92,2
0,25	65,8
0,125	20,4
0,063	9,9

Results	
D ₈₅	0,41
D ₆₀	0,23
D ₅₀	0,20
D ₁₅	0,09
D ₁₀	0,06

Coefficient of uniformity	
D ₆₀ /D ₁₀	3,60



Made By: THAND

Checked By: CVZ

Date: 15. jun 2022

Date: 17. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

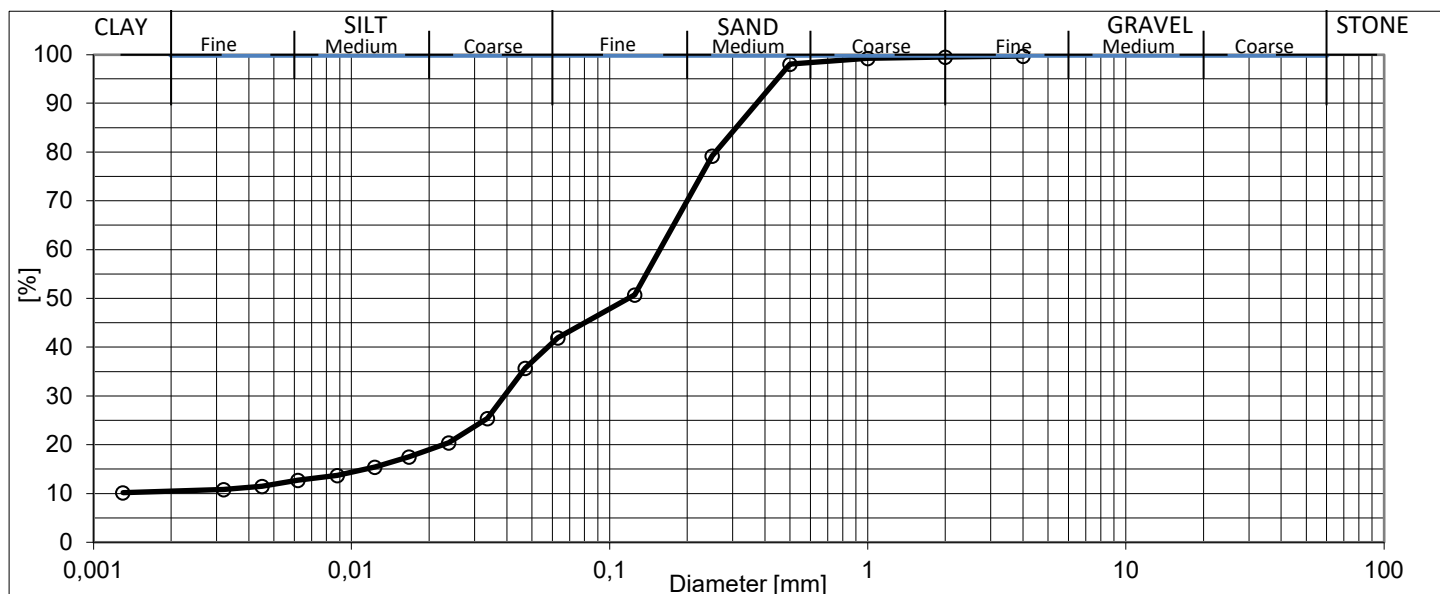
Inspection Section	BH03-S21-10m
Sample Description	Sand, Fine medium
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	15. jun 2022

Sieving	
Sieve size [mm]	Passing %
4	99,7
2	99,5
1	99,2
0,5	98,0
0,25	79,2
0,125	50,7
0,063	41,9
0,0471	35,7
0,0336	25,4
0,0238	20,4
0,0167	17,5
0,0123	15,4
0,0088	13,7
0,0062	12,7
0,0045	11,5
0,0032	10,8
0,0013	10,2

Results	
D ₈₅	0,31
D ₆₀	0,16
D ₅₀	0,12
D ₁₅	0,012
D ₁₀	

Coefficient of uniformity	
D ₆₀ /D ₁₀	



Made By: THAND

Checked By: CVZ

Date: 15. jun 2022

Date: 21. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

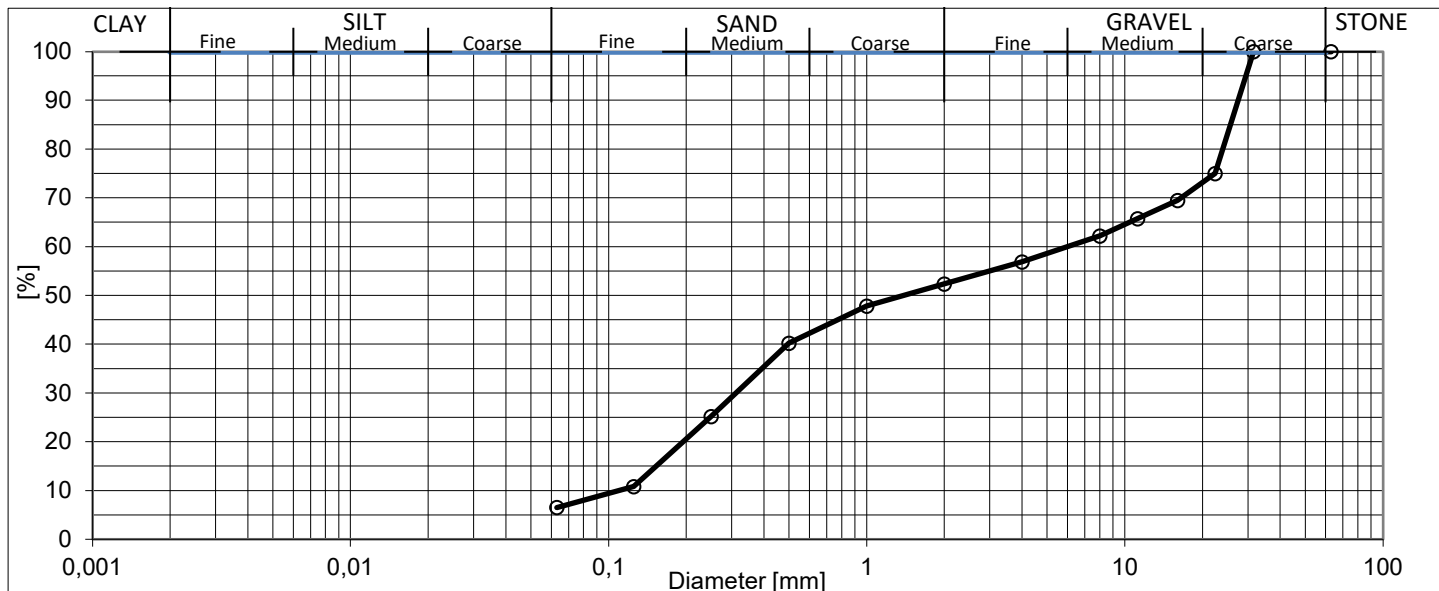
Inspection Section	BH03-S30-15
Sample Description	Sand, medium
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	16. jun 2022

Sieving	
Sieve size [mm]	Passing %
63	100,0
31,5	100,0
22,4	75,0
16	69,5
11,2	65,8
8	62,2
4	56,9
2	52,4
1	47,8
0,5	40,2
0,25	25,2
0,125	10,8
0,063	6,5

Results	
D ₈₅	25,67
D ₆₀	5,98
D ₅₀	1,40
D ₁₅	0,15
D ₁₀	0,11

Coefficient of uniformity	
D ₆₀ /D ₁₀	54,63



Made By: THAND

Checked By: CVZ

Date: / 15-06-2022

Date: 16. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

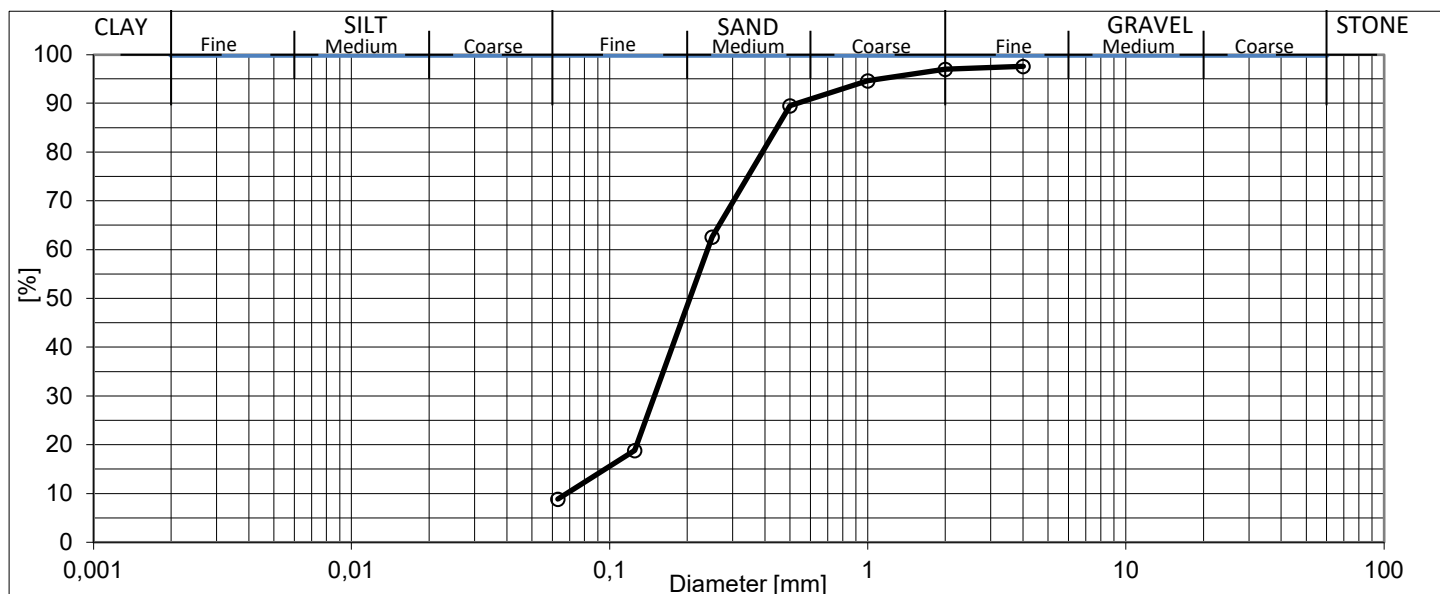
Inspection Section	BH03-S41-20
Sample Description	Sand, fine - medium
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	17. jun 2022

Sieving	
Sieve size [mm]	Passing %
4	97,6
2	97,0
1	94,7
0,5	89,5
0,25	62,6
0,125	18,8
0,063	8,9

Results	
D ₈₅	0,45
D ₆₀	0,24
D ₅₀	0,20
D ₁₅	0,10
D ₁₀	0,07

Coefficient of uniformity	
D ₆₀ /D ₁₀	3,53



Made By: THAND

Checked By: CVZ

Date: 17. jun 2022

Date: 17. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

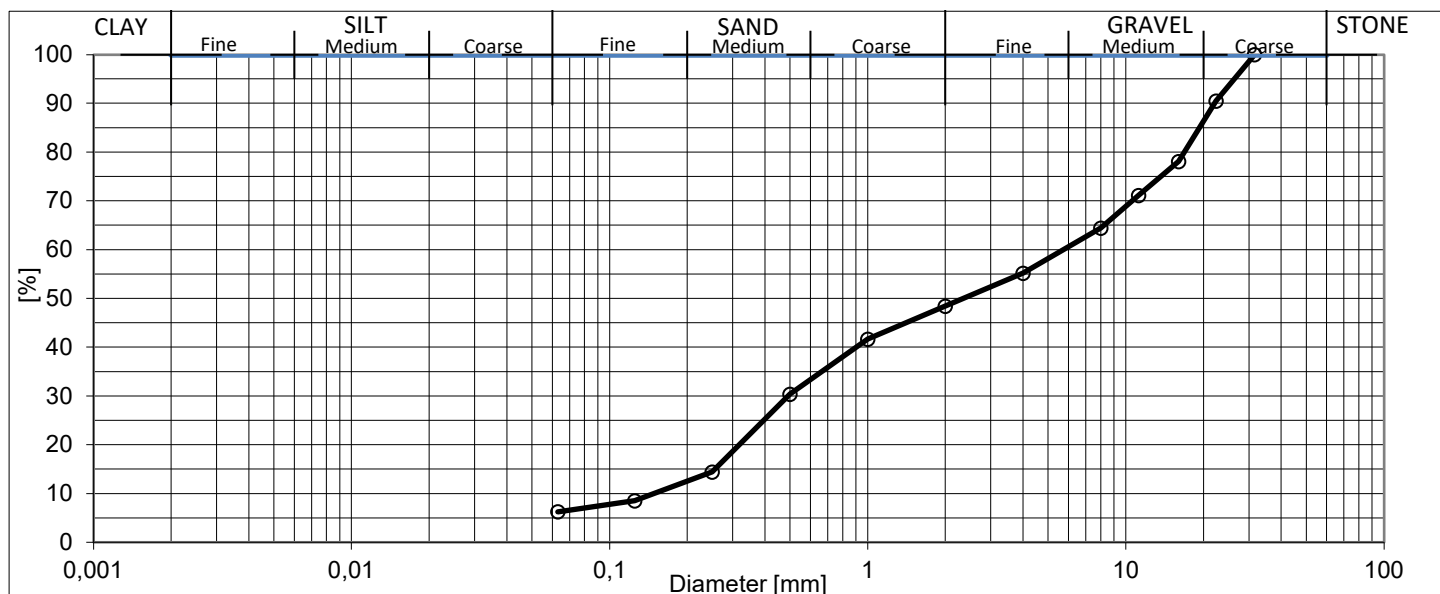
Inspection Section	BH03-S51-25
Sample Description	Sand, medium - coarse
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	14. jun 2022

Sieving	
Sieve size [mm]	Passing %
31,5	100,0
22,4	90,5
16	78,1
11,2	71,1
8	64,4
4	55,2
2	48,4
1	41,7
0,5	30,4
0,25	14,4
0,125	8,5
0,063	6,3

Results	
D ₈₅	19,30
D ₆₀	5,74
D ₅₀	2,35
D ₁₅	0,26
D ₁₀	0,15

Coefficient of uniformity	
D ₆₀ /D ₁₀	38,59



Made By: MALT / THAND

Checked By: CVZ

Date: 14-06 / 16-06-2022

Date: 17. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

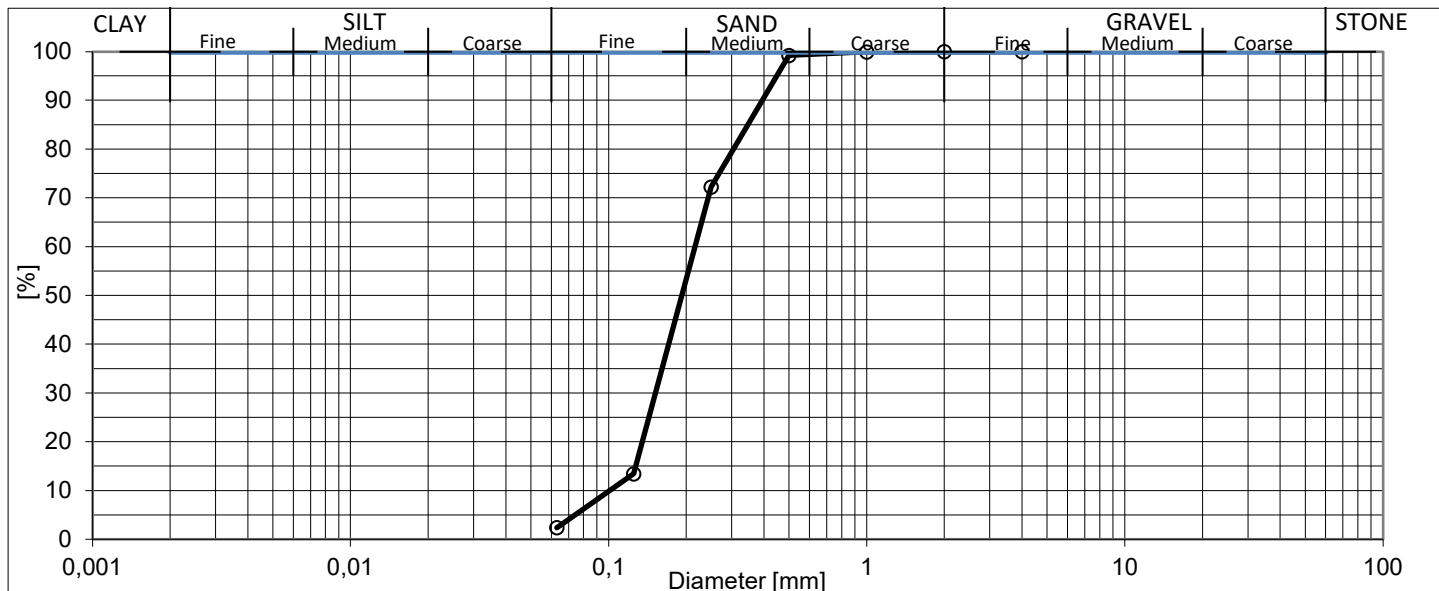
Inspection Section	BH03-S63-31,5
Sample Description	Sand, Fine medium
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	15. jun 2022

Sieving	
Sieve size [mm]	Passing %
4	100,0
2	100,0
1	99,9
0,5	99,2
0,25	72,2
0,125	13,5
0,063	2,4

Results	
D ₈₅	0,35
D ₆₀	0,22
D ₅₀	0,19
D ₁₅	0,13
D ₁₀	0,10

Coefficient of uniformity	
D ₆₀ /D ₁₀	2,15



Made By: THAND

Checked By: CVZ

Date: 15. jun 2022

Date: 16. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

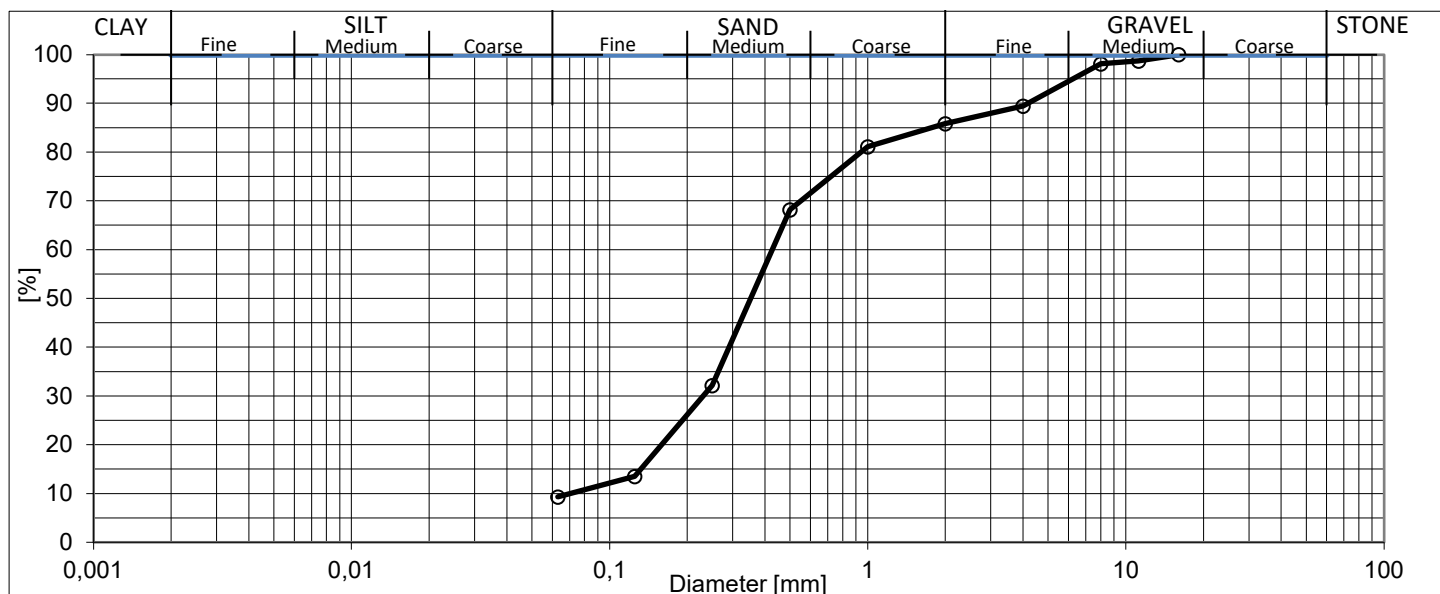
Inspection Section	BH04-S5-2
Sample Description	Sand, fine - medium
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	15. jun 2022

Sieving	
Sieve size [mm]	Passing %
16	100,0
11,2	98,7
8	98,1
4	89,5
2	85,8
1	81,1
0,5	68,2
0,25	32,1
0,125	13,5
0,063	9,3

Results	
D ₈₅	1,77
D ₆₀	0,43
D ₅₀	0,35
D ₁₅	0,13
D ₁₀	0,07

Coefficient of uniformity	
D ₆₀ /D ₁₀	6,10



Made By: THAND

Checked By: CVZ

Date: 15. jun 2022

Date: 17. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

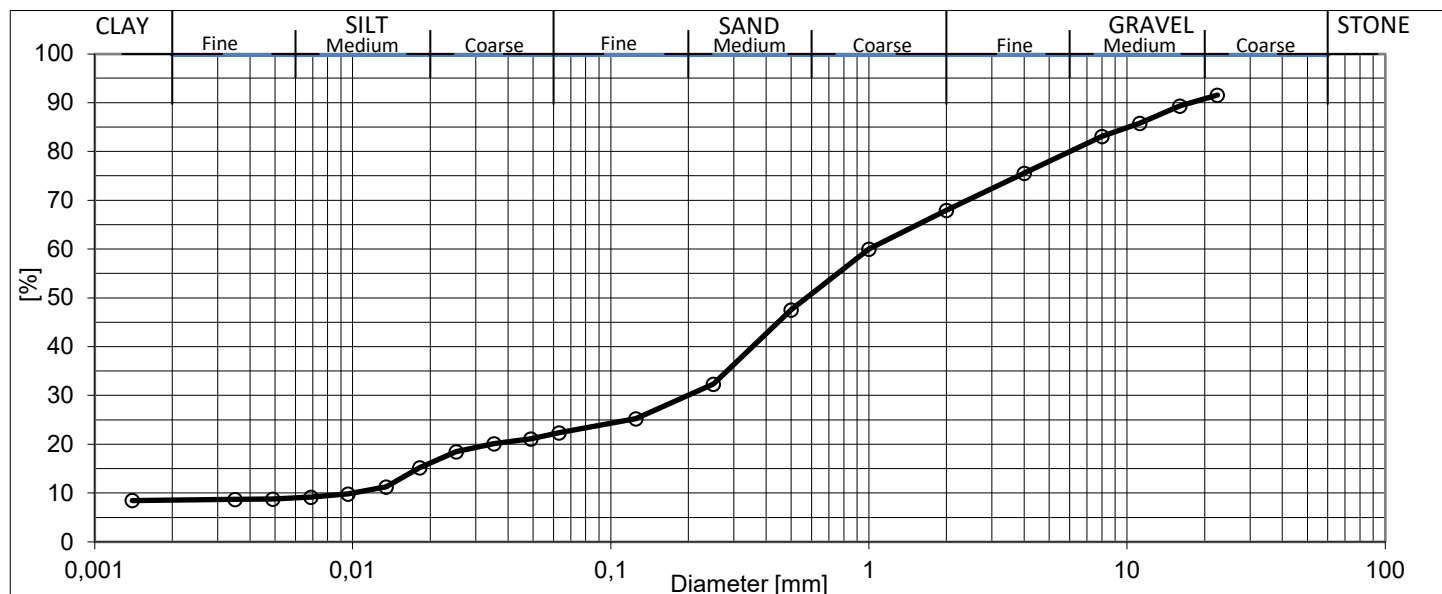
Inspection Section	BH04-S18-8,5
Sample Description	Sand, medium
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	15. jun 2022

Sieving	
Sieve size [mm]	Passing %
22,4	91,6
16	89,3
11,2	85,8
8	83,1
4	75,5
2	68,0
1	60,0
0,5	47,6
0,25	32,3
0,125	25,3
0,063	22,3
0,049	21,1
0,0353	20,1
0,0252	18,5
0,0182	15,2
0,0135	11,3
0,0096	9,8
0,0069	9,2
0,0049	8,8
0,0035	8,7
0,0014	8,5

Results	
D ₈₅	10,17
D ₆₀	1,00
D ₅₀	0,57
D ₁₅	0,018
D ₁₀	0,010

Coefficient of uniformity	
D ₆₀ /D ₁₀	99,96



Made By: THAND

Checked By: CVZ

Date: 15. jun 2022

Date: 22. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

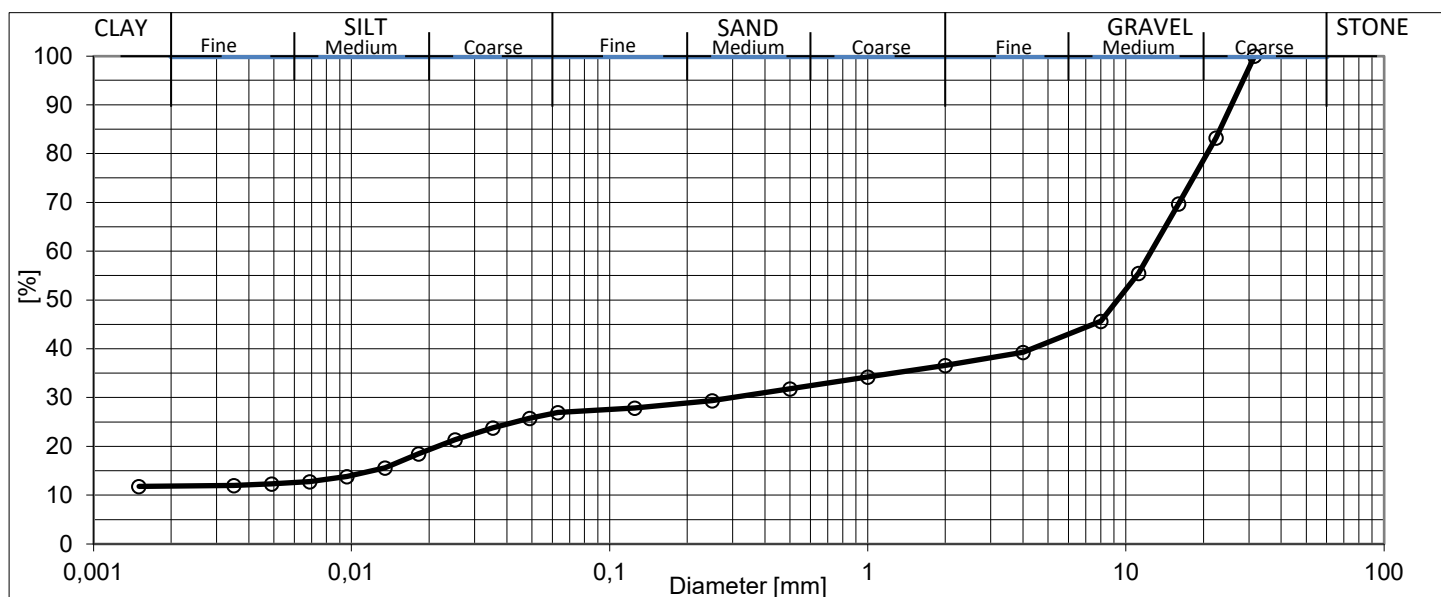
Inspection Section	BH04-S29-14
Sample Description	Sand, medium - coarse
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	15. jun 2022

Sieving	
Sieve size [mm]	Passing %
31,5	100,0
22,4	83,2
16	69,7
11,2	55,5
8	45,7
4	39,3
2	36,6
1	34,3
0,5	31,8
0,25	29,4
0,125	27,8
0,063	26,9
0,049	25,8
0,0353	23,8
0,0252	21,4
0,0182	18,5
0,0135	15,6
0,0096	13,8
0,0069	12,8
0,0049	12,3
0,0035	12,0
0,0015	11,8

Results	
D ₈₅	23,24
D ₆₀	12,54
D ₅₀	9,28
D ₁₅	0,013
D ₁₀	

Coefficient of uniformity	
D ₆₀ /D ₁₀	



Made By: THAND

Checked By: CVZ

Date: 15. jun 2022

Date: 21. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

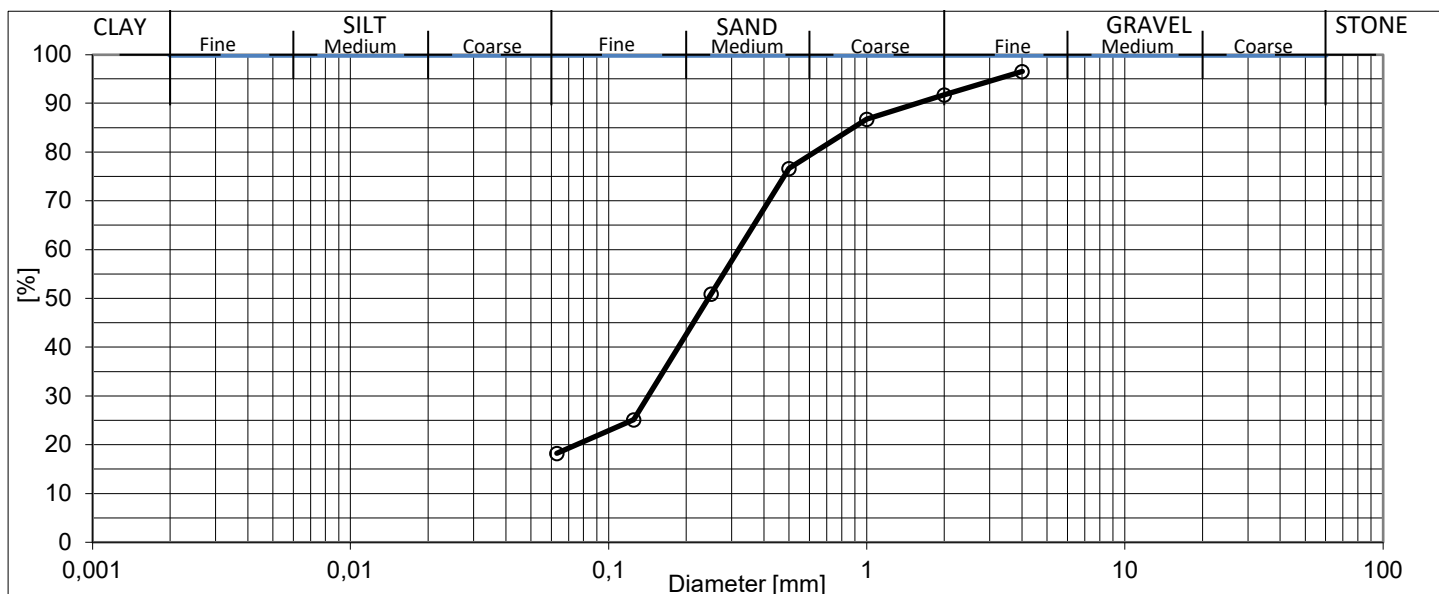
Inspection Section	BH04-S90-44,5
Sample Description	Sand, Fine medium
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	15. jun 2022

Sieving	
Sieve size [mm]	Passing %
4	96,5
2	91,7
1	86,7
0,5	76,7
0,25	50,9
0,125	25,1
0,063	18,2

Results	
D ₈₅	0,89
D ₆₀	0,32
D ₅₀	0,24
D ₁₅	
D ₁₀	

Coefficient of uniformity	
D ₆₀ /D ₁₀	



Made By: THAND

Checked By: CVZ

Date: 15. jun 2022

Date: 16. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

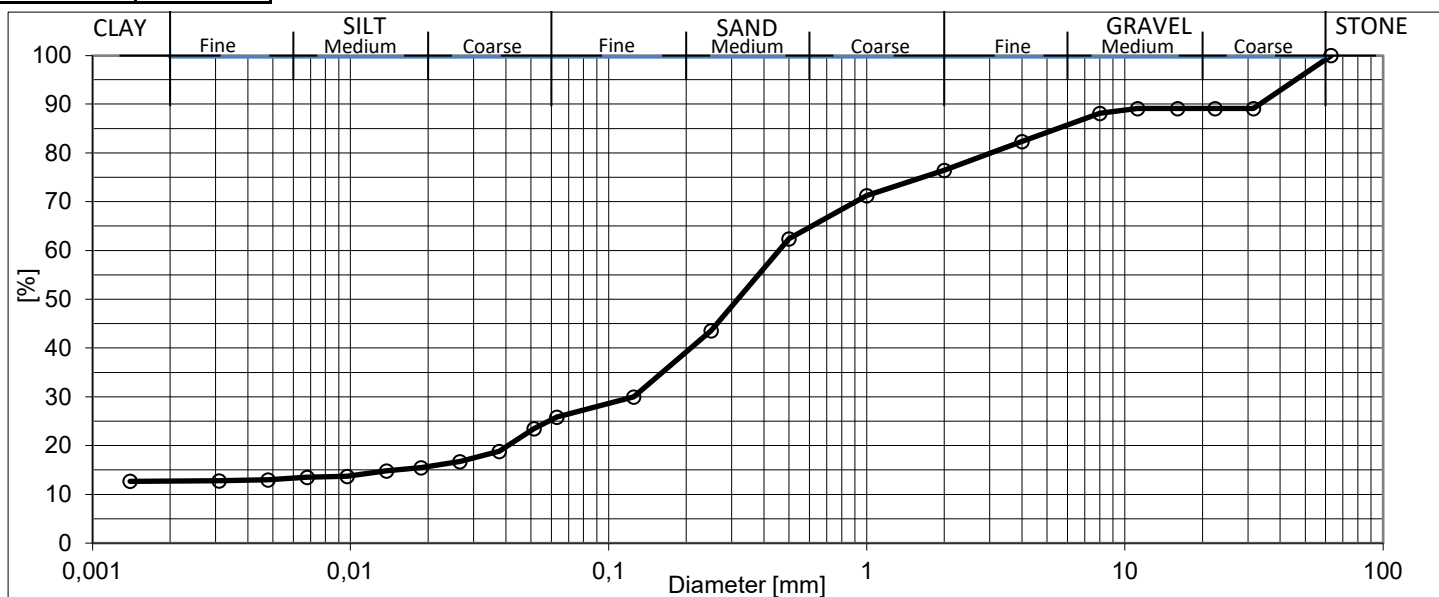
Inspection Section	BH04-S53-26
Sample Description	Sand, Fine medium
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	15. jun 2022

Sieving	
Sieve size [mm]	Passing %
63	100,0
31,5	89,1
22,4	89,1
16	89,1
11,2	89,1
8	88,1
4	82,4
2	76,5
1	71,2
0,5	62,4
0,25	43,6
0,125	30,0
0,063	25,9
0,0514	23,5
0,0377	18,8
0,0265	16,7
0,0188	15,5
0,0138	14,8
0,0097	13,7
0,0068	13,5
0,0048	13,0
0,0031	12,8
0,0014	12,7

Results	
D ₈₅	5,49
D ₆₀	0,46
D ₅₀	0,32
D ₁₅	0,018
D ₁₀	

Coefficient of uniformity	
D ₆₀ /D ₁₀	



Made By: THAND

Checked By: CVZ

Date: 15. jun 2022

Date: 22. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

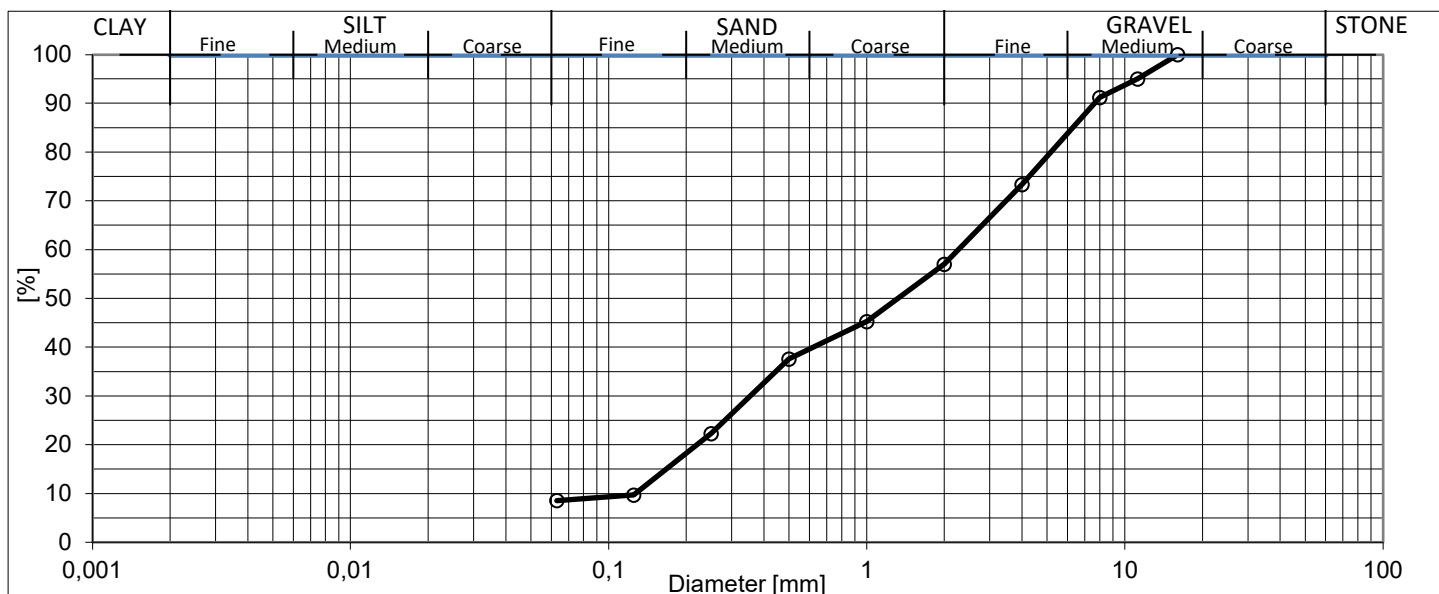
Inspection Section	BH04-S64-31,5
Sample Description	Sand, medium - coarse
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	15. jun 2022

Sieving	
Sieve size [mm]	Passing %
16	100,0
11,2	95,0
8	91,2
4	73,4
2	57,0
1	45,2
0,5	37,6
0,25	22,3
0,125	9,7
0,063	8,6

Results	
D ₈₅	6,29
D ₆₀	2,27
D ₅₀	1,32
D ₁₅	0,17
D ₁₀	0,13

Coefficient of uniformity	
D ₆₀ /D ₁₀	17,87



Made By: THAND

Checked By: CVZ

Date: 15. jun 2022

Date: 16. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

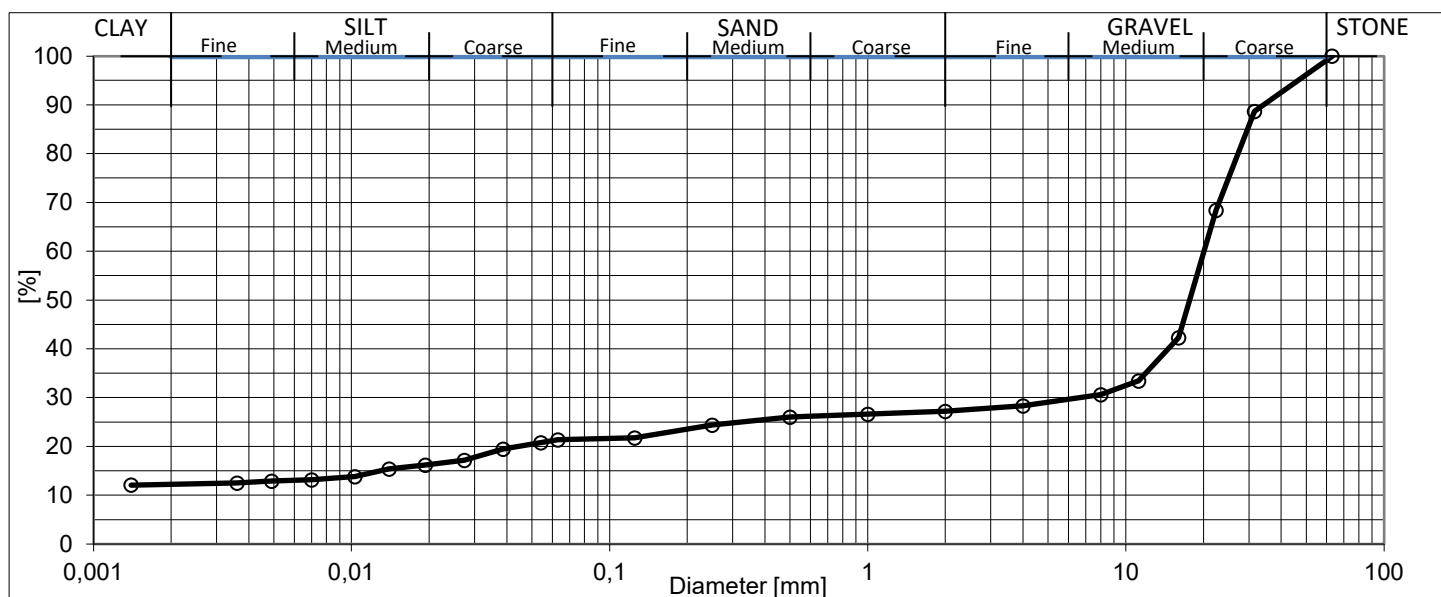
Inspection Section	BH04-S73-36
Sample Description	Gravel, sandy
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	16. jun 2022

Sieving	
Sieve size [mm]	Passing %
63	100,0
31,5	88,7
22,4	68,4
16	42,3
11,2	33,5
8	30,6
4	28,4
2	27,2
1	26,6
0,5	26,1
0,25	24,4
0,125	21,8
0,063	21,4
0,0541	20,8
0,0387	19,5
0,0274	17,2
0,0193	16,2
0,014	15,4
0,0103	13,8
0,007	13,2
0,0049	12,9
0,0036	12,5
0,0014	12,1

Results	
D ₈₅	29,61
D ₆₀	20,10
D ₅₀	17,67
D ₁₅	0,013
D ₁₀	

Coefficient of uniformity	
D ₆₀ /D ₁₀	



Made By: THAND

Checked By: CVZ

Date: 16. jun 2022

Date: 22. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

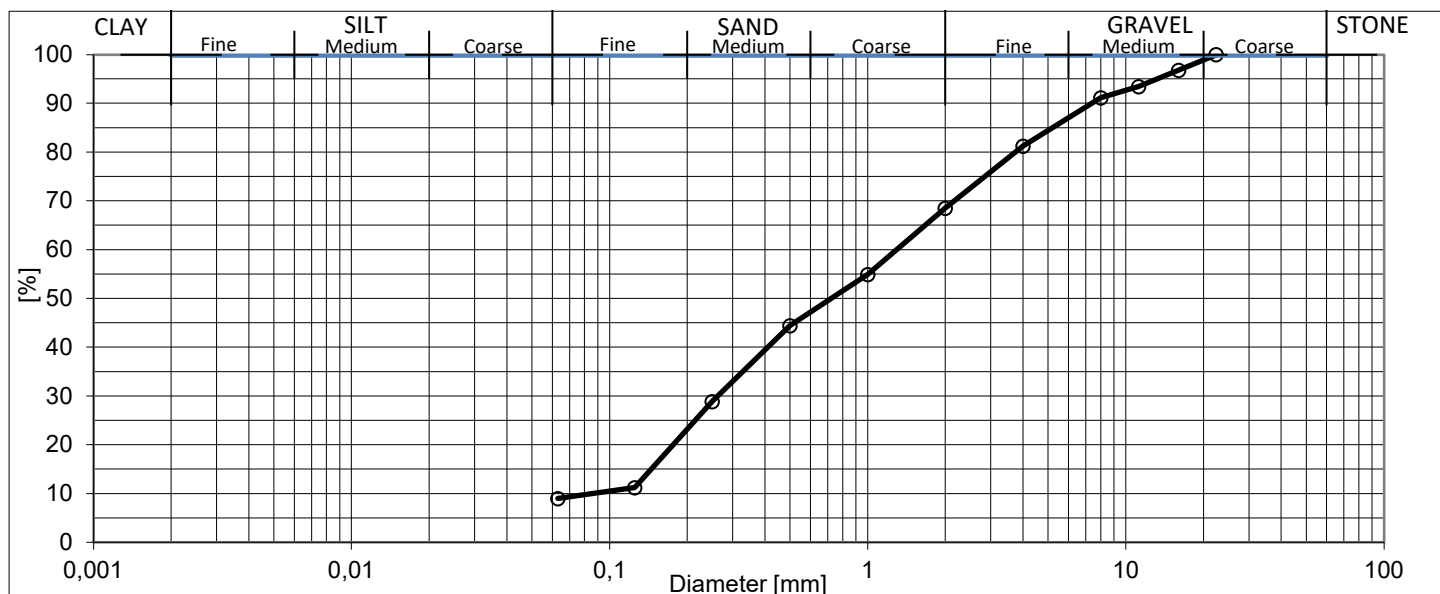
Inspection Section	BH04-S80-39,5
Sample Description	Sand, medium - coarse
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	15. jun 2022

Sieving	
Sieve size [mm]	Passing %
22,4	100,0
16	96,8
11,2	93,5
8	91,2
4	81,2
2	68,5
1	54,9
0,5	44,4
0,25	28,9
0,125	11,2
0,063	9,0

Results	
D ₈₅	5,20
D ₆₀	1,30
D ₅₀	0,72
D ₁₅	0,14
D ₁₀	0,09

Coefficient of uniformity	
D ₆₀ /D ₁₀	15,14



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Checked By: CVZ

Date: 15. jun 2022

Date: 17. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

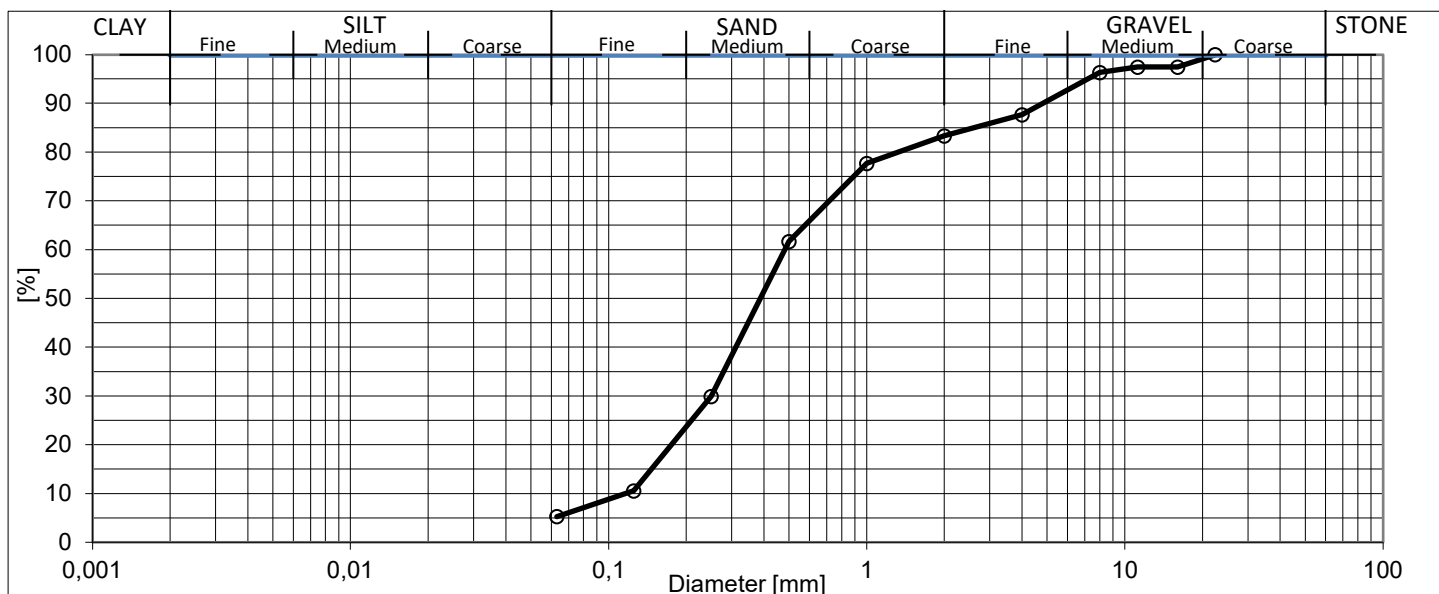
Inspection Section	BH04-S90-44,5
Sample Description	Sand, Fine medium
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	15. jun 2022

Sieving	
Sieve size [mm]	Passing %
22,4	100,0
16	97,4
11,2	97,4
8	96,3
4	87,7
2	83,3
1	77,7
0,5	61,7
0,25	29,9
0,125	10,5
0,063	5,3

Results	
D ₈₅	2,61
D ₆₀	0,48
D ₅₀	0,39
D ₁₅	0,15
D ₁₀	0,12

Coefficient of uniformity	
D ₆₀ /D ₁₀	4,13



Made By: THAND

Checked By: CVZ

Date: 15. jun 2022

Date: 16. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

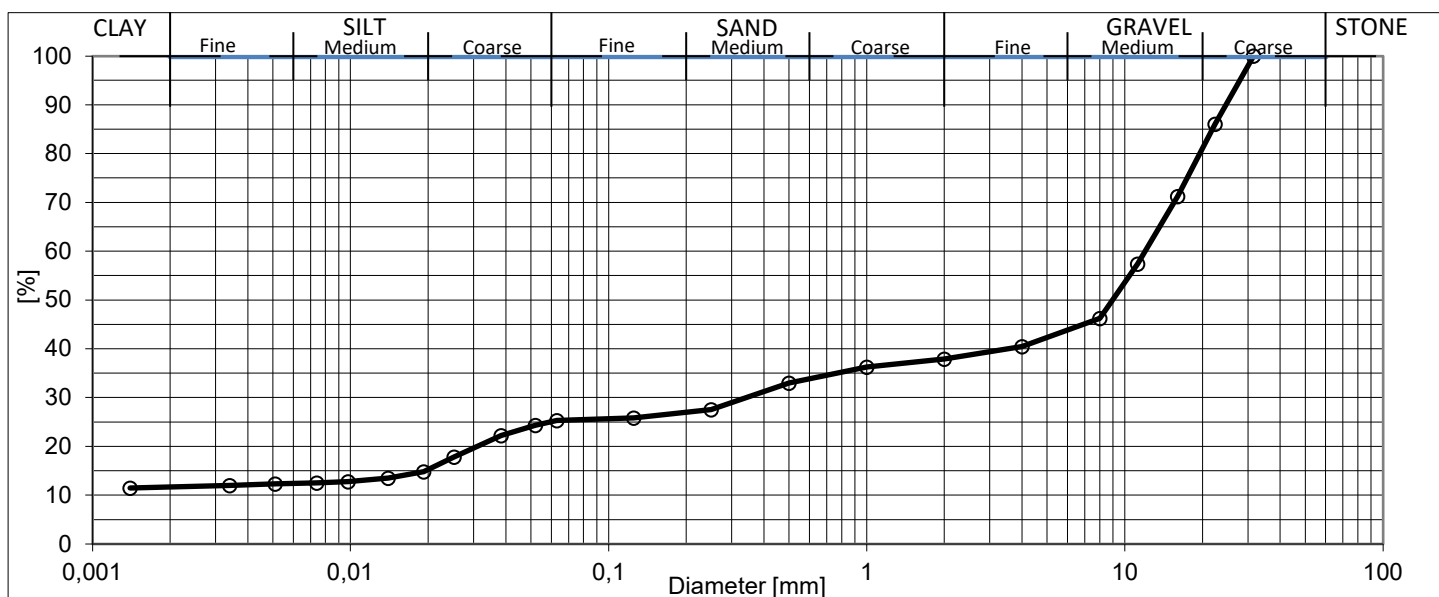
Inspection Section	BH04-S95-47
Sample Description	Gravel
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	15. jun 2022

Sieving	
Sieve size [mm]	Passing %
31,5	100,0
22,4	86,0
16	71,2
11,2	57,4
8	46,2
4	40,5
2	37,9
1	36,2
0,5	33,0
0,25	27,5
0,125	25,8
0,063	25,3
0,052	24,3
0,0383	22,2
0,0252	17,8
0,0192	14,8
0,014	13,5
0,0098	12,8
0,0074	12,5
0,0051	12,3
0,0034	12,0
0,0014	11,5

Results	
D ₈₅	21,88
D ₆₀	11,98
D ₅₀	8,96
D ₁₅	0,02
D ₁₀	

Coefficient of uniformity	
D ₆₀ /D ₁₀	



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Checked By: CVZ

Date: 15. jun 2022

Date: 22. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

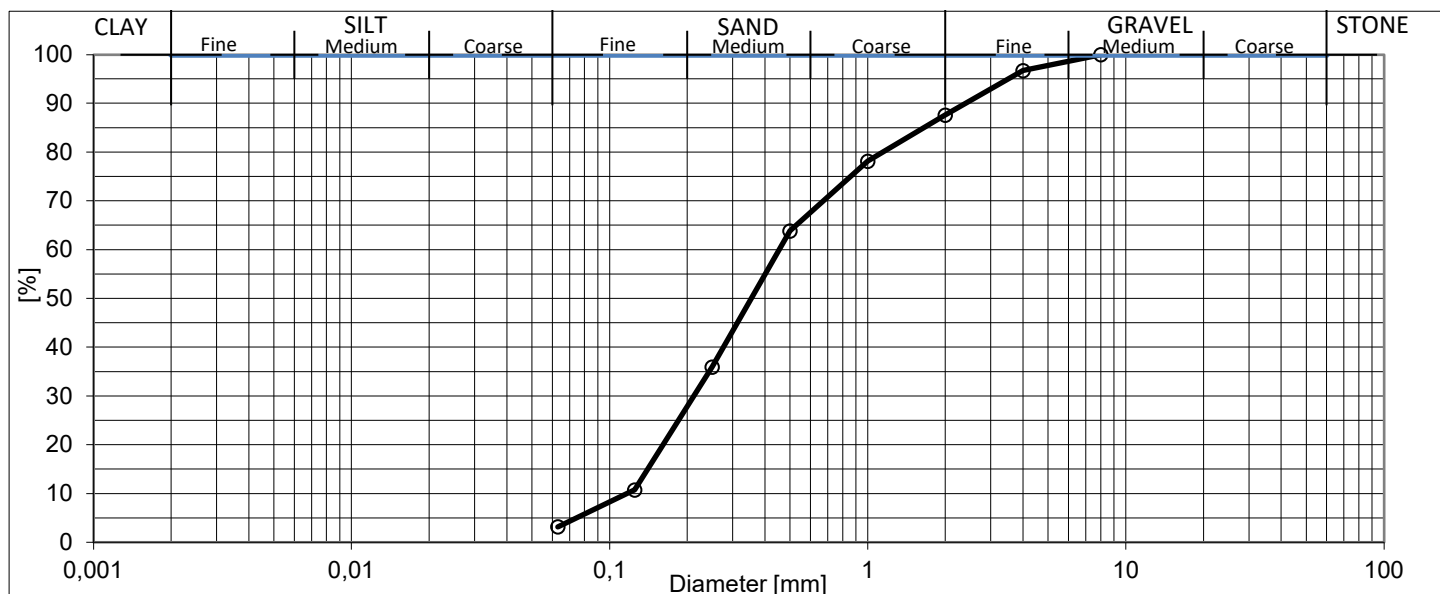
Inspection Section	BH05-S11-5
Sample Description	Sand, medium - coarse
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	17. jun 2022

Sieving	
Sieve size [mm]	Passing %
8	100,0
4	96,7
2	87,6
1	78,1
0,5	63,8
0,25	35,9
0,125	10,8
0,063	3,2

Results	
D ₈₅	1,65
D ₆₀	0,45
D ₅₀	0,35
D ₁₅	0,14
D ₁₀	0,12

Coefficient of uniformity	
D ₆₀ /D ₁₀	3,90



Made By: THAND

Checked By: CVZ

Date: 17. jun 2022

Date: 17. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

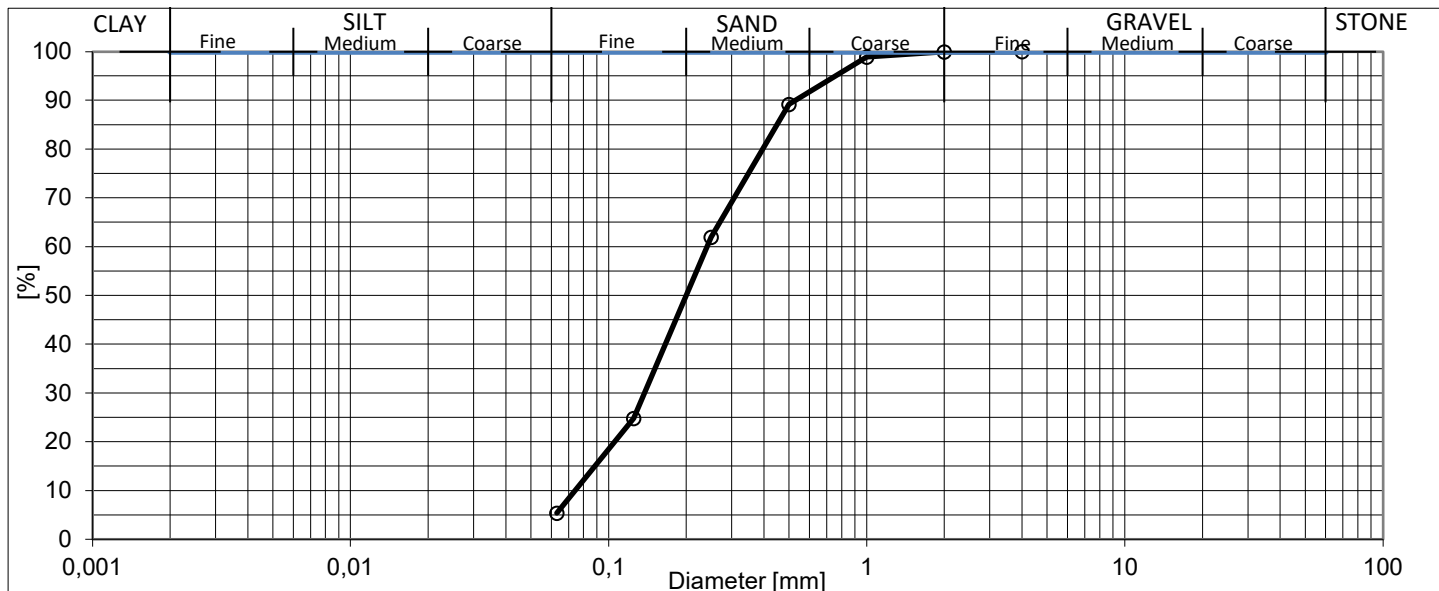
Inspection Section	BH05-S21-10
Sample Description	Sand, medium
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	17. jun 2022

Sieving	
Sieve size [mm]	Passing %
4	100,0
2	99,9
1	98,9
0,5	89,2
0,25	61,9
0,125	24,8
0,063	5,4

Results	
D ₈₅	0,45
D ₆₀	0,24
D ₅₀	0,20
D ₁₅	0,09
D ₁₀	0,07

Coefficient of uniformity	
D ₆₀ /D ₁₀	3,25



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Date: 17. jun 2022

Date: 17. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

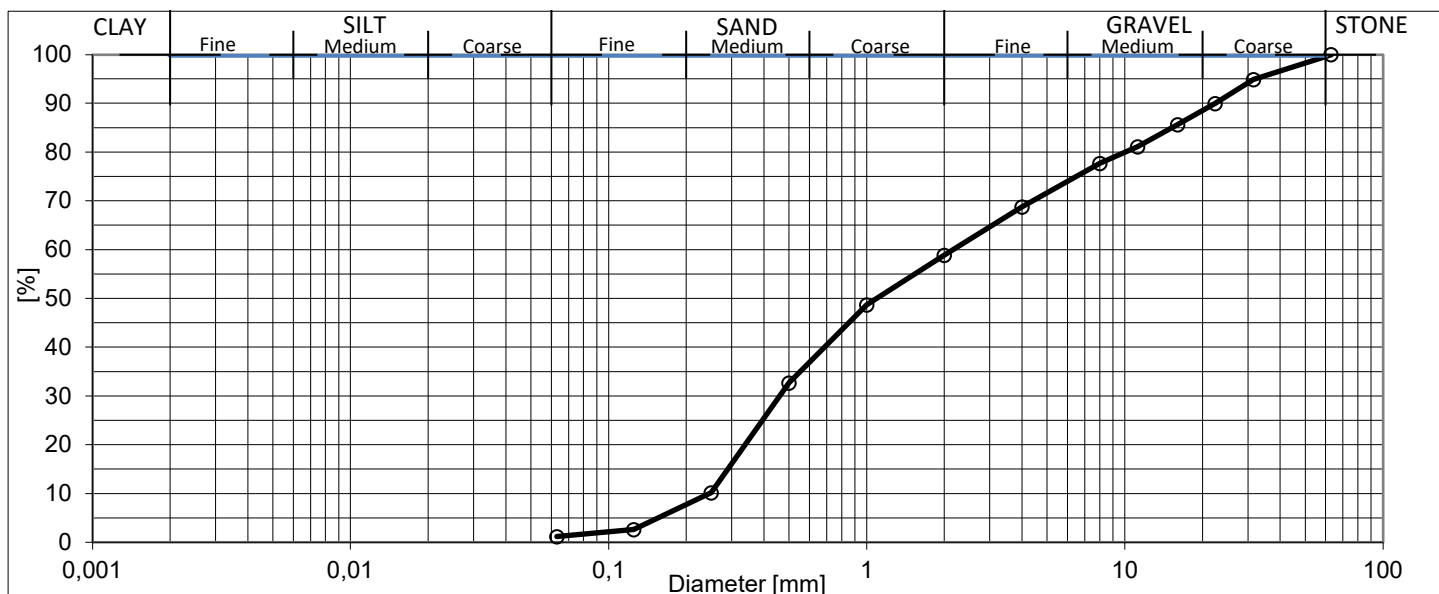
Inspection Section	BH05-S31-15
Sample Description	Sand, coarse
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	20. jun 2022

Sieving	
Sieve size [mm]	Passing %
63	100,0
31,5	94,9
22,4	90,0
16	85,6
11,2	81,1
8	77,7
4	68,8
2	58,9
1	48,7
0,5	32,7
0,25	10,2
0,125	2,6
0,063	1,2

Results	
D ₈₅	15,24
D ₆₀	2,16
D ₅₀	1,09
D ₁₅	0,29
D ₁₀	0,25

Coefficient of uniformity	
D ₆₀ /D ₁₀	8,80



Made By: THAND

Checked By: CVZ

Date: 20. jun 2022

Date: 20. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

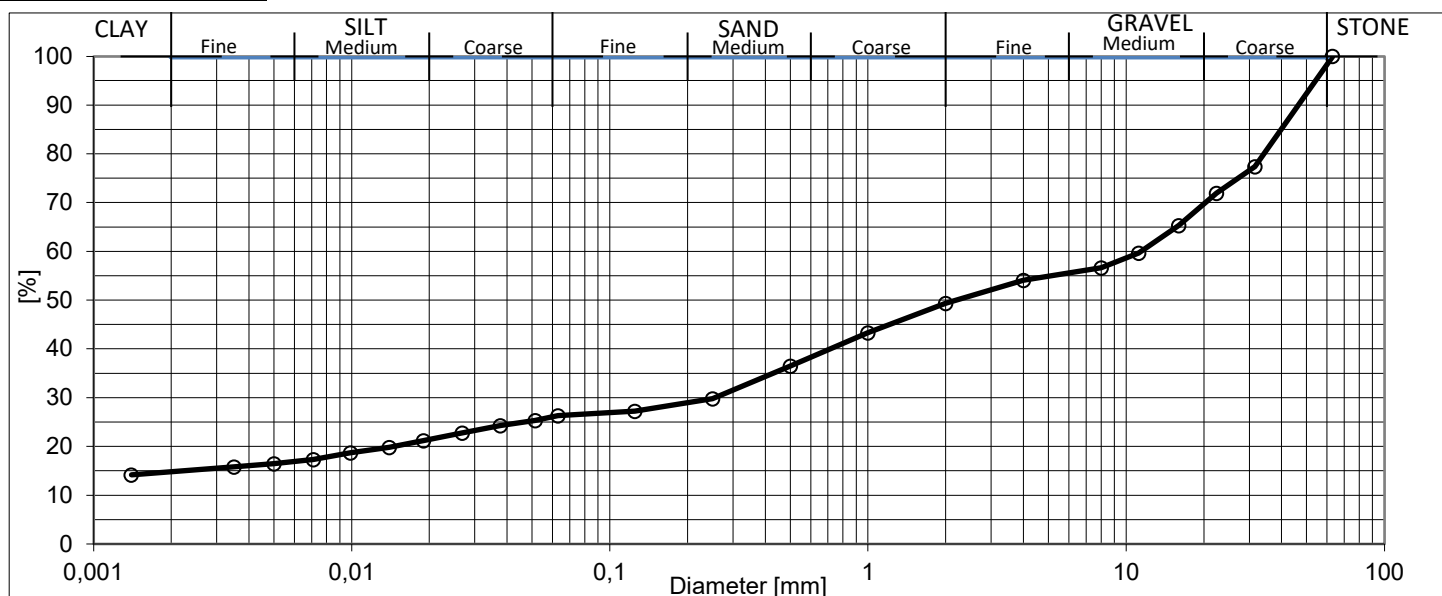
Inspection Section	BH05-S41-20
Sample Description	Sand, medium - coarse
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	17. jun 2022

Sieving	
Sieve size [mm]	Passing %
63	100,0
31,5	77,4
22,4	71,9
16	65,3
11,2	59,7
8	56,6
4	54,1
2	49,4
1	43,3
0,5	36,5
0,25	29,8
0,125	27,2
0,063	26,3
0,0514	25,3
0,0377	24,3
0,0268	22,8
0,019	21,2
0,014	19,8
0,0099	18,7
0,0071	17,3
0,005	16,5
0,0035	15,8
0,0014	14,2

Results	
D ₈₅	39,81
D ₆₀	11,44
D ₅₀	2,19
D ₁₅	0,03
D ₁₀	

Coefficient of uniformity	
D ₆₀ /D ₁₀	



Made By: THME

Checked By: CVZ

Date: 17. jun 2022

Date: 21. jun 2022

PER AARSLEFF A/S Laboratorium

TEST METHODS: DS/EN 933-1, DS/EN 933-9, DS/EN 1744-1, prVI 99-11



AARSLEFF

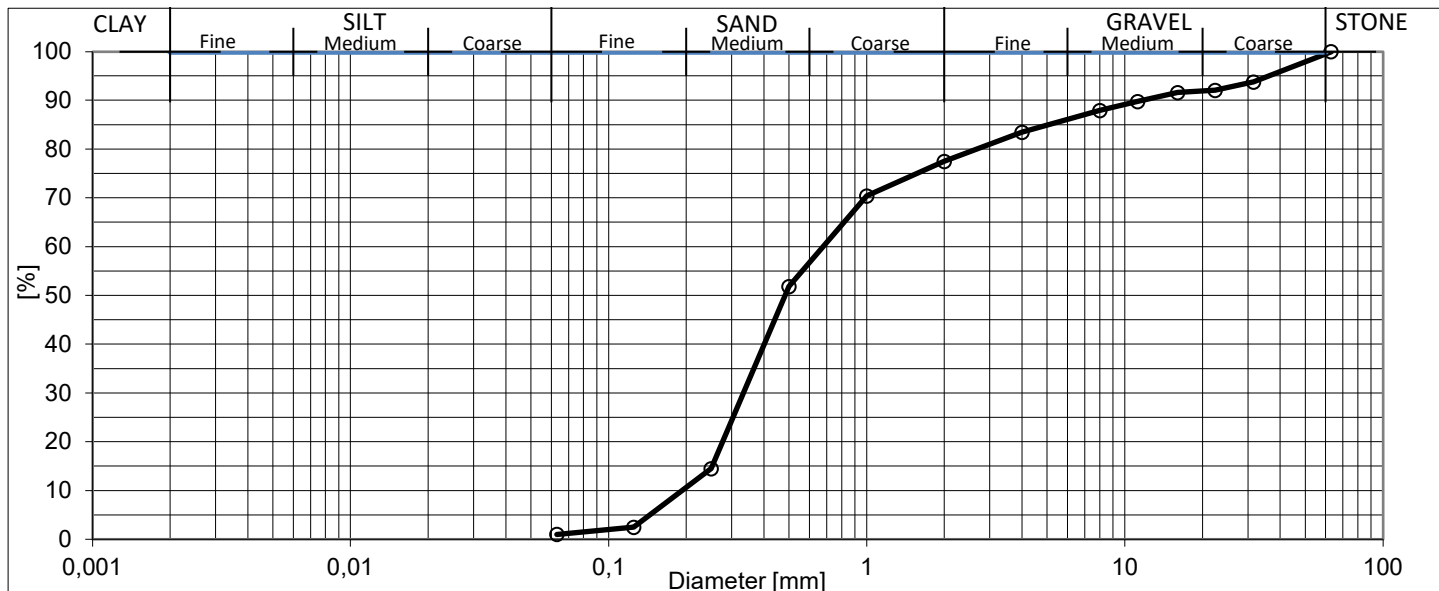
Inspection Section	BH05-S51-25
Sample Description	Sand, fine-medium
Location	Gilbjerg Hoved

Lab Number	
Job Number	908091-1100051481
Date Sampled	20. jun 2022

Sieving	
Sieve size [mm]	Passing %
63	100,0
31,5	93,8
22,4	92,1
16	91,6
11,2	89,7
8	87,9
4	83,5
2	77,5
1	70,4
0,5	51,8
0,25	14,5
0,125	2,5
0,063	1,0

Results	
D ₈₅	5,08
D ₆₀	0,68
D ₅₀	0,48
D ₁₅	0,25
D ₁₀	0,19

Coefficient of uniformity	
D ₆₀ /D ₁₀	3,52



Made By: THAND

Checked By: CVZ

Date: 20. jun 2022

Date: 20. jun 2022

APPENDIX 6.1-6.5 – FIELD LOGS

Sag: 232193-281	DGU-nr:	Kote: Terrain	Init.: H-PB	Dato: 17 / 5 / 22
Boring: BH01	Lok.: Lilleløje	Bundpejl: 25,0m	Vandspejl: 15,60	Side: 1 a 5
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 6"	Filterdim.: 225	Slidsestr.:	Sandstr.: 3

Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Notater	
over terræn	Dybde m.	Prøve	Prøve- nr.:	Lag- grænse		Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm	Fore rør	Dybde af: forgravning/ udtagne miljøprøver/ fræsning (fra/til)/ omrigning til DTH
	20		1		muld Sand Sort								
	40												
	60		2										
	80			0,70									
	100		3		Sand								
	20												
	40												
	60		4										
	80			1,80									
	100		5		Leofuld is agger sandet Fugly								
	20						5	10	2				
	40						5	19	4				
	60		6										
	80												
	100		7										
	20				ml-Sandet Brunen Tdr		5	45	18				
	40						5	10	4				
	60		8										
	80												
	100		9										
	20						4	48	17				
	40						4	7	4			Vær Lille Tryk Lab	
	60		10										
	80												
	100		11	60	Stop POSE prøve								
	20						4	27	10				
	40						4	10	4				
	60		12										
	80												
	100		13										

Sag: 232193-281	DGU-nr:	Kote: Terrain	Init.: R7-PB	Dato: 17 / 5 / 22
Boring: B101	Lok.: Lilleby	Bundpejl:	Vandspejl:	Side: 2 a 5
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 60	Filterdim.:	Slidsestr.:	Sandstr.: 3

Pejlerør	Dybde m.	Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Fore rør	Notater
		Prøve nr.:	Lag- grænse			Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm		
	20				grub sten	20	4	1/2	1/2				Venlig Tegning
	40					40							
	60	14				60							
	80					80							
	100	15			Do	100							
	20					20				7			Lilleby sand
	40					40				10			100 mm d. 20
	60	16				60				10			
	80					80				13			
	100	17			Do	100							
	20					20							
	40					40							
	60	18				60				14			100 mm d. 20
	80					80				11			100 mm d. 20
	100	19			Do	100				18			100 mm d. 20
	20					20				21			
	40					40				17			
	60	20				60							
	80					80							
	100	21			100 stor pose p. 40	100							Lilleby sand
	20					20				27			100 mm d. 20
	40					40				11			100 mm d. 20
	60	22				60				11			
	80					80							
	100	23			100 Blandt	100							
	20					20							
	40					40							
	60	24				60							Lilleby sand
	80					80							
	100	25			100	100							

Sag: 132 AS-281	DGU-nr:	Kote: Terrain	Init.: RJ-13	Dato: 17 / 5 / 22
Boring: BH01	Lok.: Lillebje	Bundpejl:	Vandspejl:	Side: 3 a 5
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 6"	Filterdim.:	Slidsestr.:	Sandstr.: 3

Pejlerør	Dybde m.	Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Fore rør	Notater
		Prøve nr.:	Prøve- nr.:	Lag- grænse		Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm		
over terræn													
	20				Sand - sten 10%	20							
	40					40							
	60		26			60							
	80					80							
	100		27		Do	100							fulled sand
	120					120				17,6			Intra m. 11,5
	140					140				29,32			mangler 6cm
	160		28			160				31,8			mangler 8cm
	180					180							
	200		29		lyst ud af marken	200							
	220				116 ³⁰ skal sæt	220							
	240		30			240							fulled sand
	260					260				8,9			intra m. 11,5
	280					280				11,2			
	300		31		stor pose p. 10%	300				11,0			
	320				- VF	320							
	340		32			340							
	360					360							
	380		33		Do	380							fulled sand
	400					400				11,4			intra m. 11,5
	420					420				6,11			
	440		34			440				3,3			
	460					460							
	480					480							
	500		35		Do	500							
	520					520							
	540					540							
	560		36			560							fulled sand
	580					580							intra m. 11,5
	600		37		Do	600							

Sund 3

AARSLEFF

Sag: 237193-281	DGU-nr:	Kote: Ferron	Init.: R3. PB	Dato: 17 / 5 / 22
Boring: B101	Lok.: Lillelejs	Bundpejl:	Vandspejl:	Side: 4 a 5
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 6"	Filterdim.:	Slidsestr.:	Sandstr.: 3

Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Fore rør	Notater
over terræn	Dybde m.	Prøve nr.	Prøve-nr.	Lag-grænse		Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antalslag pr. 7,5 cm		
	20				Sand - sten - grå VF	20							
	40					40							
	60		38		- Sten	60							
	80					80							
	100		39			100							lublet sand inramning
	20					20							
	40		40			40							
	60					60							
	80					80							
	100		41	200	stor rose prøve	100							
	20					20							
	40		42			40							lublet sand inramning
	60					60				56			
	80					80				89			
	100		43		sand grå	100				14			
	20					20				14			
	40		44			40							
	60					60							
	80				Do	80							
	100		45			100							lublet sand inramning
	20					20				44			
	40		46		Do	40				53			
	60					60				66			
	80					80							
	100		47			100							
	20					20							
	40		48		Do	40							
	60					60							
	80					80							
	100		49			100							

Sag: 732193-291	DGU-nr:	Kote: Terrain	Init.: R7-P0	Dato: 17 / 5 / 22
Boring: B101	Lok.: Lilleleje	Bundpejl:	Vandspejl:	Side: 5 a 5
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 6"	Filterdim.:	Slidsestr.:	Sandstr.: 3

Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Notater	
over terræn	Dybde m.	Prøve nr.	Prøve- nr.	Lag- grænse		Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm	Fore rør	Dybde af: forgravning/ udtagne miljøprøver/ fræsning (fra/til)/ omrigning til DTH
	20				Sand - sten gra	20							
	40					40							
	60		50			60							
	80					80							
	00		51		stor pose prøve 25,0m	00							
	20					20							
	40					40							
	60					60							
	80					80							
	00					00							
	20					20							
	40					40							
	60					60							
	80					80							
	00					00							
	20					20							
	40					40							
	60					60							
	80					80							
	00					00							
	20					20							
	40					40							
	60					60							
	80					80							
	00					00							

232193281

Sag: <i>200193281</i>	DGU-nr:	Kote: <i>Terræn</i>	Init.: <i>V18-PB</i>	Dato: <i>3 / 5 / 22</i>
Boring: <i>B1102</i>	Lok.: <i>g. Kildevej</i>	Bundpejl: <i>24,20</i>	Vandspejl: <i>18,62</i>	Side: <i>1 a 5</i>
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: <i>6"</i>	Filterdim.: <i>Ø25</i>	Slidsestr.:	Sandstr.: <i>3</i>

Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Notater
over terræn	Dybde m.	Prøve	Prøve- nr.:	Lag- grænse		Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm	
	20		1		<i>muld Javel SpM</i>	20						<i>Forground 1,5 ↓ Man ikke trykkes</i>
	40											
	60		2	<i>etc</i>								
	80				<i>Sand lgr gul</i>							
	100		3									
	20											
	40		4									
	60			<i>170</i>	<i>ber Eglid</i>							
	80		5									
	100				<i>STEIN SAND GRUS</i>	20	<i>4 max 7,1</i>					
	20		6			40	<i>4 7,1 7,1</i>					
	40											
	60		7		<i>Do</i>							
	80											
	100		8									
	20											
	40		9									
	60											
	80		10									
	100											
	20		11		<i>stor pose</i>	50						
	40											
	60		12									
	80											
	100		13		<i>Do</i>							

Sag: 175-281 232-4114 148-95	DGU-nr:	Kote: Terrain	Init.: 018-03	Dato: 3 / 5 / 22
Boring: BHo2	Lok.: Gilleleje	Bundpejl:	Vandspejl:	Side: 2 a 5
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 6"	Filterdim.:	Slidsestr.:	Sandstr.:

Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Notater
over terræn	Dybde m.	Prøve	Prøve- nr.:	Lag- grænse		Dybde m.	vinge kg	intakt kg	omrør kg	de	antal slag pr. 7,5 cm	
	20				Sten sand g-45	20					15	
	40		14			40					11	
	60					60					97	
	80					80						
	100		15		Do	100						
	120					120						
	140		16			140						
	160					160						
	180					180						
	200		17			200						
	220				SAND 646	220						
	240		18			240						
	260					260						
	280					280						
	300		19			300						
	320				SAND 9200 6403	320						
	340					340						
	360		20			360						
	380					380						
	400		21		Stor porøs sand	400						
	420					420						
	440					440						
	460		22			460						
	480				Do	480						
	500		23			500						
	520					520						
	540		24			540						
	560					560						
	580					580						
	600		25		Do	600						

Sag: 195-101 227 WPM 1000	DGU-nr:	Kote: Terræn	Init.: W13 - FB	Dato: 3 / 5 / 22
Boring: R1102	Lok.: Gilleleje	Bundpejl:	Vandspejl:	Side: 3 a
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 6"	Filterdim.:	Slidestr.:	Sandstr.: 3

Pejlerør	Dybde m.	Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Fore rør	Notater
		Prøve nr.:	Lag- grænse			Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm		
over terræn													
	20												
	40												
	60	26			Do								
	80												
	100	27											
	20				Do								
	40												
	60	28											
	80												
	100	29			Fract. Fra 14.10 - 14.20 Sand 12.10 - 12.20								
	20												
	40												
	60	30											
	80												
	100	31			Stok 10.30								
	20												
	40												
	60	32											
	80												
	100	33			Fract. Fra 16.10 - 16.30 16.10								
	20												
	40												
	60	34											
	80												
	100	35											
	20				Fract. Fra 17.30								
	40												
	60	36											
	80												
	100	37											

Sag: 193-281 23200000000000000000	DGU-nr:	Kote: Terrain	Init.: V13-PB	Dato: 3 / 5 / 22
Boring: B102	Lok.: Gilleleje	Bundpejl:	Vandspejl:	Side: 4 a 5
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 6"	Filterdim.:	Slidsestr.:	Sandstr.:

Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Notater	
over terræn	Dybde m.	Prøve	Prøve- nr.:	Lag- grænse		Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm	Fore rør	Dybde af: forgravning/ udtagne miljøprøver/ fræsning (fra/til)/ omrigning til DTH
	20				Sten - grus - 7gr	20				59			
	40		38			40				126			
	60					60				196			
	80					80				22			
	100		39			100							
	20					20							
	40					40							
	60		40		Sten - grus: 7gr VF	60				42		Udtaget miljøprøve inert 11/13	
	80					80				60			
	100		41		Stor pose	100				78			
	20					20							
	40					40							
	60		42			60							
	80					80							
	100		43		Do	100						Udtaget miljøprøve inert 11/13	
	20					20				70			
	40					40				107			
	60		44			60				148			
	80					80							
	100		45		Lo	100							
	20					20							
	40					40							
	60		46		Sand - 7gr	60						Udtaget miljøprøve inert 11/13	
	80					80							
	100		47			100							
	20					20							
	40					40							
	60		48		Sten - 7gr	60							
	80					80							
	100		49			100							

Sag: 195-281 7324444444	DGU-nr:	Kote: Terræn	Init.: V1-PB	Dato: 3 / 5 / 22
Boring: B1102	Lok.: Lilleløje	Bundpejl:	Vandspejl:	Side: 5 a 5
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 6"	Filterdim.:	Slidsestr.:	Sandstr.:

Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Notater	
over terræn	Dybde m.	Prøve	Prøve- nr.:	Lag- grænse		Dybde m.	vinge kg	intakt kg	ømrørt kg	dybde m	antal slag pr. 7,5 cm	Fore rør	Dybde af: forgravning/ udtagne miljøprøver/ fræsning (fra/til)/ omrigning til DTH
	20				Sten + grus	20				8.5		1.000.000	
	40					40				9.14			
	60		50			60				12			
	80					80				17			
	100		51		Sten + grus	100							
	20					20							
	40					40							
	60					60							
	80					80							
	100					100							
	20					20							
	40					40							
	60					60							
	80					80							
	100					100							
	20					20							
	40					40							
	60					60							
	80					80							
	100					100							
	20					20							
	40					40							
	60					60							
	80					80							
	100					100							

Sag: <i>152193-281</i>	DGU-nr:	Kote: <i>terras</i>	Init.: <i>R3-RB</i>	Dato: <i>17/5/22</i>
Boring: <i>BH03</i>	Lok.: <i>gilleboje</i>	Bundpejl:	Vandspejl:	Side: <i>1</i> a <i>5</i>
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: <i>8"</i>	Filterdim.:	Slidsestr.:	Sandstr.:

Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Fore rør	Notater
over terræn	Dybde m.	Prøve	Prøve-nr.:	Lag-grænse		Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm		
	20		1		<i>muld jord</i>								
	40				<i>sand</i>								
	60		2										
	80												
	100		3										
	20												
	40												
	60		4										
	80												
	100		5										<i>fuldt sand</i>
	20												<i>fuldt sand</i>
	40												
	60		6										
	80												
	100		7		<i>sand-græs-gul-sten</i>								
	20												
	40												
	60		8										<i>fuldt sand</i>
	80												
	100		9										
	20												
	40												
	60		10										
	80												
	100		11		<i>5.0 stor pose prøve</i>								<i>fuldt sand</i>
	20												
	40												
	60		12										
	80												
	100		13										

Sag: 132193-28	DGU-nr:	Kote: Terrian	Init.: 10-18	Dato: 19/5/22
Boring: BHO3	Lok.: Lilleleje	Bundpejl:	Vandspejl:	Side: 2 a 6
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 8"	Filterdim.:	Slidsestr.:	Sandstr.:

Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Fore rør	Notater
over terræn	Dybde m.	Prøve nr.	Prøve-nr.	Lag-grænse		Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm		
	20				Sand 1/4 gul								
	40												
	60		17							5.3			Lukket sand
	80				Do					4.7			
	100		15							4.4			
	20												
	40				Do								
	60		16										
	80												
	100		12							6.7			Lukket sand
	20												
	40				Do					8.8			
	60		18							4.8			
	80												
	100		17							9.0			
	20				Do								
	40												
	60		20							5.6			Lukket sand
	80		12							6.5			
	100		11		Stor pose prøve					3.95			
	20												
	40												
	60		22										
	80												
	100		23							4.9			Lukket sand
	20									4.6			ind. RAN
	40									7.8			
	60		24							11.1			
	80												
	100		25										

Sag: 23219328	DGU-nr:	Kote: TR	Init.: SS-KG	Dato: 25 / 5 / 22
Boring: BH03	Lok.: Gillelge	Bundpejl:	Vandspejl:	Side: 3 a 6
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 8"	Filterdim.:	Slidsestr.:	Sandstr.:

Pejlerør	Dybde m.	Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Fore rør	Notater
		Prøve nr.:	Prøve- nr.:	Lag- grænse		Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm		
	20				Sand, Tor, gulbrun								
	40									12,45			Lukket Samle
	60	26							46			IND RAM	
	80								79				
	13,00	27			— 11 —				12,9	1113		Tor	
	20												
	40												
	60	28											
	80			13,8									
	14,00	29			ibl. Sten				14,0			Lukket Samle	
	20			14,3					66			ind Ram	
	40				St. Sten				810			Tor	
	60	30							1418	121812			
	80												
	15,00	31										Stor pose PTØRE 15m	
	20												
	40												
	60	32		15,8					155			Lukket Samle	
	80				Tor Str. ke, Sv. Siltet, gråbrun				41	11		ind Ram	
	16,00	33		15,9	7. Sten				15,95	1212		Tor	
	20												
	40												
	60	34											
	80												
	17,00	35			— 11 —				17,0			Lukket Samle	
	20								46			ind Ram	
	40								78				
	60	36							1375	78		Tor	
	80												
	18,00	37											

Sag: 232193-281	DGU-nr:	Kote: VR	Init.: SS-K6	Dato: 30 / 5 / 22
Boring: BHO3	Lok.: Lilleløje	Bundpejl:	Vandspejl:	Side: 4 a 6
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 8"	Filterdim.:	Slidsestr.:	Sandstr.:

Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Notater	
over terræn	Dybde m.	Prøve	Prøve- nr.:	Lag- grænse		Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm	Fore rør	Dybde af: forgravning/ udtagne miljøprøver/ fræsning (fra/til)/ omrigning til DTH
	20				Sand, tør, gulløst	20							
	40		38			40				18,50			Lukket Sonde i DTH
	60					60					5,5		
	80					80				5,6			
	100		39			100			18,73	6,5			
	20			19,30	Sand, GRÅ, VF.	20							
	40		40			40							Stor Pølse Pølse 20m
	60		P40			60							
	80					80							
	100		41			100			20,10	4,6		Lukket Sonde i DTH	
	20					20				6,4		VS. 156 mot	
	40			20,4	Svagt, Gruset.	40			19,70	5,4			
	60		42			60							
	80			20,8	Mere, Gruset, IBL, Sten	80							
	100		43			100							
	20			21,20	% Sten, Sv. Siltet	20							
	40		44			40				21,5			Lukket Sonde i DTH
	60					60					3,5		1 ind Børm VS. 149 mot
	80					80				4,4			
	100		45			100			21,90	5,5			
	20				— 11 —	20							
	40		46			40							
	60					60							
	80					80							
	100		49			100			23,0			Lukket Sonde i DTH	
	20					20				2,9		1 ind Børm VS. 121 mot	
	40					40				5,3			
	60		48			60			23,40	4,5			
	80					80							
	100		49			100							

Sag: 232193-281	DGU-nr:	Kote: TR	Init.: SS, KG	Dato: 31 / 5 / 22
Boring: BH03	Lok.: Lilleløge	Bundpejl:	Vandspejl:	Side: 5 a
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 8"	Filterdim.:	Slidsestr.:	Sandstr.:

Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Notater
over terræn	Dybde m.	Prøve	Prøve- nr.:	Lag- grænse		Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm	
	20				Sand, st. gruset, grå, VF. SAND	20						
	40		50							24,5		
	60									2		ind. Rør
	80		50							23		
	25 00	P	51			25 00			24,0	34		VS. 13,8 m
	20					20						Stor Pose Prøve 25 cm
	40					40						
	60		52			60						
	80					80						
	26 00		53			26 00			26,0			Lukket Sonde
	20					20				43		ind. Rør
	40		2630		M. i. m. Grus more siltslet	40			26,4	57		VS. 12,40 m
	60		54			60						
	80		2640			80						
	27 00		55		1/2 Grus	27 00						
	20					20						
	40		2930			40			27,5			Lukket Sonde
	60		56		SAND, silt, VF. GRA	60				44		ind. Rør
	80					80				45		
	28 00		57			28 00			27,5	55		VS. 13,8 m
	20					20						
	40		58			40						
	60					60						
	80					80						
	29 00		58			29 00			29,0			Lukket Sonde
	20					20				34		ind. Rør
	40					40				44		
	60		60			60			29,5	45		VS. 14,1 m
	80					80						
	30 00		61			30 00						

Sag: 232193-281	DGU-nr:	Kote: TR	Init.: SS, K6	Dato: 31 / 5 / 22
Boring: B1103	Lok.: Gilleløje	Bundpejl:	Vandspejl:	Side: 6 a 6
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 811	Filterdim.:	Slidsestr.:	Sandstr.:

Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Notater	
over terræn	Dybde m.	Prøve	Prøve- nr.:	Lag- grænse		Dybde m.	vinge kg	Intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm	Fore rør	Dybde af: forgravning/ udtagne miljøprøver/ fræsning (fra/til)/ omrigning til DTH
	20				Sand, gr, VF.	20							
	40					40				30,5			Lettest Sand
	60		62			60				5 9			ind Rør
	80				— 11 —	80				9 8			VS 138
	31,00		63			31,00				30,9	8 9		
	20					20							
	40				— 11 —	40							
	60		64			60							
	80					80							
	32,00		65		32,00				32,0			Lettest Sand	
	20				— 11 —	20				8 8			ind Rør
	40					40				9 9			
	60		66			60				32,5	7 8		VS 156 mur
	80				— 11 —	80							
	33,00		67			33,00							
	20					20							
	40				ibl. organisk mat., sv. grus kul	40							
	60		68			60				33,3			Lettest Sand
	80			33,7		80				6 8			ind Rør
	34,00		69		34,00				34,9	8 9		VS 146 mur	
	20				V-shaped hole	20							
	40					40							
	60		70			60							
	80				V-shaped hole	80							
	35,00		71			35,00				35,0			Lettest Sand
	20					20				6 4			ind Rør
	40				40				4 4				
	60				60				35,4	5 4		VS 8, 110	
	80				80								
	00				00								

Sag: 232193-201	DGU-nr:	Kote: TR	Init.: SS-167	Dato: 4 / 5 / 22
Boring: B1104	Lok.: Gilleleje	Bundpejl: 3000	Vandspejl:	Side: 1 a 9
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 8"	Filterdim.: 0,25	Slidsestr.:	Sandstr.: TILBAGEFYLD

Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Notater	
over terræn	Dybde m.	Prøve	Prøve- nr.	Lag- grænse		Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm	Fore rør	Dybde af: forgravning/ udtagne miljøprøver/ fræsning (fra/til)/ omrigning til DTH
	20		1		Sand, grus, sten, tor, brun	20							
	40		2			40							
	60					60							
	80					80							
	100		3			100			1,00			Lukket Sonde	
	20			h2	Sr. Stenet, ibl. grå sand	20				4 3		ind RAM	
	40		4			40				5 2		Tør	
	60					60				1,45 2 3			
	80					80							
	100		5			200			2,00			Lukket Sonde	
	20					20				3 5		ind RAM	
	40		6			40				5 5			
	60					60			2,50	4 5		Tør	
	80					80							
	100		7			300			1,25				
	20					20							
	40		8			40							
	60					60							
	80					80							
	100		9			100			1,12			Lukket Sonde	
	20					20				2 2		ind RAM	
	40		10			40				2 3			
	60					60			1,45	4 5		Tør	
	80					80							
	100		11			500							
	20			S2	St. Stenet	20							
	40					40				5,5			Lukket Sonde
	60		12			60					5 4		ind RAM
	80					80				5 5			
	100		13			600				5 8		Tør	

Sag: 232143-281	DGU-nr:	Kote: 101	Init.: SS-KG	Dato: / /
Boring: BH04	Lok.: Gilleleje	Bundpejl: 50,00	Vandspejl:	Side: 2 a 9
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 8"	Filterdim.: 0,25	Slidsestr.:	Sandstr.: TILBAGEFYLD

Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Notater
over terræn	Dybde m.	Prøve	Prøve-nr.:	Lag-grænse		Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm	
	20				Sand, guls, stenet, br. brun/grå	20						
	40					40						
	60		14			60						
	80					80						
	100		618		Sr. brød, mere fint	100			80			Lukket Sond
	120		15			120			12	2		ind Ram
	140					140			22	2		Tpr
	160		16			160			24	2		
	180		276		mere Lys/Grå	180						
	200		17			200						
	220		83			220						
	240		18		St. Stenet	240			8,5			Lukket Sond
	260					260			5	8		ind Ram
	280		87			280			8	9		
	300		19		Stenet	300			8,5	8	11	ter
	320					320						
	340					340						
	360		20			360						
	380					380						
	400		21			400			10,0			Lukket Sond
	420					420				2	4	ind Ram
	440					440			9	9		
	460		22			460			10,5	11	10	Tpr
	480					480						
	500		23			500						
	520					520						
	540		24			540			11,5			Lukket Sond
	560					560			8	9		ind Ram
	580					580			5	16		
	600		25			600			11,5	17	19	Ter

TILBAGEFYLD



Sag: 232193-281	DGU-nr:	Kote: JØL.	Init.: SSKØ	Dato: 9 / 5 / 22
Boring: BHO1	Lok.: Lilleleje	Bundpejl: 50,00	Vandspejl:	Side: 3 a 7
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 8"	Filterdim.: 0,25	Slidsestr.:	Sandstr.:

Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Notater	
over terræn	Dybde m.	Prøve	Prøve- nr.:	Lag- grænse		Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm	Fore rør	Dybde af: forgravning/ udtagne miljøprøver/ fræsning (fra/til)/ omrigning til DTH
	20				Sand, grus, stenet, + bl. SV. leret	20							
	40												
	60		26										
	80												
	100		27			1300			13,0				Lukket Sonde
	120									8,10			ind. Ram.
	140									10,13			Tør
	160		28						13,45	13,18			
	180			13,7									
	200		29		St. Stenet	1400							
	220												
	240								14,5				Lukket Sonde
	260		30							8,12			ind. Ram.
	280									20,21			
	300		31			1500			15,8	24,23			Tør
	320	A											A-Rør. MIS. A-Rør. DEF AF Sten
	340		32										
	360												
	380												
	400		33			1600			16,0				Lukket Sonde
	420									6,14			ind. Ram.
	440									16,25			
	460		34						16,75	24,24			Tør
	480												
	500		35			1700							
	520												
	540												
	560		36						17,5				Lukket Sonde
	580									6,8			ind. Ram.
	600		37							14,17			
	620												
	640												
	660												
	680												
	700		38			1800				23,2			Tør

BENTONIT

TILBAGE F. YLD.

Sag: 232193-281	DGU-nr:	Kote: TR	Init.: SS-KG	Dato: 10 / 5 / 22
Boring: B1104	Lok.: Gilleleje	Bundpejl: 50,00	Vandspejl:	Side: 4 a 9
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 8"	Filterdim.: 0,25	Slidsestr.:	Sandstr.: TILBAGEFYLD

Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Notater		
over terræn	Dybde m.	Prøve	Prøve- nr.:	Lag- grænse		Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm	Fore rør	Dybde af: forgravning/ udtagne miljøprøver/ fræsning (fra/til)/ omrigning til DTH	
	20				Sand, sv. leret, gub, Støret 1/3 Brun, tør.	20								
	40					40								
	60		38			60								
	80					80								
	1900		39			1900			19,9				Lukket Sand	
	20					20				18,6			ind Ram 2 cm mangler 9 cm	
	40					40			19,34	32,34			Tør	
	60		40			60								
	80					80								
	2000		41			2000								
	20					20								
	40					40			20,5				Lukket Sand	
	60		42			60				22,3			ind Ram 6 cm mangler 13 cm	
	80					80				43,46			Tør	
	2100		43			2100			20,8	41				
	20					20								
	40					40								
	60		44		Støret	60								
	80					80								
	2200		45			2200			22,0				Lukket Sand	
	20					20				6,14			ind Ram	
	40					40				16,21				
	60		46			60			22,5	28,3			Tør	
	80					80								
	2300		47			2300								
	20					20								
	40					40								
	60		48			60			23,5				Lukket Sand	
	80					80				2,3			ind Ram	
	2400		49			2400			23,95	21,26			Tør	

TILBAGEFYLD

Sag: 232143-28	DGU-nr:	Kote: TQ	Init.: SS.K6	Dato: 11 / 5 / 22
Boring: B104	Lok.: Gilleleje	Bundpejl: 50,00	Vandspejl:	Side: 5 a 9
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 8"11	Filterdim.: 0,25	Slidsestr.:	Sandstr.: TILBAGE FYLD

Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Notater	
over terræn	Dybde m.	Prøve	Prøve- nr.:	Lag- grænse		Dybde m.	vinge	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm		Fore rør
	20				SAND, SV. Lert, græs, Stenet vs. Brun. Tor	20							
	40					40							
	60	50				60							
	80					80							
	100					100				250			Lukket Son
	20	51				20				59		lukket Son	
	40					40				25,49	28,29		lukket Son
	60	52				60				30,20			lukket Son
	80					80							lukket Son
	100					100				26,5			lukket Son
	20	53				20				41		lukket Son	
	40					40				20,31			lukket Son
	60	54				60				26,95	48,1		lukket Son
	80					80							lukket Son
	100					100				28,0			lukket Son
	20	55	220	St. Stenet		20				18		lukket Son	
	40					40				28,2	24,96		lukket Son
	60	56				60							lukket Son
	80					80							lukket Son
	100					100				29,5			lukket Son
	20	57				20				7,11		lukket Son	
	40					40				16,20			lukket Son
	60	58				60				22,29			lukket Son
	80					80							lukket Son
	100					100				24,18			lukket Son
	20	59	290	Stenet		20						lukket Son	
	40					40							lukket Son
	60	60				60							lukket Son
	80					80							lukket Son
	100					100							lukket Son
	20	61				20						lukket Son	
	40					40							lukket Son
	60					60							lukket Son
	80					80							lukket Son
	100					100							lukket Son

TILBAGE FYLD

Aarsleff



Sag: 232193-281	DGU-nr:	Kote: TOR	Init.: 55 kg	Dato: 12 / 5 / 22
Boring: B1104	Lok.: Gilleleje	Bundpejl: 50,00	Vandspejl:	Side: 6 a 9
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 8"	Filterdim.: 0,25	Slidsestr.:	Sandstr.: 7,2 BAGET YLD

Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Fore rør	Notater
over terræn	Dybde m.	Prøve	Prøve-nr.	Lag-grænse		Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm		
	20				Sand, grus, sv. leret, Stenot, 18% grus	20							
	40		304		Tør	40							
	60	-62			Sand, grus, VF., Sten 312	60							Sandstump fra 30,4 m
	80					80							↓
	100	-63				31 00				31,0			Lukket Sand
	20					20					20,5		ind Rør 6,5 cm
	40					40					16,9		VS. 12,5 m
	60	-64				60				31,39	14 10		
	80		317		St. Stenot	80							
	100	-65				32 00							
	20					20							
	40					40							
	60	-66				60				32,5			Lukket Sand
	80					80					22		Mingler
	100	-67				33 00					21 30		ind Rør 7 cm
	20					20					34 35		Mingler 6,5 cm
	40					40							VS. 16,0 m
	60					60							
	80					80							
	100	-69				34 00					34,0		Lukket Sand
	20					20					25		ind Rør 7,5 cm
	40					40					32		Mingler 11,5 cm
	60	-70				60				34,25	24 11		VS. 15,5 m
	80					80							
	100	-71				35 00							
	20					20							
	40					40							
	60	-72				60				35,5			Lukket Sand
	80					80					21 4		Mingler
	100	-73				36 00					32 36		ind Rør 9,5 cm
	20					20							
	40					40							
	60					60							
	80					80							
	100					36 00					30		Mingler 10,5 cm
													VS. 21,2 m

TIL BAGE FYLD

Sag: 232193-281	DGU-nr:	Kote: T02	Init.: SS-KG	Dato: 16 / 5 / 22
Boring: B1104	Lok.: Gilleboje	Bundpejl: 50,00	Vandspejl:	Side: 7 a 9
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 8"	Filterdim.: 0,25	Slidsestr.:	Sandstr.: TILBAGEFYLD

Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Notater
over terræn	Dybde m.	Prøve nr.	Prøve-nr.	Lag-grænse		Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm	
	20				Sand, Grus, St. Stenat VF. g/c	20						
	40					40						
	60	74		36,7		60						
	80				St. Stenat + St. gruset	80						
	100	75				100			37,0			Lukket Sonde
	120					120				2 2		ind Rør
	140					140				2 3		
	160	76				160			37,4	3 4		VS. 18,3 mtr
	180					180						
	200	77		37,7	Stenat	200						
	220					220						
	240	78				240			38,5			Lukket Sonde
	260					260				6 6		ind Rør
	280					280				7 8		
	300	79				300			38,9	8 9		VS. 19,6 mtr
	320					320						
	340	80				340						
	360					360						
	380					380						
	400	81				400			40,5			Lukket Sonde
	420					420				8 4		ind Rør
	440					440				8 6		
	460	82				460			40,5	6 7		VS. 19,6 mtr
	480					480						
	500	83		40,8	med sandet	500						
	520					520						
	540	84		41,3	Sand, Grus, Sv. Gruset, VF	540						
	560					560			41,5			Lukket Sonde
	580					580				6 8		ind Rør
	600	85				600				8 8		
	620					620				7 10		VS. 12,9 mtr

TILBAGE FYLD

Sag: 232193-28	DGU-nr:	Kote: TOR	Init.: SS. K6	Dato: 17 / 5 / 22
Boring: BH04	Lok.: Gilleboje	Bundpejl: 50,00	Vandspejl:	Side: 8 a 9
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 8"	Filterdim.: 0,25	Slidsestr.:	Sandstr.: TILBAGEFILD

Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Notater		
over terræn	Dybde m.	Prøve	Prøve- nr.:	Lag- grænse		Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm	Fore rør	Dybde af: forgravning/ udtagne miljøprøver/ fræsning (fra/til)/ omrigning til DTH	
	20				Sand, grå, groset, VF	20								
	40					40								
	60		86			60								
	80					80								
	100		87			100				430			Lukket sonde	
	120					120					109		IND RAM	
	140					140				438	108		VS. 17,8m	
	160		88			160								
	180					180								
	200		89			200				440				
	220				— —	220								
	240					240								
	260		90			260				445			Lukket Sonde	
	280					280					105		IND RAM	
	300		91			300				449	88		VS. 19,4m	
	320					320					88			
	340		92			340								
	360					360								
	380		93			380				460			LUKKET SONDE	
	400					400					106		IND RAM	
	420					420				98				
	440		94			440				48,45	87		VS. 24,10	
	460					460								
	480					480								
	500		95			500				47,45				
	520					520								
	540		96			540					108		LUKKET SONDE	
	560					560					88		IND RAM	
	580					580					88			
	600		97			600				4790	86		VS. 27,00	

TILBAGE FILD

Sag: 232193	DGU-nr:	Kote: TR	Init.: PRN/HANSE	Dato: 23 / 5 / 22
Boring: BH04	Lok.: Lilleleje	Bundpejl: 50,00	Vandspejl:	Side: 9 a 9
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 8"	Filterdim.: 0,25	Slidsestr.:	Sandstr.: SAND 3 ØMRING FILTER

Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Notater	
over terræn	Dybde m.	Prøve	Prøve- nr.:	Lag- grænse		Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm		Fore rør
TILBAGEFYLD	20				SAND grø i gruset i bl kolksten - stør	20						Stør Blækprøve fr 15-17	
	40		98			40							
	60					60							
	80					80							
	100		99			100				49	49		
	20					- 11 -	20				34		Indtrængning u.s 29,5
	40		100				40				56		
	60						60				80		
	80						80						
	100		101				100						
STOP DYBDE 50,00 MUT						20							
	40				40								
	60				60								
	80				80								
	100				100								
	20				20								
	40				40								
	60				60								
	80				80								
	100				100								

Sag: <i>117374</i>	DGU-nr:	Kote: <i>Terræn</i>	Init.: <i>V13-88</i>	Dato: <i>25/4/22</i>
Boring: <i>1115</i>	Lok.: <i>1115</i>	Bundpejl:	Vandspejl: <i>225</i>	Side: <i>1 a 5</i>
Foringsrør: <input type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: <i>6"</i>	Filterdim.:	Slidsestr.:	Sandstr.:

Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Notater	
over terræn	Dybde m.	Prøve	Prøve- nr.	Lag- grænse		Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm	Fore rør	Dybde af: forgravning/ udtagne miljøprøver/ fræsning (fra/til)/ omrigning til DTH
	20				<i>gult sand</i>	20							
	40					40							
	60					60							
	80					80							
	100				<i>Do</i>	100							
	20					20							
	40					40							
	60					60							
	80					80							
	100				<i>Do</i>	100							
	20					20							
	40					40							
	60					60							
	80					80							
	100				<i>Do</i>	100							
	20				<i>VF</i>	20							
	40				<i>gul</i>	40							
	60					60							
	80					80							
	100				<i>Do</i>	100							
	20					20							
	40					40							
	60					60							
	80					80							
	100				<i>Do</i>	100							
	20					20							
	40					40							
	60					60							
	80					80							
	100				<i>Do</i>	100							

Sag: <i>152 193-781</i>	DGU-nr:	Kote: <i>Terræn</i>	Init.: <i>VH-PB</i>	Dato: <i>25 / 4 / 22</i>
Boring: <i>BH 05</i>	Lok.: <i>Gilleboje</i>	Bundpejl:	Vandspejl:	Side: <i>2 a 5</i>
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.:	Filterdim.:	Slidsestr.:	Sandstr.:

Pejlerør	Dybde m.	Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Notater
		Prøve	Prøve-nr.:	Lag-grænse		Dybde m.	vinge kg	intakt kg	omrørt	dybde m	antal slag pr. 7,5 cm	
<i>over terræn</i>	20				<i>Sand gul VF</i>	20						
	40		<i>14</i>									
	60											
	80				<i>Do</i>							
	100		<i>15</i>									
	20											
	40		<i>16</i>									
	60				<i>Do</i>							
	80											
	100		<i>17</i>									
	20											
	40		<i>18</i>	<i>370</i>	<i>m Sand</i>	<i>grå</i>						
	60											
	80											
	100		<i>19</i>									
	20					<i>Do</i>						
	40		<i>20</i>									
	60											
	80											
	100		<i>21</i>			<i>Do</i>						
	20											
	40		<i>22</i>			<i>SAND STEN GRUS</i>						
	60											
	80											
	100		<i>23</i>									
20												
40		<i>24</i>			<i>Do</i>							
60												
80												
100		<i>25</i>										

D:\15\Borejournal

Sag: 232193-281	DGU-nr:	Kote: Terræn	Init.: Vt-98	Dato: 25 / 4 / 22
Boring: BHC5	Lok.: Lillekøje	Bundpejl:	Vandspejl:	Side: 3 a 5
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 6"	Filterdim.:	Slidsestr.:	Sandstr.:

Pejlerør	Dybde m.	Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Fore rør	Notater
		Prøve nr.:	Prøve- grænse	Lag- grænse		Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm		
over terræn													
	20				Sand - silten	20							
	40					40							
	60	26				60				5			26-27 Sand - silten
	80					80				6			
	100	27				100				6			
	20				Sten - grus - sand	20							
	40					40							
	60	28				60							
	80					80							
	100	29			Do	100							
	20					20				27			
	40					40				28			
	60	30				60							
	80				Do	80							
	100	31				100							
	20					20							
	40					40							
	60	32				60							
	80					80							
	100	33				100							
	20					20							
	40					40							
	60	34				60							
	80					80							
	100	35				100							
	20					20							
	40					40							
	60	36				60							
	80					80							
	100	37			Do	100							

Aarsleff Borejournal

Sag: 252193-281	DGU-nr:	Kote: Terræn	Init.: V17-PB	Dato: 25 / 4 / 22
Boring: B1105	Lok.: Lillebjerg	Bundpejl:	Vandspejl:	Side: 14 a
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 6"	Filterdim.:	Slidsestr.:	Sandstr.:

Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Notater	
over terræn	Dybde m.	Prøve	Prøve-nr.:	Lag-grænse		Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm	Fore-rør	Dybde af: forgravning/udtagne miljøprøver/fræsning (fra/til)/omrigning til DTH
	20				Sand - sten grus	20							
	40		38			40							
	60					60							
	80					80							
	100		39		Do	100							
	20					20				66			
	40					40				54			
	60		40			60				65			
	80					80							
	100		41		Sten grus	100							
	20					20							
	40					40							
	60		42			60				34			
	80					80				87			
	100		43			100				910			
	20				Sand - grus	20							
	40					40							
	60		44			60							
	80					80							
	100		45		Do	100							
	20					20							
	40					40							
	60		46			60							
	80				Do	80							
	100		47			100							
	20					20							
	40					40							
	60		48			60							
	80				Do	80							
	100		49			100							

Sag: 232193-281	DGU-nr:	Kote: Terræn	Init.: V17-PB	Dato: 25 / 4 / 22
Boring: B105	Lok.: Gilleboje	Bundpejl:	Vandspejl:	Side: 5 a 5
Foringsrør: <input checked="" type="checkbox"/> Ja <input type="checkbox"/> Nej	Boringsdim.: 6"	Filterdim.:	Slidsestr.:	Sandstr.:





Pejlerør		Prøver			Jordartsbeskrivelse	Vingeforsøg				SPT		Fore rør	Notater
over terræn	Dybde m.	Prøve	Prøve-nr.:	Lag-grænse		Dybde m.	vinge kg	intakt kg	omrørt kg	dybde m	antal slag pr. 7,5 cm		
	20				Sand - grus - sten gml	20							Lukket sand
	40		50			20							
	60				stør pose 25.0 m	60							79 11k
	80		51			80							
	100					100							
	20					20							
	40					40							
	60					60							
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	80					80							
	100					100							

APPENDIX 7.1 – RISK LOG

Energinet-Gildbjerg Hoved HDD

Risk Log

2022-06-30

No.	Description	Time	Risk level
1	<p>Risk description: Boulders in soil - large</p> <p>Cause description: Cause #1: Primarily boulders in clay till, gravel and dense gravel in the glacier layer. Cause #15: Several boulders resulted in delays of Geotechnical boreholes. Cause #19: Encountering one or several large boulders during HDD can cause delay in operations.</p> <p>Effect description: Effect #1: Can lead to withdrawal and new HDD pilot hole.</p> <p>Control-4: <i>Minimize drilling distance in clay till and gravel layers.</i> Possible - No deadline</p>	Time	
12	<p>Risk description: Not possible to maintain sufficient pressure</p> <p>Cause description: Cause #12: Relevant for sand deposits. In dry sand drilling fluid can flow into the soil. Drilling is expected in the late glacial and glacial sand layer.</p> <p>Effect description: Effect #10: New start up can be required or change of drilling procedure.</p> <p>Control-11: <i>Minimize drilling in dry sand or coarse material.</i> Possible - No deadline</p> <p>Control-12: <i>Design of drilling mud according to conditions - saturated and non-saturated.</i> Possible - No deadline</p>	Time	
14	<p>Risk description: Drilling below and above water table</p> <p>Cause description: Cause #14: When there is a change going from saturated to unsaturated conditions this can cause loss of pressure.</p> <p>Effect description: Effect #12: Can require more pressure and require adaptation of set-up.</p> <p>Control-12: <i>Design of drilling mud according to conditions - saturated and non-saturated.</i> Possible - No deadline</p>	Time	
8	<p>Risk description: Challenging drilling conditions and area constraints due to multiple parallel HDD</p> <p>Cause description: Cause #8: Blow out can lead to a situation with no feasible drilling route. Challenging due to long length of app. 1 km and sand deposits. Cause #16: Up to three parallel HDD routes.</p> <p>Effect description: Effect #7: In worst case new alignment or new contractor is required.</p>	Time	

16	<p>Risk description: Boulders in soil - small</p> <p>Cause description: Cause #1: Primarily boulders in clay till, gravel and dense gravel in the glacier layer.</p> <p>Effect description: Effect #14: Withdraw and minor rerouting of HDD</p>	Time	
2	<p>Risk description: Limited geotechnical information between Gilbjerg Hoved HDD and offshore cable survey</p> <p>Cause description: Cause #2: Uncertain geology towards sea at marine exit point. Nearest geotechnical borehole is on 10m water depth.</p> <p>Effect description: Effect #13: Uncertain to contractor how plan the work at sea.</p> <p>Control-6: <i>Contractor shall familiarize himself with the cable route survey reports.</i> Possible - No deadline</p>	Time	
5	<p>Risk description: Blowout, damage to road</p> <p>Cause description: Cause #5: HDD crossing of road at Gilbjerg Hoved. Start point is close to surface of the road.</p> <p>Effect description: Effect #4: Settlements of road leading to potential closure of road.</p> <p>Control-7: <i>Safe distance from HDD starting point to road and amount of overburden between HDD and road.</i> Possible - No deadline</p>	Time	
6	<p>Risk description: Blowout, damage to surroundings</p> <p>Cause description: Cause #6: Gilbjerg Hoved is nature 2000 area. Probability dependent of depth of drilling which is expected in the post glacial layer.</p> <p>Effect description: Effect #5: Blow out can results in drilling mud at surface in Natura 2000 area, this can cause a delay require cleaning up and informing authorities.</p> <p>Control-2: <i>Response plan shall handle this to minimize impact on area.</i> Possible - No deadline</p> <p>Control-8: <i>Increase overburden.</i> Possible - No deadline</p> <p>Control-9: <i>Manage use of drilling mud additives</i> Possible - No deadline</p>	Time	
4	<p>Risk description: Blowout, easy clean up</p> <p>Cause description: Cause #4: Probability is highest when drilling through sand deposits.</p> <p>Effect description: Effect #3: New drilling is required</p>	Time	

17 **Risk description:**
Large boulder reduces diameter of HDD casing
Cause description:
Cause #18: Encountering boulders when pulling pilot pipe may cause damage to pipe.
Effect description:
Effect #15: Damage to pilot pipe and increased friction and risk when pulling cable through pipe.
Control-15:
Design pilot pipe according to high voltage cable and HDD according to pilot pipe.
Possible - No deadline

Time



11 **Risk description:**
Risk of friction during drilling
Cause description:
Cause #11: Probability is in general largest in clay till.
Effect description:
Effect #9: Can lead to new reaming up several times leading to delays. Pipes can get stocked due to friction.
Control-10:
Additives to drilling mud.
Possible - No deadline

Time



15 **Risk description:**
Crossing of high voltage cable.
Cause description:
Cause #17: Depth of high voltage cable is not known.
Control-13:
Awareness of cable when planning HDD route.
Possible - No deadline

Control-14:
LER investigation and contact to cable owner
Possible - No deadline

Time



10 **Risk description:**
Interference with roots
Cause description:
Cause #10: There can be roots from vegetation.

Time



