

APRIL 2021
ENERGINET ELTRANSMISSION A/S

THOR OFFSHORE WIND FARM LANDFALL SITE INVESTIGATIONS

GEOTECHNICAL INVESTIGATION
REPORT NO. 1

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GEOTECHNICAL INVESTIGATION
REPORT NO. 1

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PREPARED

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1 Purpose of the investigation

A geotechnical investigation has been undertaken at the landfall site of the Thor Offshore Wind Farm project at Fjaltring.

The purpose of the investigation is to provide geological and geotechnical data in sufficient detail for the planning and design of the HDD at the site.

2 Project

The location of the landfall site and a planned 300m wide corridor for the HDD is shown on the location plan "G002", dated 10 August 2017 and prepared by Energinet Eltransmission A/S.

The location plan Encl. No. 1.14. is based on location plan "G002" and shows the planned centreline of corridor for the HDD.

Currently, there is no information about the planned depth of the HDD. However, the planned investigation depth for geotechnical investigation has been set to level -25m, DVR90 by Energinet.

3 Field investigation and laboratory work

The geotechnical field investigations were performed during the period 3 to 16 March 2021 and comprised 3 nos. geotechnical boreholes denoted B/CPT 1, B/CPT 3 and B/CPT 4, and 6 nos. CPTs denoted CPT 1 – CPT 6.

The locations of the boreholes and CPTs were surveyed using GPS equipment.

The locations of the boreholes and CPTs are shown on the Site Location Plan, Encl. No. 1.14.

The geotechnical boreholes were performed to a depth of 27.0 – 31.0 m below ground level (m b. g. l.).

The boreholes were drilled with a hydraulic rig, using casing, shell and auger techniques and with a borehole diameter of 150 mm.

The CPTs were performed to a depth of 12.8 – 21.5m b. g. l.

The depth of the CPTs were planned to match the depth of the neighbouring boreholes. However, all CPTs were terminated at maximum thrust of the CPT equipment at approx. 10 tons. Under level of refusal, SPT tests were performed in cohesionless soils for every 2 - 3m in the neighbouring borehole.

The CPTs were carried out with a piezocone, which enables measurements of tip and sleeve resistance as well as pore water pressure.

SPT tests shows the number of blows, N , necessary to achieve a penetration of the sampler of 300mm, N_{300} .

During the drilling, the thicknesses and depths of all encountered strata were noted. Representative, disturbed samples were recovered from all layers and at intervals not exceeding 0.5m.

In the boreholes undisturbed tube samples (A-tubes) or large, disturbed samples (approx. 10 kg) were recovered for approx. every 5.0m from approx. 5.0m b. g. l. A-tubes were recovered in cohesive soils and disturbed samples were recovered in sand deposits.

Field vane tests were carried out in cohesive soils in order to determine the undrained shear strengths of the materials in the undisturbed state, as well as after remoulding (C_{FV} respectively C_{FVR}).

A standpipe, consisting of Ø25mm PVC tube with slots at the base, was installed in the boreholes B/CPT 4 and B/CPT 5 to allow monitoring of the ground water level in the boreholes. A bentonite plug was installed above the filter to prevent surface water from influencing the water level in the standpipe.

Monitoring of the water levels was performed on 29 March 2021.

A geological description and classification of all soil samples was carried out in the laboratory. This work was performed in accordance with the guidelines in the Danish Geological Society's publication "Vejledning i ingeniørgeologisk prøvebeskrivelse" dated February 2009.

The carbonate content of the soil samples was qualitatively evaluated by the reaction of the samples to 10 % hydrochloric acid.

The natural water content, w , of the soil samples was determined on selected samples.

The bulk density of the soil was conducted on all suitable undisturbed samples.

The Plasticity Index by Atterberg limit tests was determined on selected soil samples.

The results of the field and laboratory work are presented on the borehole logs, Enclosure Nos. 1.1, 1.4, 1.5 and the CPT logs, Enclosure Nos. 1.1CPT – 1.6CPT.

The results of the above has been reported to the Jupiter Database.

The particle size distribution by sieve analysis and by combined sieve and hydrometer analysis was determined on selected soil samples. The results of these tests are given in table 3 and in Enclosure Nos. 1.7 – 1.9.

The thermal conductivity was determined on selected soil samples. The results of these tests are given in table 4 and in Enclosure Nos. 1.10 – 1.12.

A legend for the symbols used on the boreholes and CPT logs is presented in Encl. A-1.

4 Levels and coordinates

All depths are measured from the ground surface as meters below ground level, (m b. g. l.).

All levels refer to the Danish National Survey System, "Dansk Vertikal Reference 1990" (DVR90).

The system DVR90 is approximately coinciding with Mean Sea Level at the shoreline.

The coordinate system used for determining coordinates for the locations of the boreholes and CPTs is UTM32.

Levels and coordinates for all boreholes and CPTs are shown in Table 1.

Table 1: Levels and coordinates at boreholes and CPTs

Borehole No. CPT No.	Ground Level Elevation (m)	X (m)	Y (m)
B/CPT 1 CPT 1	+1.3	446,032	6,257,440
CPT 2	+1.2	446,012	6,257,295
CPT 3	+3.7	446,239	6,257,460
B/CPT 4 CPT 4	+2.7	446,221	6,257,293
B/CPT 5 CPT 5	+5.1	446,407	6,257,482
CPT 6	+3.3	446,366	6,257,310

5 Subsurface conditions

5.1 General

In general, the subsurface conditions encountered in the boreholes comprise of postglacial sand and gravel overlying late glacial and glacial clay, sand and gravel deposits. These deposits are then primarily overlying Miocene clay and sand deposits along with Miocene Gytta.

In the boreholes B/CPT 4 and B/CPT 5 the upper 0.6 and 0.8 m comprises of topsoil.

Below the topsoil and from terrain in borehole B/CPT 1 postglacial sand and gravel is found to a depth of 3.7 – 4.9 m b. g. l. The postglacial deposits are underlain by late glacial and glacial sand, gravel and clay to 14.7 – 17.2 m b. g. l. Most of the clay deposits are very high plasticity clay.

In borehole B/CPT 5 the late glacial and glacial deposits are underlain by 0.3 m of glacial clay till. Under the clay till in borehole B/CPT 5, and under the late glacial and glacial deposits in the other boreholes, Miocene deposits, primarily consisting of clay and sand, are encountered to the base of the boreholes 27.0 – 30.0 m b. g. l. However, in borehole B/CPT 4 and B/CPT 5 Miocene gytta is encountered from 22.5 to 25.3 m b. g. l. Most of the clay deposits are very high plasticity clay.

CPT tip resistances from 5 to >20 MPa are recorded in the late glacial sand, indicating that these deposits are medium dense to dense.

In the Miocene sand deposits, SPT tests results are generally greater than 50 blows pr. 300 mm, indicating that these deposits are generally very dense.

The subsurface conditions can be divided into the general layers as shown in Table 2.

Table 2: Subsurface conditions

Soil type	B/CPT 1 Elev. (m)	B/CPT 4 Elev. (m)	B/CPT 5 Elev. (m)
TOPSOIL and SAND, Re	-	+2.7 - +1.9	+5.1 - +4.5
SAND and GRAVEL, Pg	+1.3 - -3.3	+1.9 - -2.3	+4.5 - +1.4
SAND and GRAVEL, Lg	-	-2.3 - -2.5	+1.4 - -1.3
CLAY, Lg/Gc	-3.3 - -12.3	-2.5 - -9.4	-1.3 - -8.9
SAND, Lg/Gc	-	-9.4 - -11.3	-
CLAY, Lg/Gc	-	-11.3 - -12.3	-
GRAVEL, Lg/Gc	-	-12.3 - -12.5	-8.9 - -10.0
SAND, Lg/Gc	-12.3 - -13.4	-	-10.0 - -12.1
CLAY TILL, Gc	-	-	-12.1 - -12.4
CLAY, Mi	-	-12.5 - -13.6	-
SAND, Mi	-13.4 - -18.0	-13.6 - -19.8	-12.4 - -18.7
GYTTJA, Mi	-	-19.8 - -20.5	-18.7 - -20.2
CLAY, Mi	-18.0 - -22.8	-20.5 - -22.7	-20.2 - -25.9
SAND, Mi	-22.8 - -25.7	-22.7 - -25.3	-

5.2 Geology

The geological conditions that apply to the area around the planned line for the HDD are briefly described here. The description is based on data from the GeoAtlas and Jupiter database and boreholes and CPTs carried out in connection with the present project.

A conceptual geological profile along the expected corridor for the project can be seen in Enclosure Nos. 1.13.

As described in section 5.1 the area is generally made up of the following layers:

Postglacial SAND and GRAVEL (S1) overlying late glacial and glacial CLAY (C1), SAND and GRAVEL (S2) and CLAY TILL (C 2) deposits. These deposits are then primarily overlying Miocen CLAY (C3) and SAND (S3) deposits along with Miocene GYTJA (G1).

5.3 Particle Size Distribution

The particle size distribution by sieve analysis and by combined sieve and hydrometer analysis was determined on sample 30A and 40A from borehole B/CPT 1, sample 22A and 43A from borehole B/CPT 4 and sample 26A and 44A from borehole B/CPT 5. The results of these tests are given in Table 3 and in Enclosure Nos. 1.7 – 1.9.

Table 3: Particle Size Distribution

Borehole No.	Sample No.	Geological Description	d ₁₀ (mm)	d ₅₀ (mm)	U (d ₆₀ / d ₁₀)
B/CPT 1	30A	SAND, fine, silty, micaceous, with small lignite fragments, sorted	0.07	0.16	2,7
B/CPT 1	40A	CLAY, very high plasticity, micaceous	-*	0.01	-*
B/CPT 4	22A	CLAY, very high plasticity	-*	0.01	-*
B/CPT 4	43A	SAND, fine, micaceous, with small fragments of lignite, sorted	0.06	0.11	2.1
B/CPT 5	26A	CLAY, very high plasticity, with many thin layers of silt	-*	0.00	-*
B/CPT 5	44A	SAND, medium - coarse, with a few gravels, sorted	0.18	0.44	3.0

* Contains more than 10% silt/clay

5.4 Thermal Conductivity

The thermal conductivity was determined on sample 40A from borehole B/CPT 1, sample 43A from borehole B/CPT 4 and sample 26A from borehole B/CPT 5. The results of these tests are given in Table 4 and in Enclosure Nos. 1.10 – 1.12.

Table 4: Thermal Conductivity

Borehole No.	Sample No.	Depth (m b. g. l.)	Geological Description	Thermal Conductivity (W / (m*K))
B/CPT 1	40A	20.0 – 20.6	CLAY, very high plasticity, micaceous	1.549
B/CPT 4	43A	20.0	SAND, fine, micaceous, with small fragments of lignite, sorted	2.207
B/CPT 5	26A	13.0 – 13.5	CLAY, very high plasticity, with many thin layers of silt	1.669

The results of the conducted tests show that the thermal conductivity of the tested samples is in the range of 1.549 – 2.207 W/(m*K).

6 Water levels

The water level in the standpipes in the boreholes was measured the 29 March 2021. The results are presented in Table 5 below:

Table 5: Water level measurements 29 March 2021

Borehole No.	Elev. (m)	Filter level (m b. g. l.)	Date	Water Level	
				Depth (m b. g. l.)	Elev. (m)
B/CPT 4	+2.7	4.4 – 5.0	29-03-2021	1.7	+1.0
B/CPT 5	+5.1	5.3 – 6.0	29-03-2021	2.5	+2.6

The ground water level is expected to vary during the course of the year due to seasonal variations.

A more detailed description of the encountered subsurface conditions can be seen on the borehole logs.

7 Geotechnical interpretations

The terrain at the boreholes and CPTs varies from +5.1 to +1.2 m.

Based on the boreholes and CPTs it is expected that the HDD will primarily be drilled in late glacial/glacial clay or in Miocene sand and clay deposits.

Field vane tests in the late glacial/glacial clay deposits show an undrained shear strength of approx. 100 – 300 kN/m³. Field vane tests in the late Miocene clay deposits show an undrained shear strength of approx. 600 – >700 kN/m³.

Furthermore, most of the late glacial, glacial and Miocene clay deposits have a very high plasticity, which is based on their water content and the visual classification of the samples

There is a potential risk of swelling for high and very high plasticity clay. If the HDD is placed in the late glacial, glacial and Miocene clay deposits, appropriate measures must be taken to ensure that the drilling equipment does not stop as a result of increased surface pressure from the clay.

The performed Atterberg limit tests shows Plasticity Indexes ranging from 6.6 to 33.5 as shown on the borehole logs Enclosure Nos. 1.1, 1.4, 1.5. indicating a lower plasticity. However, based on the water content and the visual classification of the samples, it is estimated that the potential risk of swelling will be that of very high plasticity clay.

The Miocene sand deposits at the western part of the line are mainly fine grained and silty. At the eastern part of the line the sand deposits are mainly fine – coarse grained. The SPT tests conducted in the Miocene sand deposits indicates, that these deposits are generally very dense.





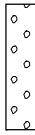


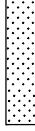
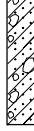

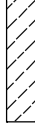
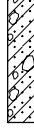

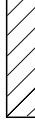

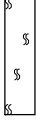

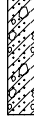







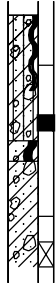
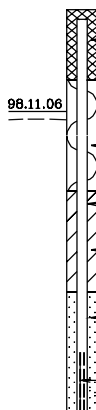
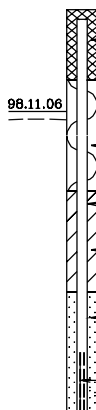











The primary challenges for the HDD will be:

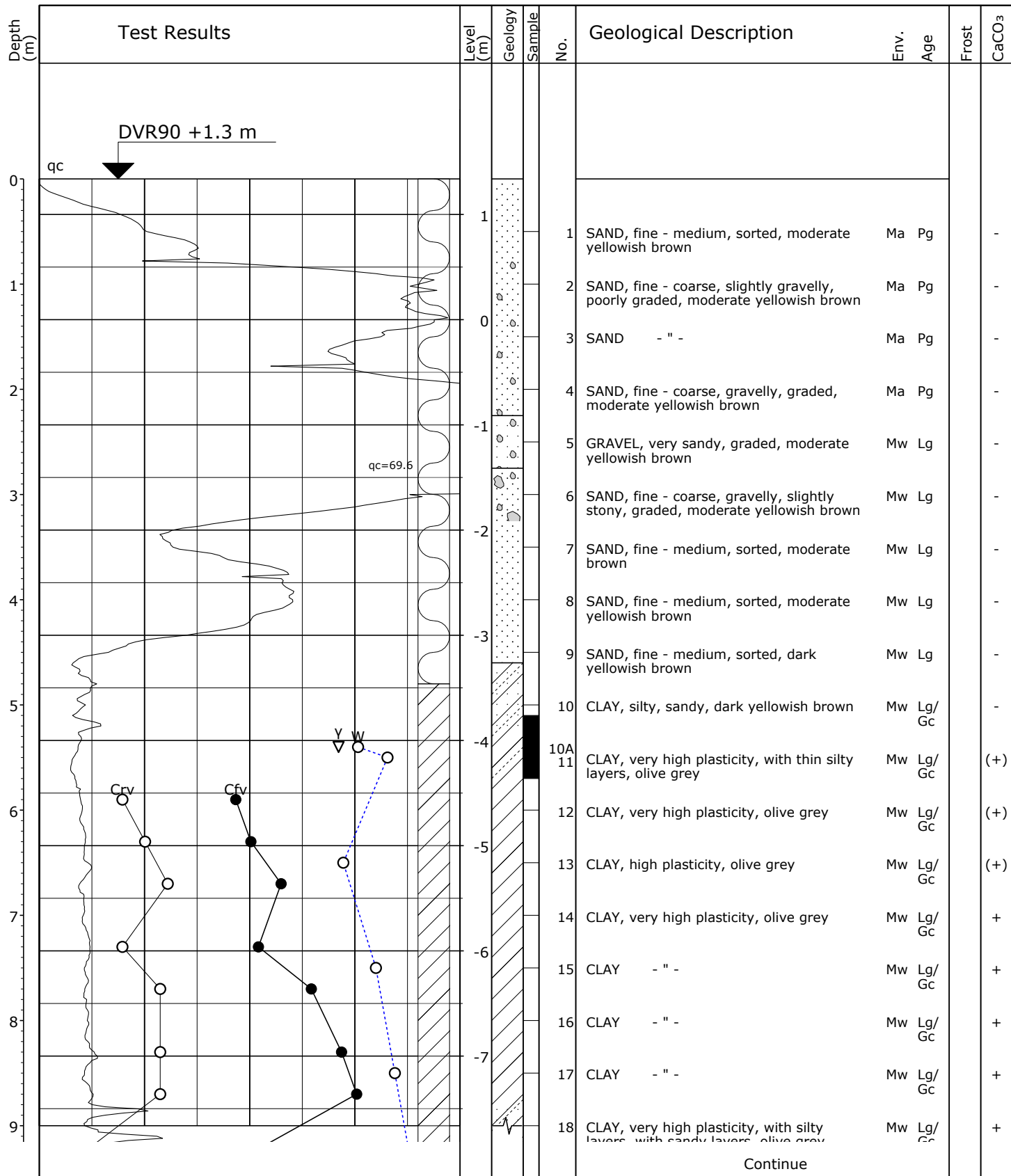
- > Risk of swelling of clays with high and very high plasticity
- > Very dense Miocene sand and clay deposits
- > Loss of pressure in sand and gravel layers

8 Final remarks

The recovered soil samples will be stored for a period of one year from the date of this report. After this period the samples will be disposed of unless other agreed with Energinet.

COWI is available for further discussions regarding geotechnical and foundation issues in relation to the project.

LEGEND FOR BOREHOLE LOGS									
Soil Signature				Location Plan			Borehole log		
<div><div> Fill</div><div> Cobbles</div><div> Limestone</div></div> <div><div> Mull</div><div> Gravel</div><div> Flint</div></div> <div><div> Peat</div><div> Sand</div><div> Clay till</div></div> <div><div> Gyttja</div><div> Silt</div><div> Silt till</div></div> <div><div> Shells</div><div> Clay</div><div> Sand till</div></div> <div><div> Plant remains</div><div> Rock</div><div> Gravel till</div></div> <p>Till deposits can be expected to contain cobbles and boulders (not apparent in borings).</p>				<div><div> LB 10</div><div> Pump Boring</div><div> Environmental Boring</div><div> Simple Boring</div><div> Stratigraphic Boring</div><div> Geotechnical in situ boring and laboratory tests</div><div> Sounding, dynamic penetration test</div></div>			<div></div> <div>3 Sample number</div> <div>Undisturbed sample</div> <div>Layer boundary</div> <div>Disturbed sample</div> <div>10 kg disturbed sample or SPT sample</div>		
				Geological abbreviations			Stand pipe		
				<div>Environment :<div><div>Fw</div><div>Freshwater deposit</div></div><div><div>Ss</div><div>Solifluction soil</div></div><div><div>Fi</div><div>Fill</div></div><div><div>Gl</div><div>Glacier deposit</div></div><div><div>Ma</div><div>Marine deposit</div></div><div><div>Wd</div><div>Washdown deposit</div></div><div><div>Ts</div><div>Top soil</div></div><div><div>Ls</div><div>Landslide deposit</div></div><div><div>Mw</div><div>Meltwater deposit</div></div><div><div>Ae</div><div>Aeolian (wind) deposit</div></div></div> <div>Age :<div><div>Re</div><div>Recent</div></div><div><div>Pg</div><div>Postglacial</div></div><div><div>Lg</div><div>Late Glacial</div></div><div><div>Gc</div><div>Glacial</div></div><div><div>Ig</div><div>Interglacial</div></div><div><div>Te</div><div>Tertiary</div></div><div><div>Ct</div><div>Cretaceous</div></div><div><div>Da</div><div>Danian</div></div></div> <td colspan="3"><div></div><div>Concrete pipe</div><div>Water level and date of observation</div><div>Backfill</div><div>Stand pipe</div><div>Bentonite filling</div><div>Sand filling</div><div>Filter</div></td>			<div></div> <div>Concrete pipe</div> <div>Water level and date of observation</div> <div>Backfill</div> <div>Stand pipe</div> <div>Bentonite filling</div> <div>Sand filling</div> <div>Filter</div>		
Definitions									
Signature	Parameter	Sym.	Unit	Definition					
	Water content	w	%	Weight of water in percent of solid matter					
	Liquid limit	w _L	%	Water content at yield point					
	Plastic limit	w _P	%	Water content at plastic limit					
	Plastic index	I _P	%	w _L - w _P					
	Volume weight	γ	kN/m ³	Ratio between total weight and total volume					
	Loss by combustion	gl	%	Weight loss of combustion in percent of solid matter					
	Reduced loss by combustion	gl _{red}	%	gl - ka					
	Lime content	ka	%	Weight of CaCo ³ in percent of solid matter					
-/(+)/+/-++	Lime sample	kp	-	Reaction w. hydrochoric acid: - = no lime; (+) = low content of lime; + = limy; ++ = high content of lime					
	Shear strength	c _v	kN/m ²	Shear strength measured with a vane test in undisturbed soil					
	Shear strength, remoulded	c _{vr}	kN/m ²	Shear strength measured with a vane test in disturbed soil					
	Drilling resistance Loaded flat drill	R _{SP}	N ₂₀₀	No. of ½-rotations pr. 200 mm penetration					
	Sounding resistance Swedish penetration test	R _{RS}	N ₂₀₀	No. of strokes pr. 200 mm penetration					
	Sounding resistance Light penetration test	R _{LSD}	N ₂₀₀	No. of strokes pr. 200 mm penetration					
	Sounding resistance SPT-probe, closed/open	SPT	N ₃₀₀	No. of strokes pr. 300 mm penetration					
Date		Designed		Controlled		Approved		Dokument no.	
06.09.2002		VKJ		CTL		TBA		9003G-A4-01	
COWI		LEGEND FOR BOREHOLE LOGS						Data sheet A-1	



○	10	20	30	W (%)
▽	12	16	20	γ (kN/m ³)
○●	100	200	300	Crv, Cfv (kPa)
➤	5	10	15	qc (MPa)
Sample 11, 24, 47 and 48: Layered. Sample 17: Slightly layered				
Sample 18-23: Varved. Sample 17-24: Ice dammed lake deposits				
Sample 27: Gravels windpolished. Sample 29: Stones windpolished				
Method: 6" auger with casing				
Projection: UTM32E89				
X: 446032 (m) Y: 6257440 (m) Plan:				

Project: A224691-001 Thor offshore wind farm. Landfall site investigations

Drilled by: Geob./SNC

Date: 2021.03.08 Geologist: Geob./LC

Public No.:

Borehole: B/CPT1

Prepared by: LNJE

Checked by: TKS Approved by: HRMO

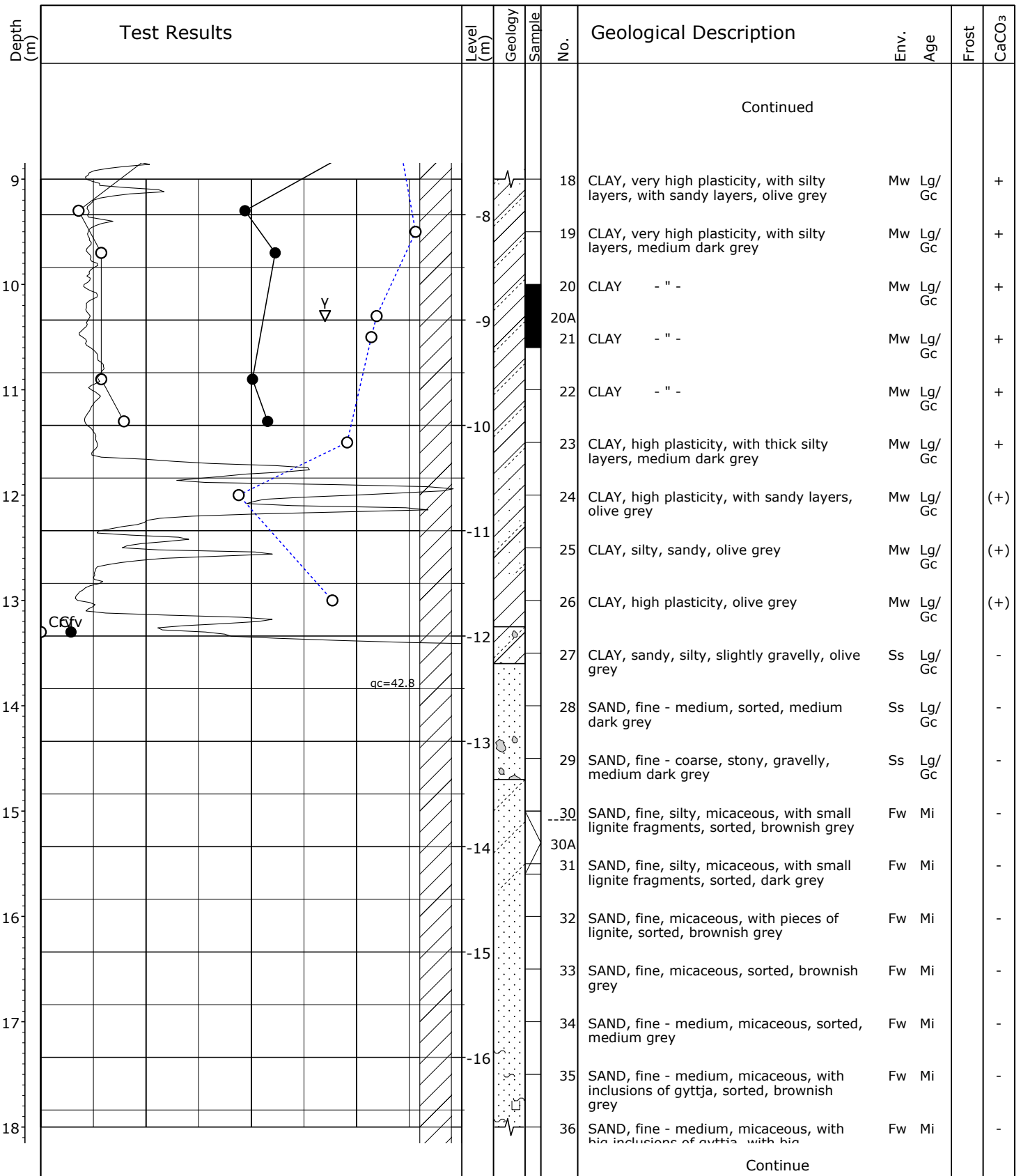
Date: 2021.04.16

Encl. No.: 1.1

P. 1/3

COWI

Borehole Log



○	10	20	30	W (%)	Sample 11, 24, 47 and 48: Layered. Sample 17: Slightly layered Sample 18-23: Varved. Sample 17-24: Ice dammed lake deposits Sample 27: Gravels windpolished. Sample 29: Stones windpolished Method: 6" auger with casing Projection: UTM32E89 X: 446032 (m) Y: 6257440 (m) Plan:
▽	12	16	20	γ (kN/m³)	
○●	100	200	300	C _{rv} , C _{fv} (kPa)	
➤	5	10	15	qc (MPa)	

Project: A224691-001

Thor offshore wind farm. Landfall site investigations

Drilled by: Geob./SNC

Date: 2021.03.08 Geologist: Geob./LC

Public No.:

Borehole: B/CPT1

Prepared by: LNJE

Checked by: TKS Approved by: HRMO

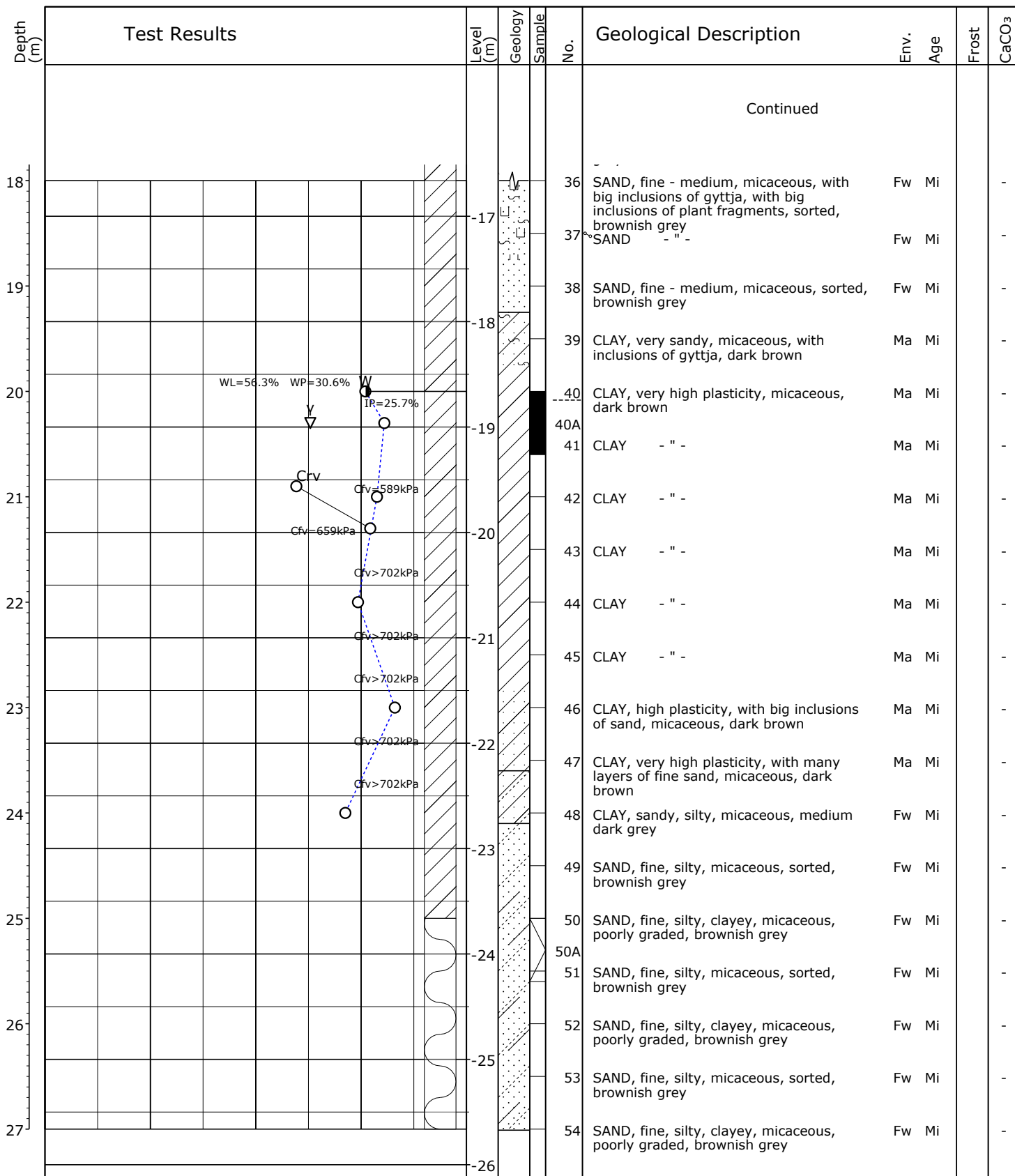
Date: 2021.04.16

Encl. No.: 1.1

P. 2/3

COWI

Borehole Log



○	10	20	30	W (%)
▽	12	16	20	γ (kN/m ³)
○●	100	200	300	C _{rv} , C _{fv} (kPa)
➤	5	10	15	qc (MPa)

Sample 11, 24, 47 and 48: Layered. Sample 17: Slightly layered
 Sample 18-23: Varved. Sample 17-24: Ice dammed lake deposits
 Sample 27: Gravels windpolished. Sample 29: Stones windpolished

Method: 6" auger with casing
 Projection: UTM32E89
 X: 446032 (m) Y: 6257440 (m) Plan:

Project: A224691-001 Thor offshore wind farm. Landfall site investigations

Drilled by: Geob./SNC

Date: 2021.03.08 Geologist: Geob./LC

Public No.:

Borehole: B/CPT1

Prepared by: LNJE

Checked by: TKS Approved by: HRMO

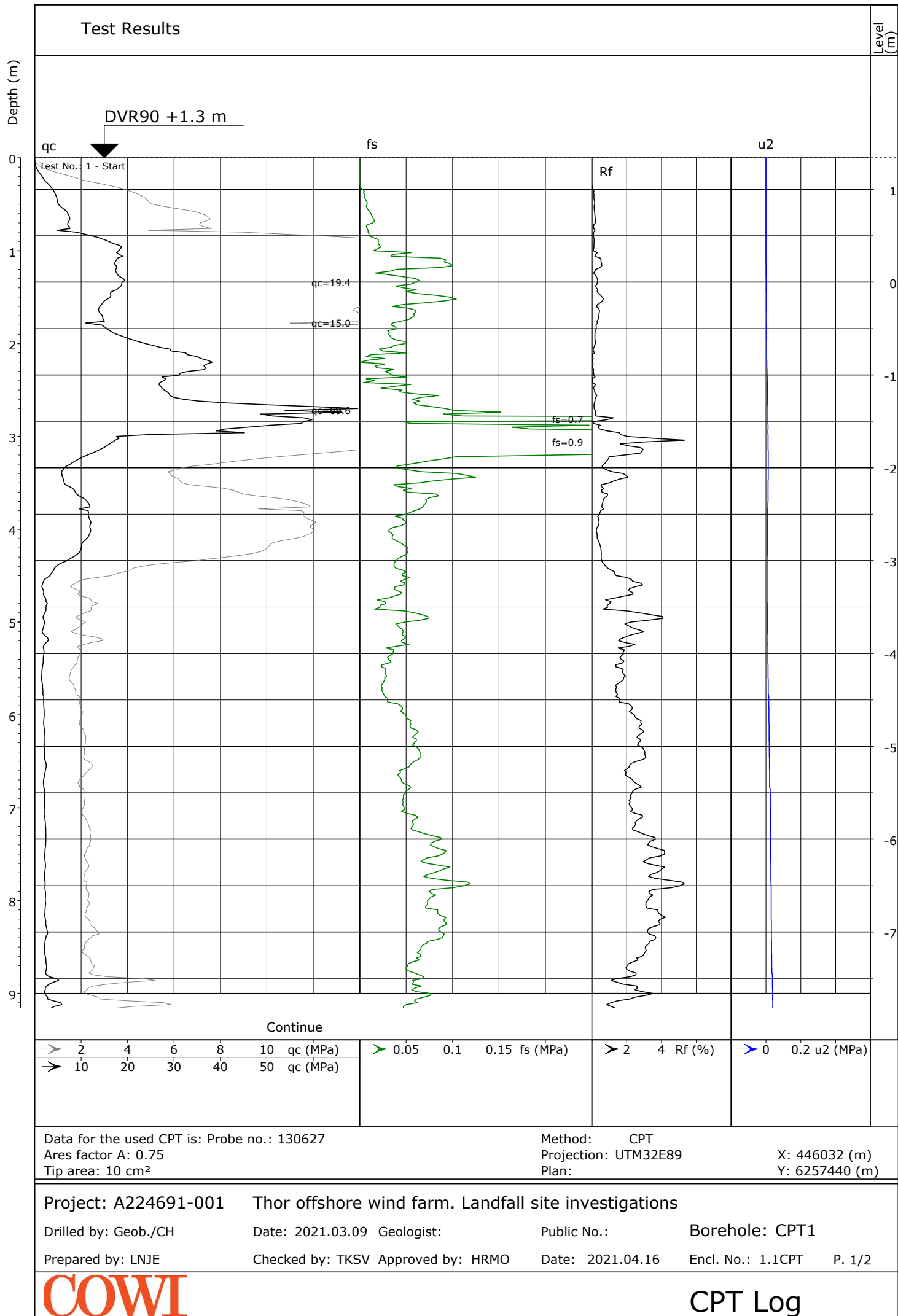
Date: 2021.04.16

Encl. No.: 1.1

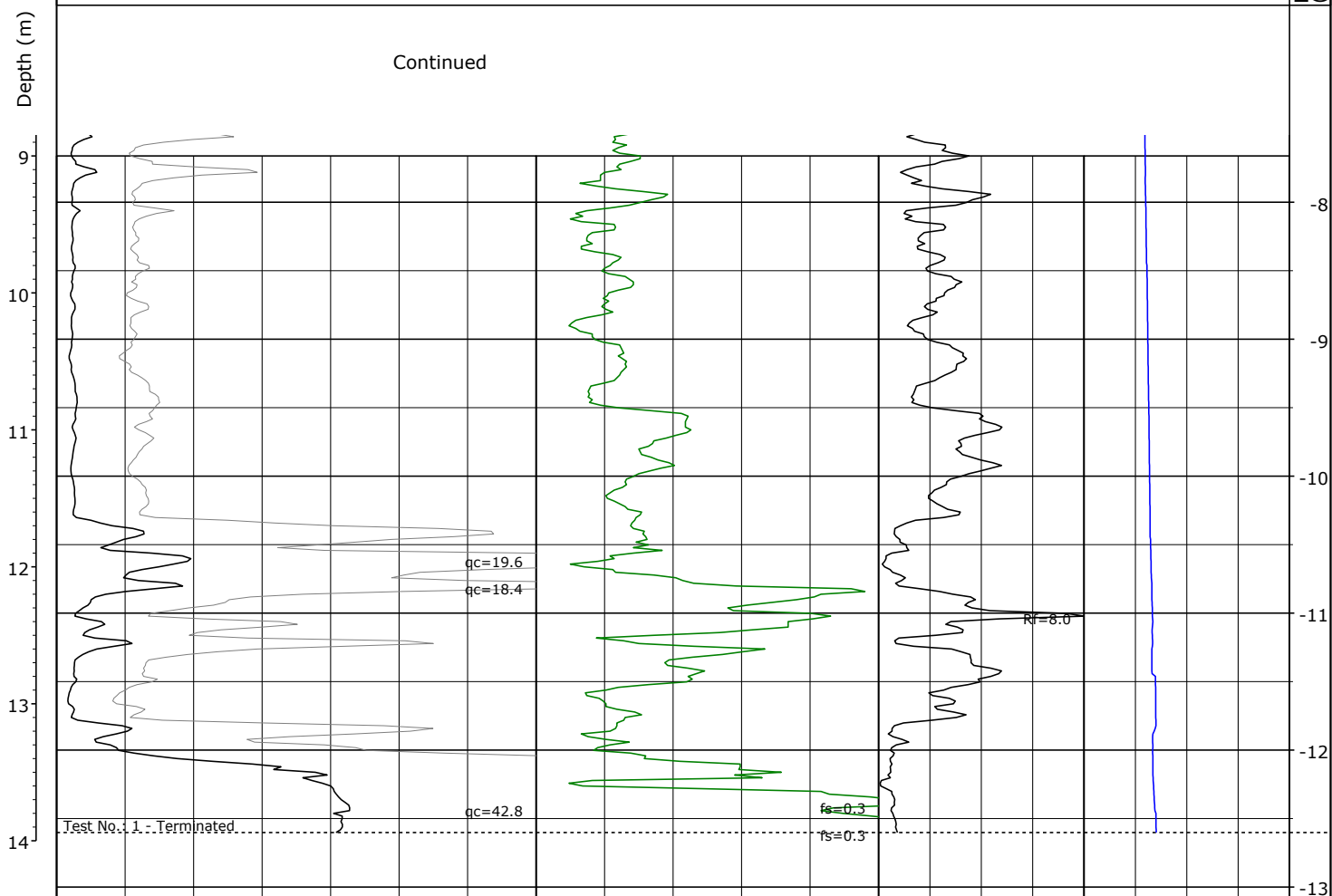
P. 3/3

COWI

Borehole Log



Test Results



→ 2 4 6 8 10 qc (MPa)	→ 0.05 0.1 0.15 fs (MPa)	→ 2 4 Rf (%)	→ 0 0.2 u2 (MPa)
→ 10 20 30 40 50 qc (MPa)			

Data for the used CPT is: Probe no.: 130627
 Ares factor A: 0.75
 Tip area: 10 cm²

Method: CPT
 Projection: UTM32E89
 Plan:
 X: 446032 (m)
 Y: 6257440 (m)

Project: A224691-001 Thor offshore wind farm. Landfall site investigations

Drilled by: Geob./CH

Date: 2021.03.09 Geologist:

Public No.:

Borehole: CPT1

Prepared by: LNJE

Checked by: TKS Approved by: HRMO

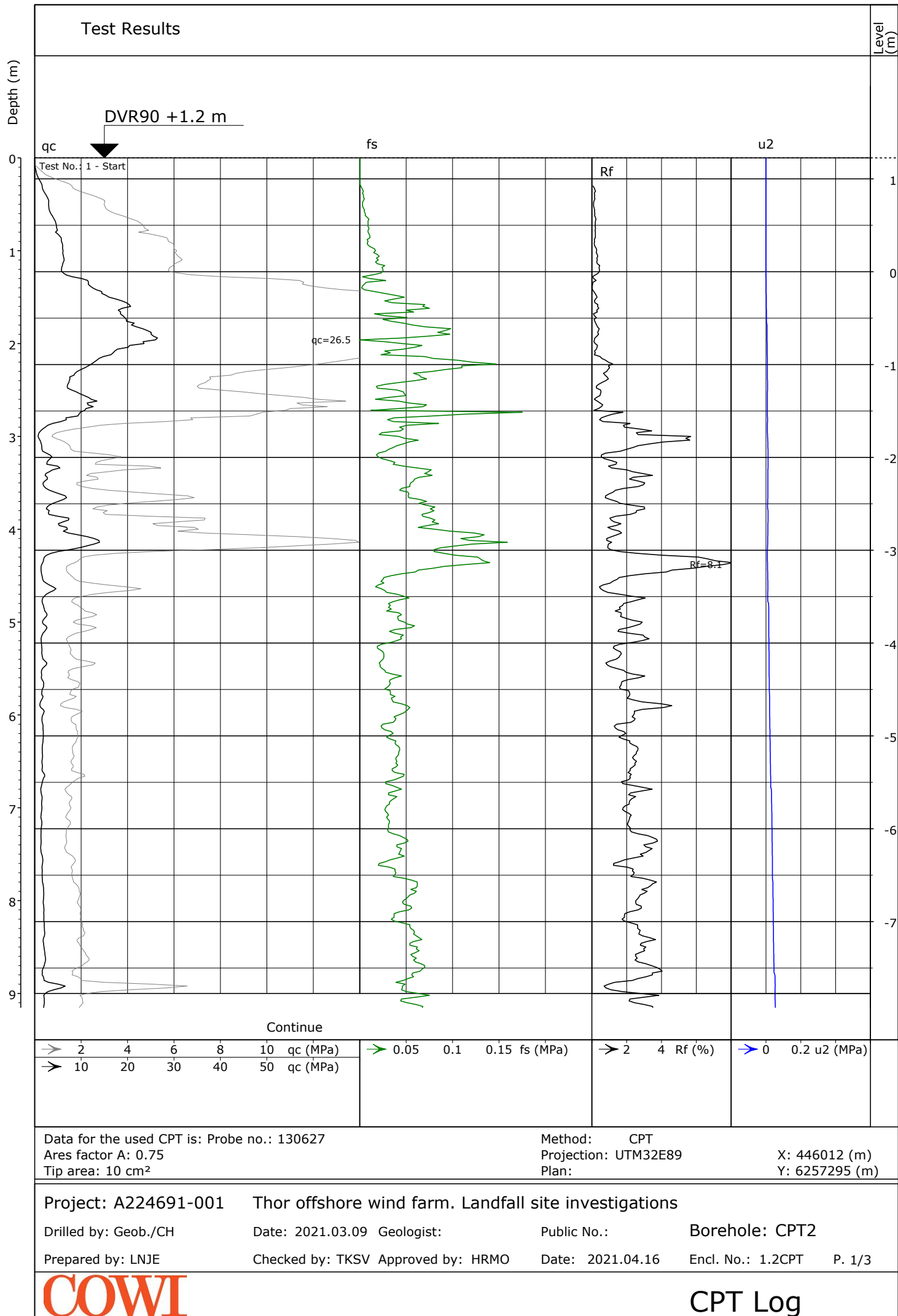
Date: 2021.04.16

Encl. No.: 1.1CPT

P. 2/2

COWI

CPT Log

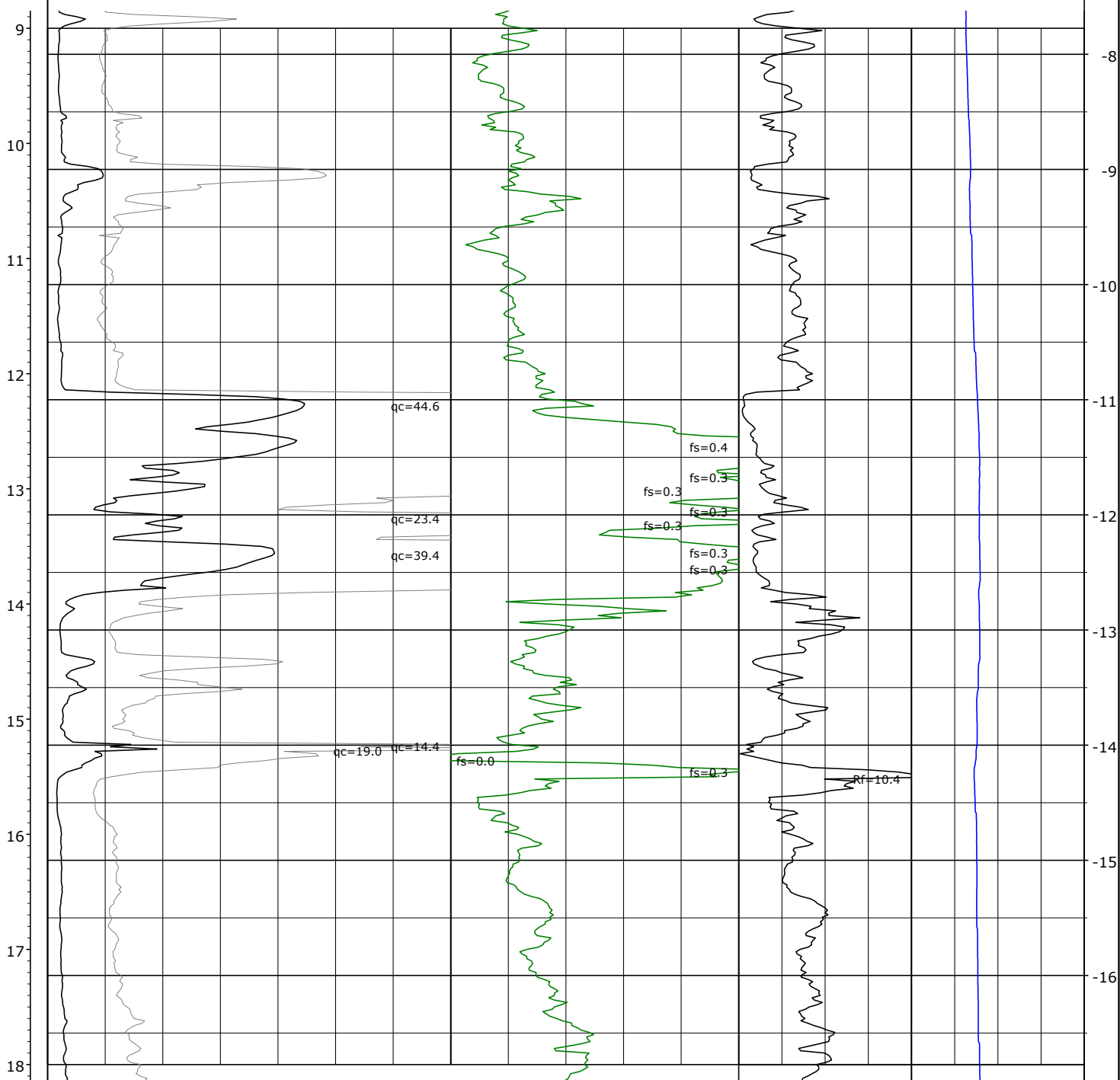


Test Results

Continued

Depth (m)

Level (m)



Continue

→ 2 4 6 8 10 qc (MPa) → 0.05 0.1 0.15 fs (MPa) → 2 4 Rf (%) → 0 0.2 u2 (MPa)
→ 10 20 30 40 50 qc (MPa)

Data for the used CPT is: Probe no.: 130627
Ares factor A: 0.75
Tip area: 10 cm²

Method: CPT
Projection: UTM32E89
Plan:
X: 446012 (m)
Y: 6257295 (m)

Project: A224691-001 Thor offshore wind farm. Landfall site investigations

Drilled by: Geob./CH

Date: 2021.03.09 Geologist:

Public No.:

Borehole: CPT2

Prepared by: LNJE

Checked by: TKS Approved by: HRMO

Date: 2021.04.16

Encl. No.: 1.2CPT

P. 2/3

COWI

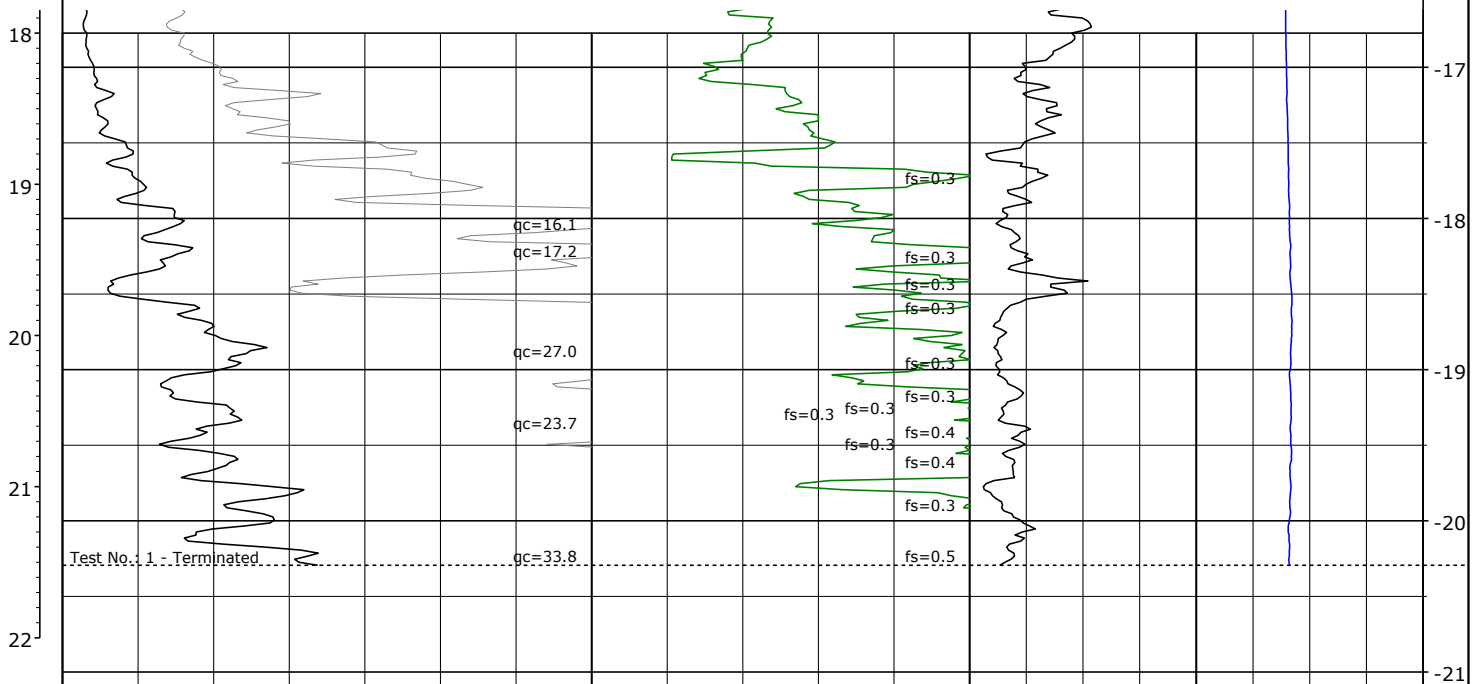
CPT Log

Test Results

Continued

Depth (m)

Level (m)



→ 2 4 6 8 10 qc (MPa)	→ 0.05 0.1 0.15 fs (MPa)	→ 2 4 Rf (%)	→ 0 0.2 u2 (MPa)
→ 10 20 30 40 50 qc (MPa)			

Data for the used CPT is: Probe no.: 130627
 Ares factor A: 0.75
 Tip area: 10 cm²

Method: CPT
 Projection: UTM32E89
 Plan:
 X: 446012 (m)
 Y: 6257295 (m)

Project: A224691-001 Thor offshore wind farm. Landfall site investigations

Drilled by: Geob./CH	Date: 2021.03.09	Geologist:	Public No.:	Borehole: CPT2
Prepared by: LNJE	Checked by: TKS	Approved by: HRMO	Date: 2021.04.16	Encl. No.: 1.2CPT P. 3/3



CPT Log

Test Results

Depth (m)

Level (m)

DVR90 +3.7 m

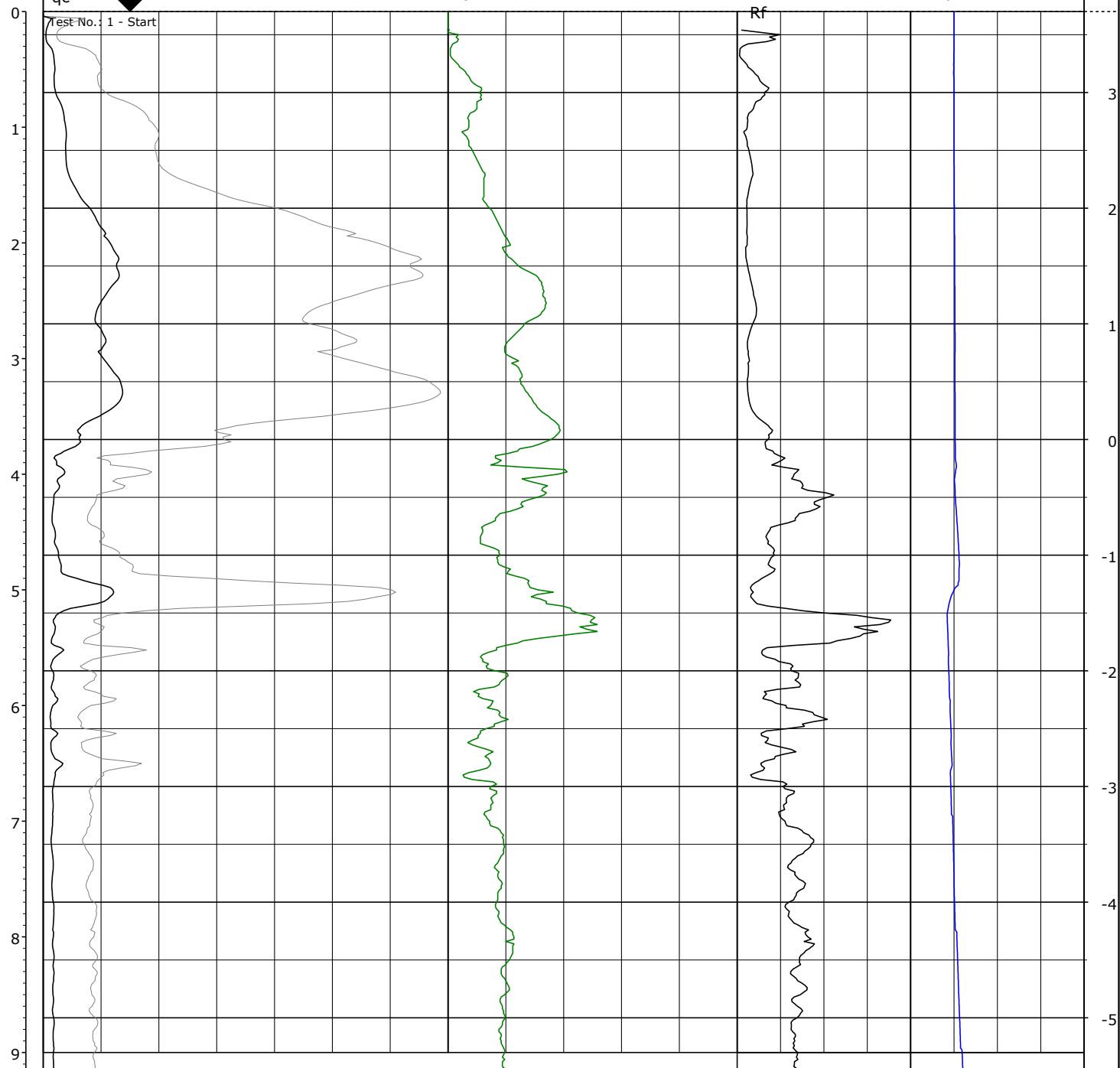
qc

fs

Rf

u2

Test No.: 1 - Start



Continue

→ 2 4 6 8 10 qc (MPa) → 0.05 0.1 0.15 fs (MPa) → 2 4 Rf (%) → 0 0.2 u2 (MPa)
 → 10 20 30 40 50 qc (MPa)

Data for the used CPT is: Probe no.: 200636
 Ares factor A: 0.75
 Tip area: 15 cm²

Method: CPT
 Projection: UTM32E89 X: 446239 (m)
 Plan: Y: 6257460 (m)

Project: A224691-001 Thor offshore wind farm. Landfall site investigations

Drilled by: Geob./CH

Date: 2021.03.09 Geologist:

Public No.:

Borehole: CPT3

Prepared by: LNJE

Checked by: TKS Approved by: HRMO

Date: 2021.04.16

Encl. No.: 1.3CPT

P. 1/2

COWI

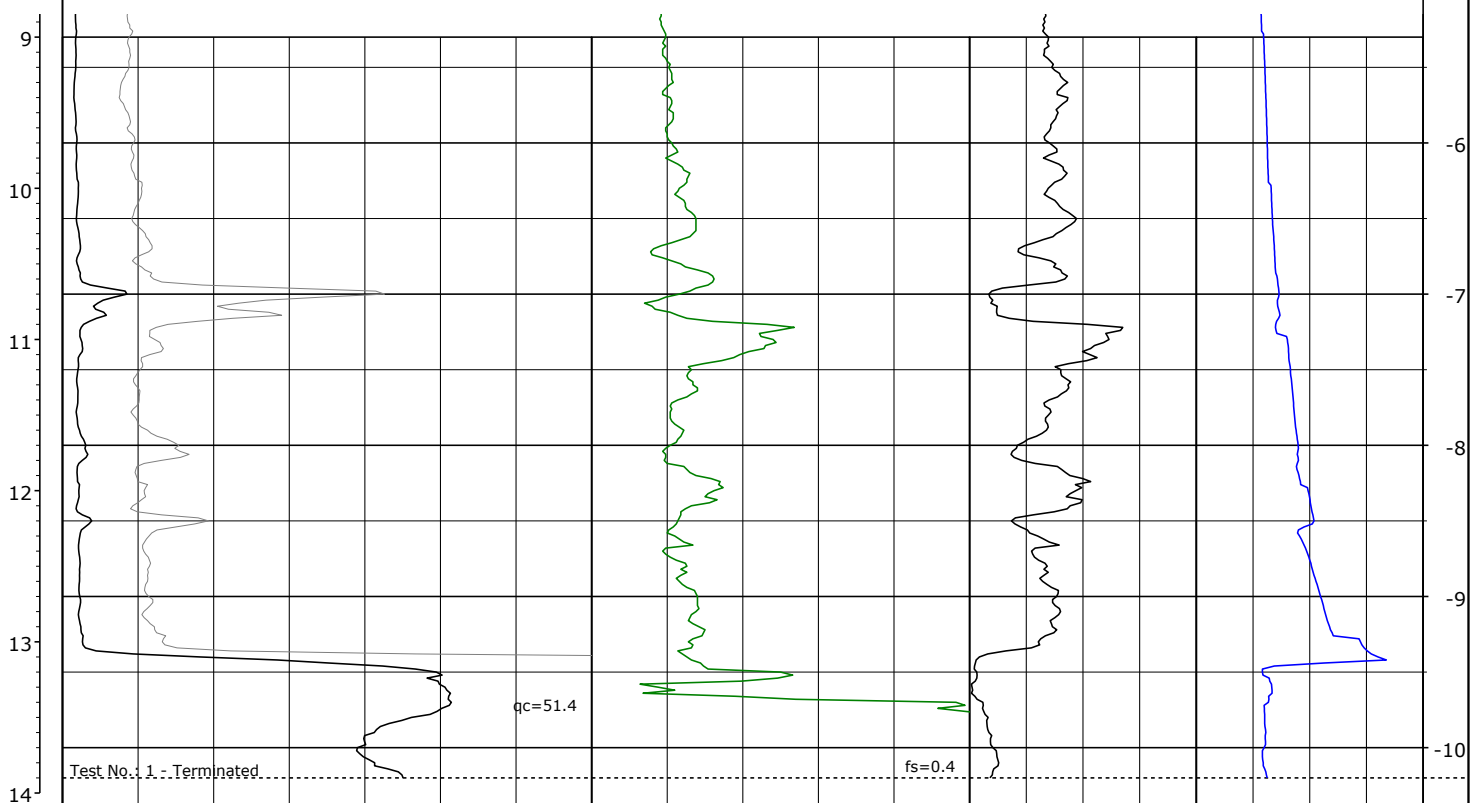
CPT Log

Test Results

Depth (m)

Level (m)

Continued



→ 2 4 6 8 10 qc (MPa)	→ 0.05 0.1 0.15 fs (MPa)	→ 2 4 Rf (%)	→ 0 0.2 u2 (MPa)
→ 10 20 30 40 50 qc (MPa)			

Data for the used CPT is: Probe no.: 200636
 Ares factor A: 0.75
 Tip area: 15 cm²

Method: CPT
 Projection: UTM32E89
 Plan:
 X: 446239 (m)
 Y: 6257460 (m)

Project: A224691-001 Thor offshore wind farm. Landfall site investigations

Drilled by: Geob./CH

Date: 2021.03.09 Geologist:

Public No.:

Borehole: CPT3

Prepared by: LNJE

Checked by: TKS Approved by: HRMO

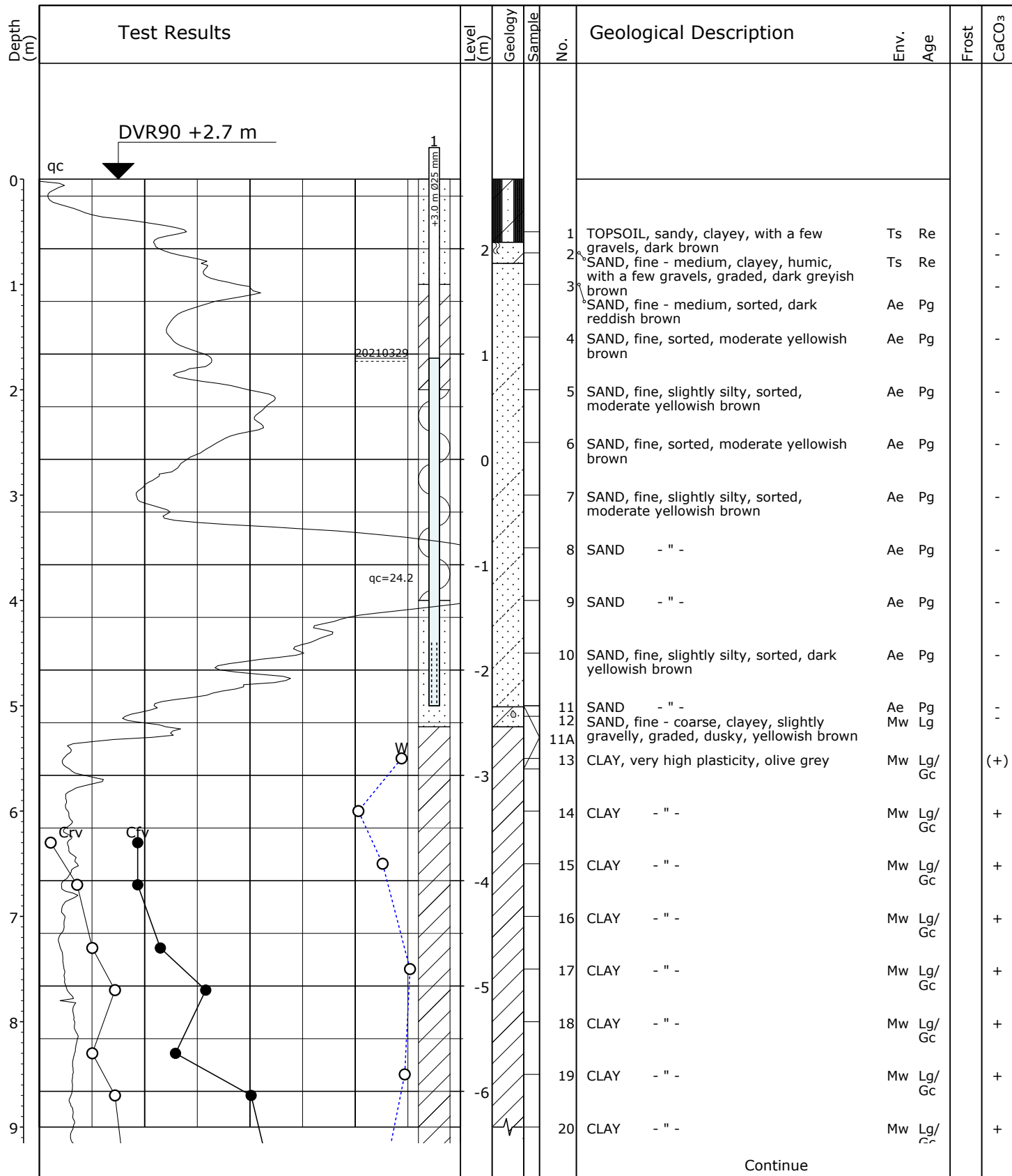
Date: 2021.04.16

Encl. No.: 1.3CPT

P. 2/2

COWI

CPT Log



○	10	20	30	W (%)	Sample 21-25 and 31: Varved
▽	12	16	20	γ (kN/m ³)	Sample 21-25 and 31: Ice dammed lake deposits
○●	100	200	300	C _v , C _{fv} (kPa)	Sample 50: Layered
▼	10	20	30	N (Blows/30 cm)	
➔	5	10	15	qc (MPa)	
					Method: 6" auger with casing
					Projection: UTM32E89
					X: 446221 (m) Y: 6257293 (m) Plan:

Project: A224691-001 Thor offshore wind farm. Landfall site investigations

Drilled by: Geob./SNC

Date: 2021.03.11 Geologist: Geob./LC

Public No.:

Borehole: B/CPT4

Prepared by: LNJE

Checked by: TKS Approved by: HRMO

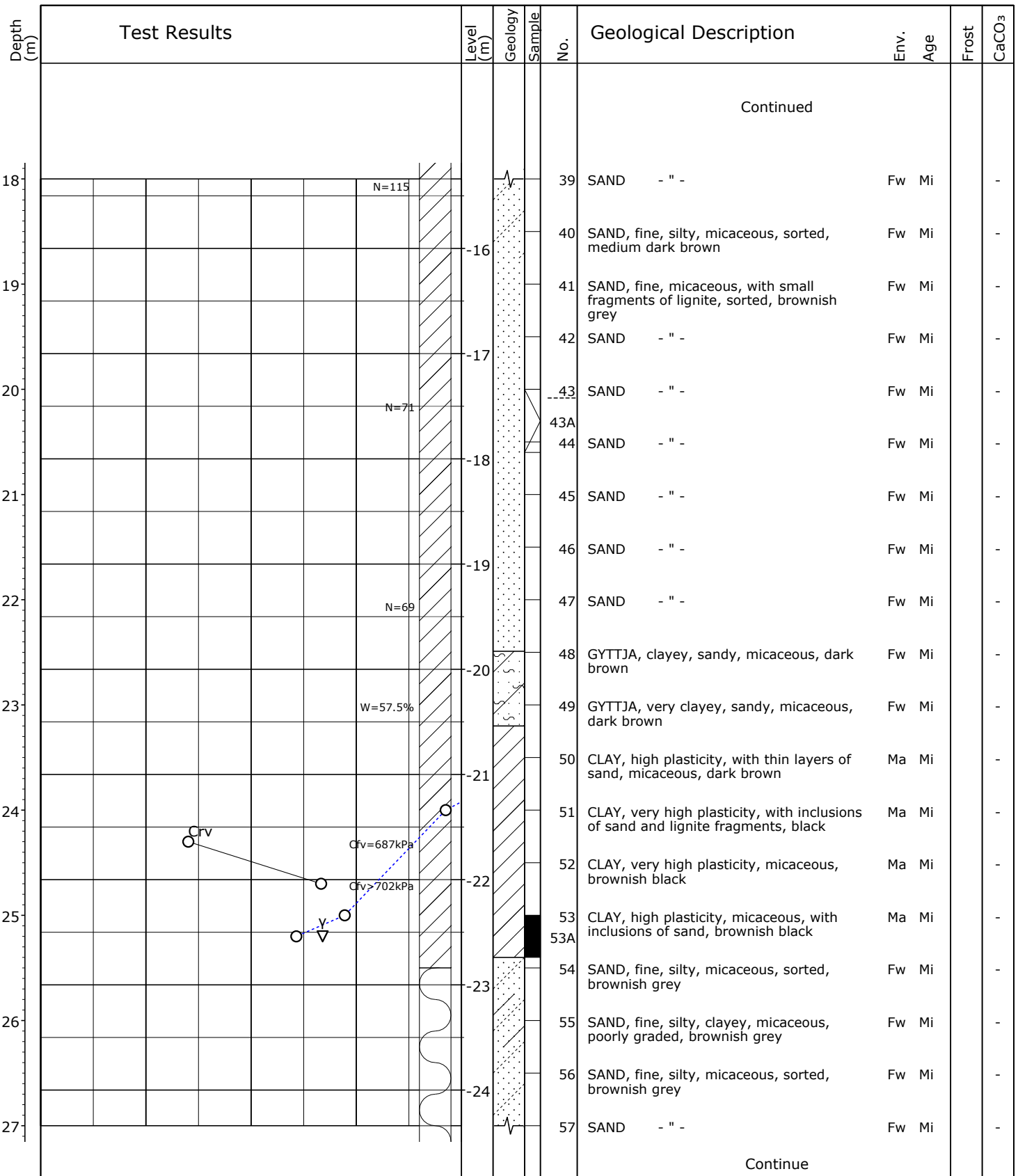
Date: 2021.04.16

Encl. No.: 1.4

P. 1/4

COWI

Borehole Log



○	10	20	30	W (%)	Sample 21-25 and 31: Varved
▽	12	16	20	γ (kN/m ³)	Sample 21-25 and 31: Ice dammed lake deposits
○●	100	200	300	Crv, Cfv (kPa)	Sample 50: Layered
▼	10	20	30	N (Blows/30 cm)	
➔	5	10	15	qc (MPa)	
					Method: 6" auger with casing
					Projection: UTM32E89
					X: 446221 (m) Y: 6257293 (m) Plan:

Project: A224691-001 Thor offshore wind farm. Landfall site investigations

Drilled by: Geob./SNC Date: 2021.03.11 Geologist: Geob./LC Public No.: Borehole: B/CPT4

Prepared by: LNJE Checked by: TKS Approved by: HRMO Date: 2021.04.16 Encl. No.: 1.4 P. 3/4



Borehole Log

[illegible]

Test Results

Depth (m)

DVR90 +2.7 m

qc

fs

Rf

u2

Test No.: 1 - Start

qc=24.2

Rf=8.6

Continue

→ 2 4 6 8 10 qc (MPa)
→ 10 20 30 40 50 qc (MPa)

→ 0.05 0.1 0.15 fs (MPa)

→ 2 4 Rf (%)

→ 0 0.2 u2 (MPa)

Data for the used CPT is: Probe no.: 130627
Ares factor A: 0.75
Tip area: 10 cm²

Method: CPT
Projection: UTM32E89
Plan:

X: 446221 (m)
Y: 6257293 (m)

Project: A224691-001 Thor offshore wind farm. Landfall site investigations

Drilled by: Geob./CH

Date: 2021.03.09 Geologist:

Public No.:

Borehole: CPT4

Prepared by: LNJE

Checked by: TKS Approved by: HRMO

Date: 2021.04.16

Encl. No.: 1.4CPT

P. 1/2

COWI

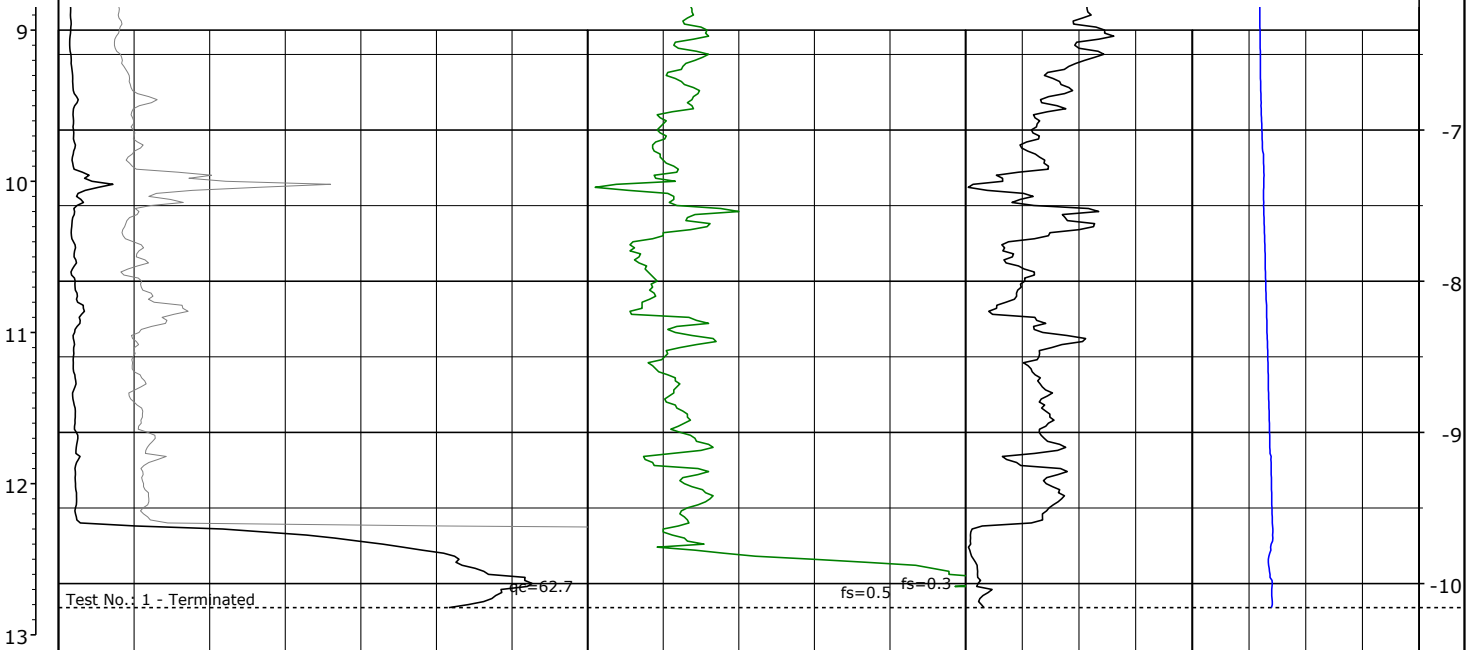
CPT Log

Test Results

Depth (m)

Level (m)

Continued



→ 2 4 6 8 10 qc (MPa)	→ 0.05 0.1 0.15 fs (MPa)	→ 2 4 Rf (%)	→ 0 0.2 u2 (MPa)
→ 10 20 30 40 50 qc (MPa)			

Data for the used CPT is: Probe no.: 130627
 Ares factor A: 0.75
 Tip area: 10 cm²

Method: CPT
 Projection: UTM32E89
 Plan:
 X: 446221 (m)
 Y: 6257293 (m)

Project: A224691-001 Thor offshore wind farm. Landfall site investigations

Drilled by: Geob./CH

Date: 2021.03.09 Geologist:

Public No.:

Borehole: CPT4

Prepared by: LNJE

Checked by: TKS Approved by: HRMO

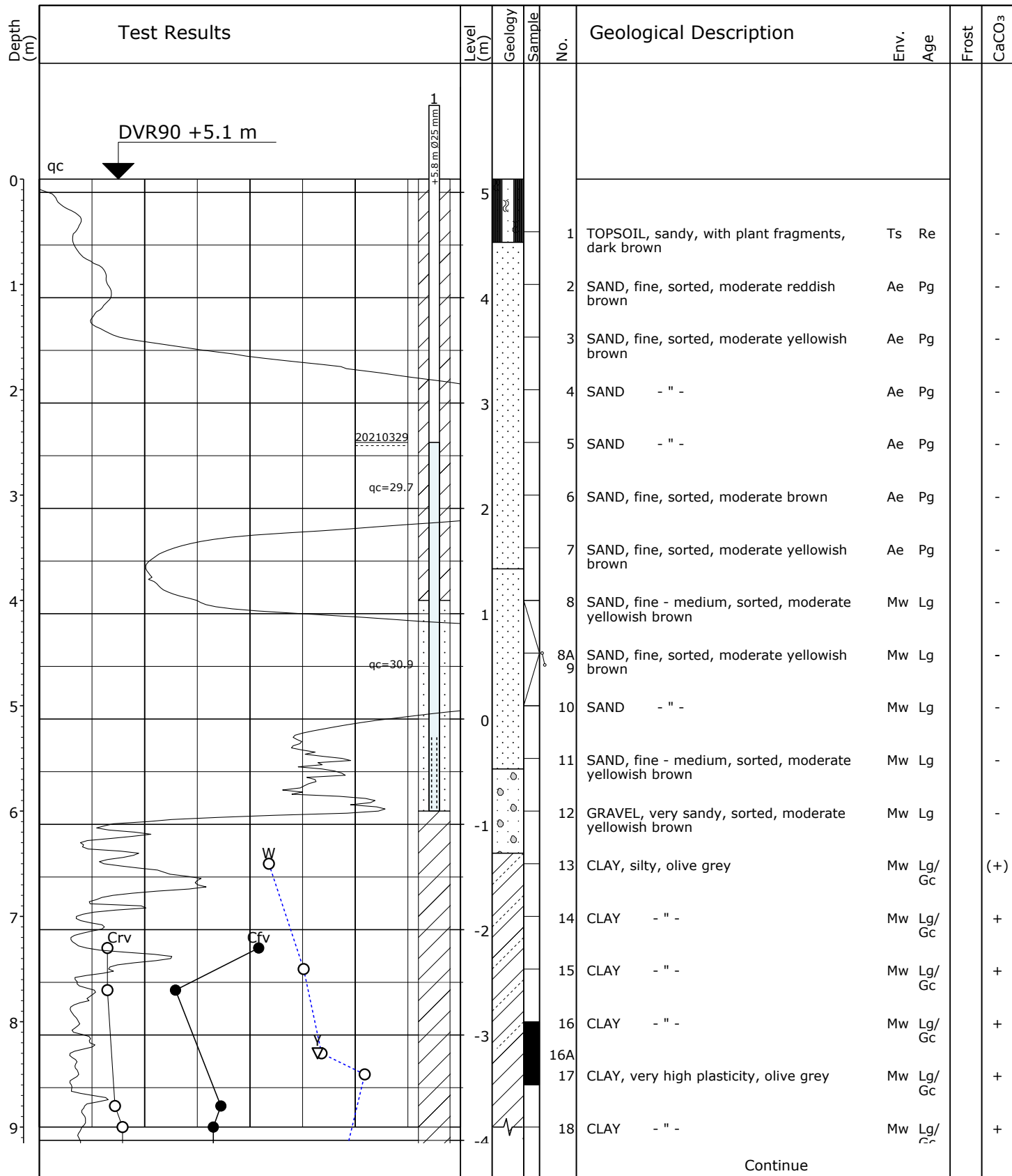
Date: 2021.04.16

Encl. No.: 1.4CPT

P. 2/2

COWI

CPT Log



○	10	20	30	W (%)	Sample 14-16 and 23-28: Varved
▽	12	16	20	γ (kN/m ³)	Sample 14-16 and 23-28: Ice dammed lake deposits
○●	100	200	300	Crv, Cfv (kPa)	Sample 36-47: Quartz sand
▼	10	20	30	N (Blows/30 cm)	
➤	5	10	15	qc (MPa)	
					Method: 6" auger with casing
					Projection: UTM32E89
					X: 446407 (m) Y: 6257482 (m) Plan:

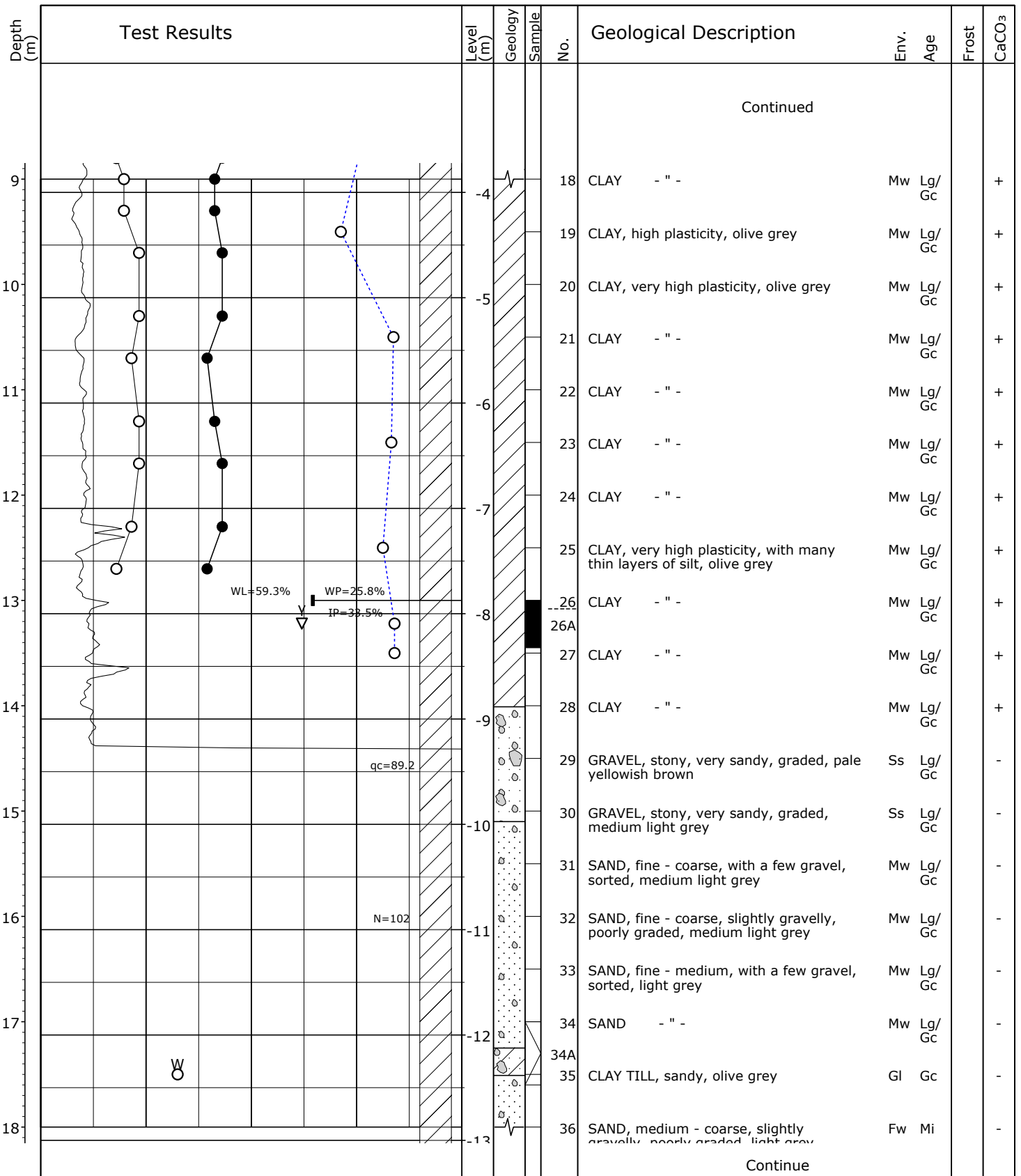
Project: A224691-001 Thor offshore wind farm. Landfall site investigations

Drilled by: Geob./MGS Date: 2021.03.16 Geologist: Geob./LC Public No.: Borehole: B/CPT5

Prepared by: LNJE Checked by: TKS Approved by: HRMO Date: 2021.04.16 Encl. No.: 1.5 P. 1/4



Borehole Log



○	10	20	30	W (%)	Sample 14-16 and 23-28: Varved
▽	12	16	20	γ (kN/m³)	Sample 14-16 and 23-28: Ice dammed lake deposits
○●	100	200	300	C _{rv} , C _{fv} (kPa)	Sample 36-47: Quartz sand
▼	10	20	30	N (Blows/30 cm)	
➤	5	10	15	qc (MPa)	

Method: 6" auger with casing
Projection: UTM32E89
X: 446407 (m) Y: 6257482 (m) Plan:

Project: A224691-001 Thor offshore wind farm. Landfall site investigations

Drilled by: Geob./MGS

Date: 2021.03.16 Geologist: Geob./LC

Public No.:

Borehole: B/CPT5

Prepared by: LNJE

Checked by: TKS Approved by: HRMO

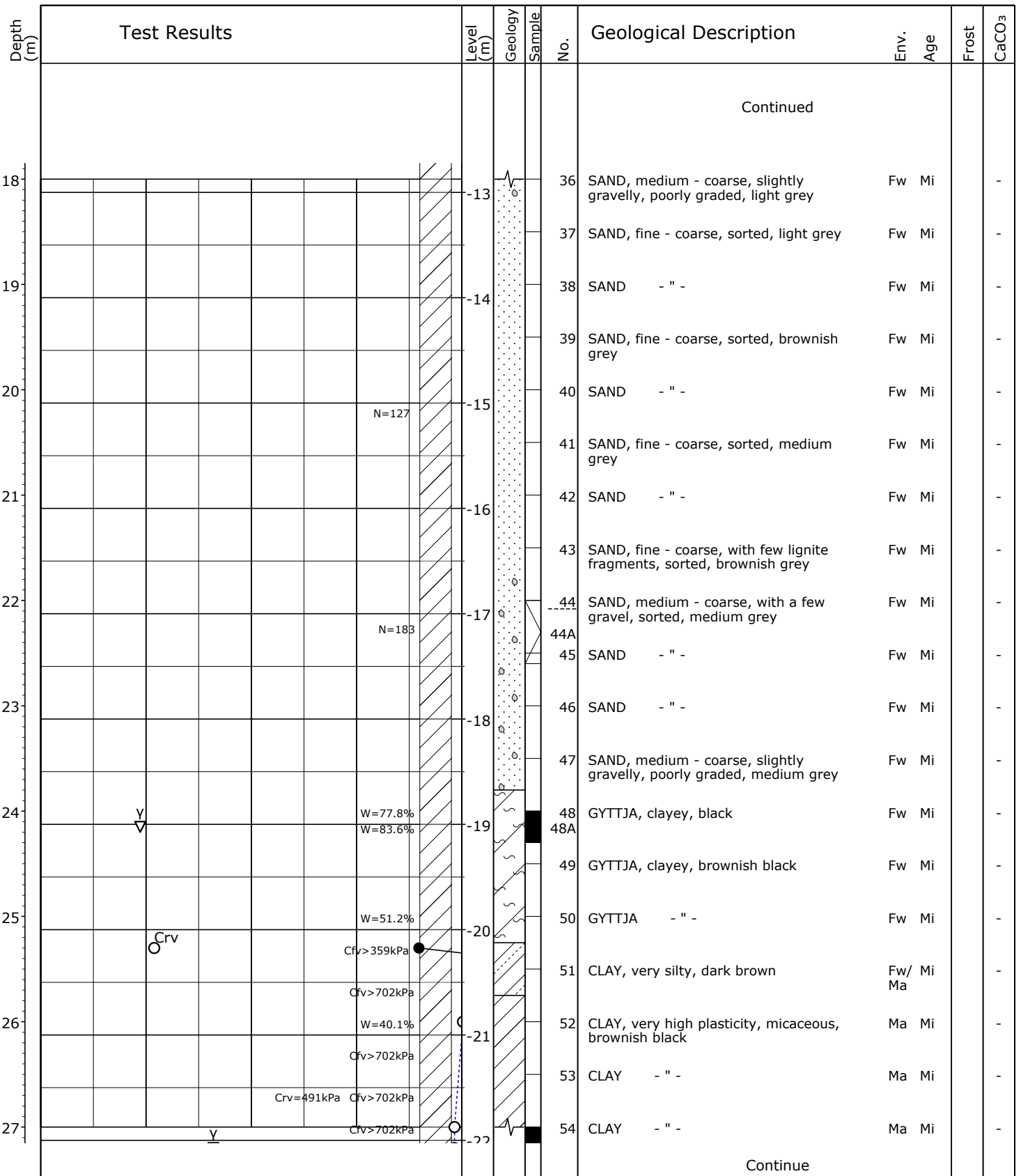
Date: 2021.04.16

Encl. No.: 1.5

P. 2/4

COWI

Borehole Log



○	10	20	30	W (%)	Sample 14-16 and 23-28: Varved
▽	12	16	20	γ (kN/m ³)	Sample 14-16 and 23-28: Ice dammed lake deposits
○●	100	200	300	Crv, Cfv (kPa)	Sample 36-47: Quartz sand
▼	10	20	30	N (Blows/30 cm)	
➔	5	10	15	qc (MPa)	
Method: 6" auger with casing					
Projection: UTM32E89					
X: 446407 (m) Y: 6257482 (m) Plan:					

Project: A224691-001 Thor offshore wind farm. Landfall site investigations

Drilled by: Geob./MGS Date: 2021.03.16 Geologist: Geob./LC Public No.: Borehole: B/CPT5

Prepared by: LNJE Checked by: TKS Approved by: HRMO Date: 2021.04.16 Encl. No.: 1.5 P. 3/4



Borehole Log

Test Results

Depth (m)

Level (m)

DVR90 +5.1 m

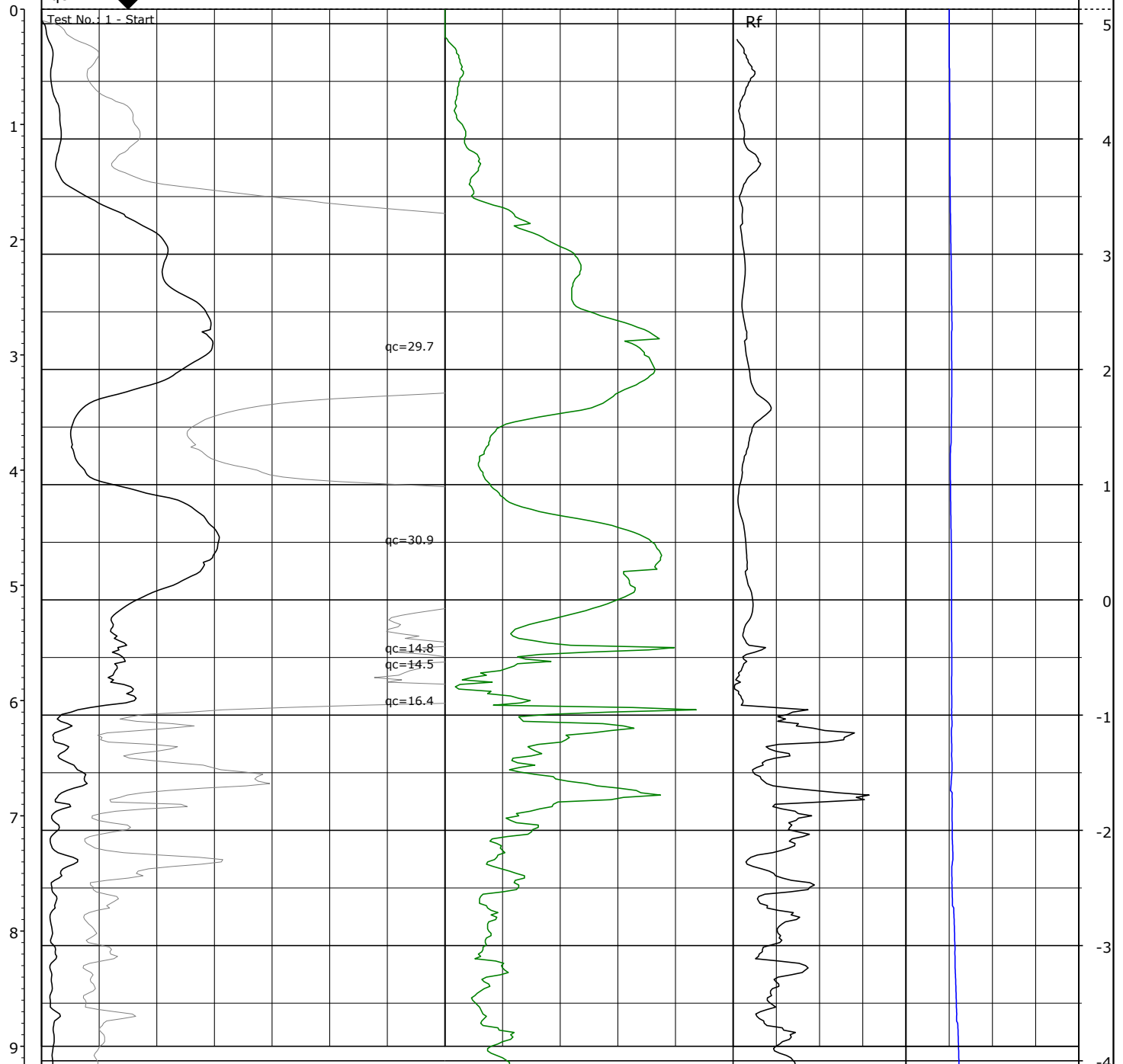
qc

fs

u2

Test No. 1 - Start

Rf



Continue

→ 2 4 6 8 10 qc (MPa) → 0.05 0.1 0.15 fs (MPa) → 2 4 Rf (%) → 0 0.2 u2 (MPa)
→ 10 20 30 40 50 qc (MPa)

Data for the used CPT is: Probe no.: 200806
Ares factor A: 0.75
Tip area: 10 cm²

Method: CPT
Projection: UTM32E89
Plan:
X: 446407 (m)
Y: 6257482 (m)

Project: A224691-001 Thor offshore wind farm. Landfall site investigations

Drilled by: Geob./CH Date: 2021.03.09 Geologist: Public No.: Borehole: CPT5
Prepared by: LNJE Checked by: TKS Approved by: HRMO Date: 2021.04.16 Encl. No.: 1.5CPT P. 1/2

COWI

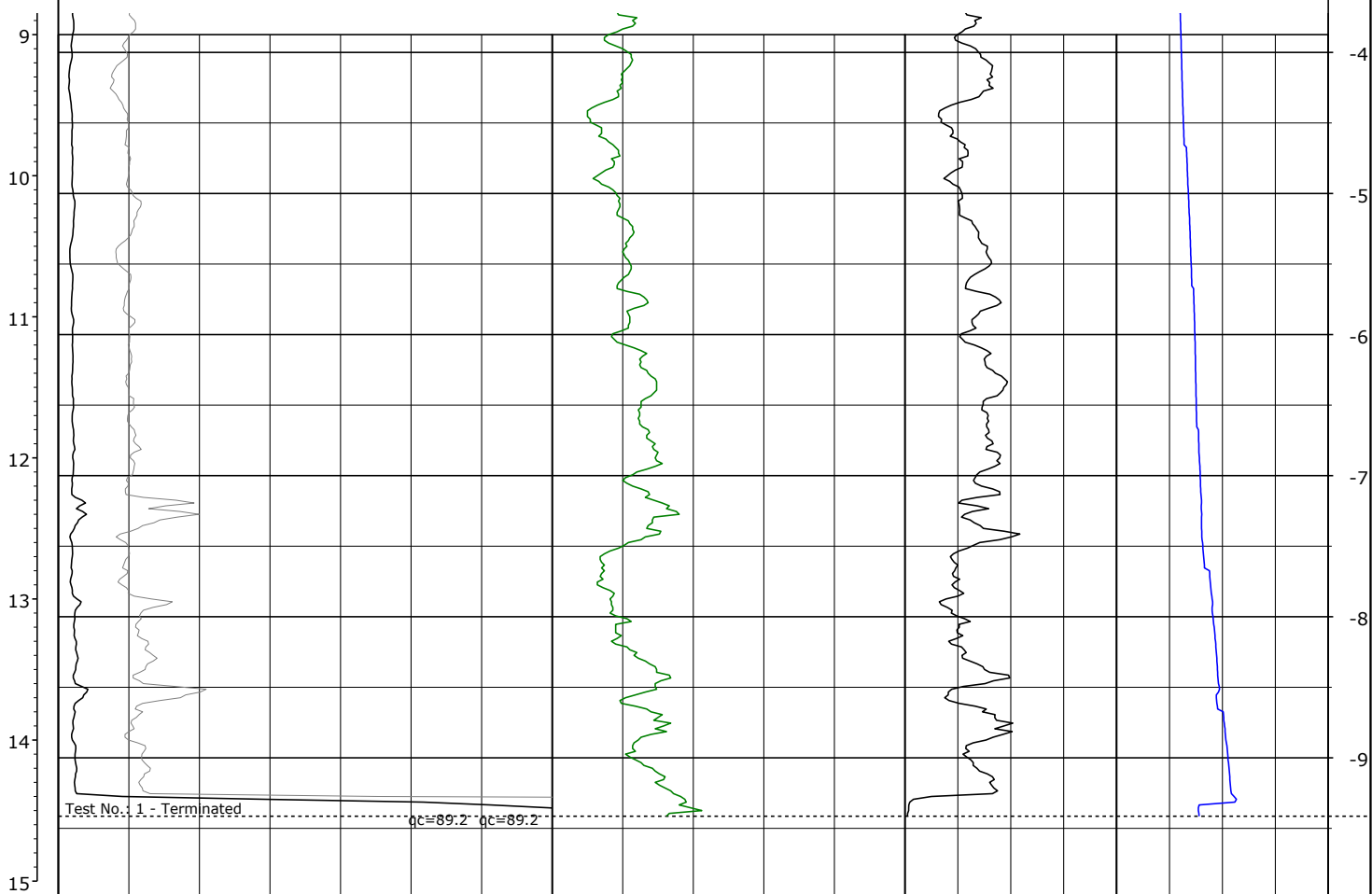
CPT Log

Test Results

Depth (m)

Level (m)

Continued



→ 2 4 6 8 10 qc (MPa)	→ 0.05 0.1 0.15 fs (MPa)	→ 2 4 Rf (%)	→ 0 0.2 u2 (MPa)
→ 10 20 30 40 50 qc (MPa)			

Data for the used CPT is: Probe no.: 200806
 Ares factor A: 0.75
 Tip area: 10 cm²

Method: CPT
 Projection: UTM32E89
 Plan:
 X: 446407 (m)
 Y: 6257482 (m)

Project: A224691-001 Thor offshore wind farm. Landfall site investigations

Drilled by: Geob./CH

Date: 2021.03.09 Geologist:

Public No.:

Borehole: CPT5

Prepared by: LNJE

Checked by: TKS Approved by: HRMO

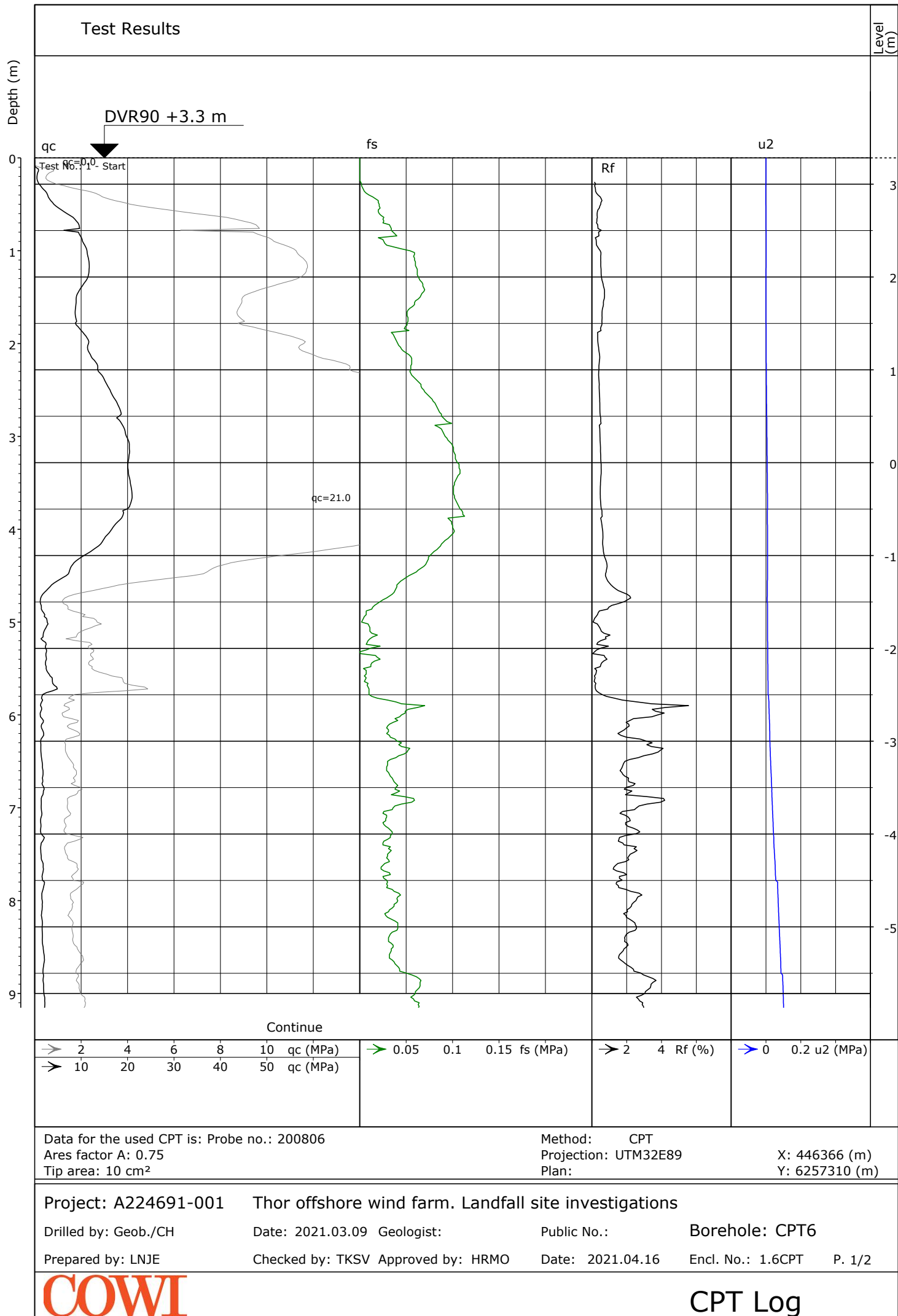
Date: 2021.04.16

Encl. No.: 1.5CPT

P. 2/2

COWI

CPT Log

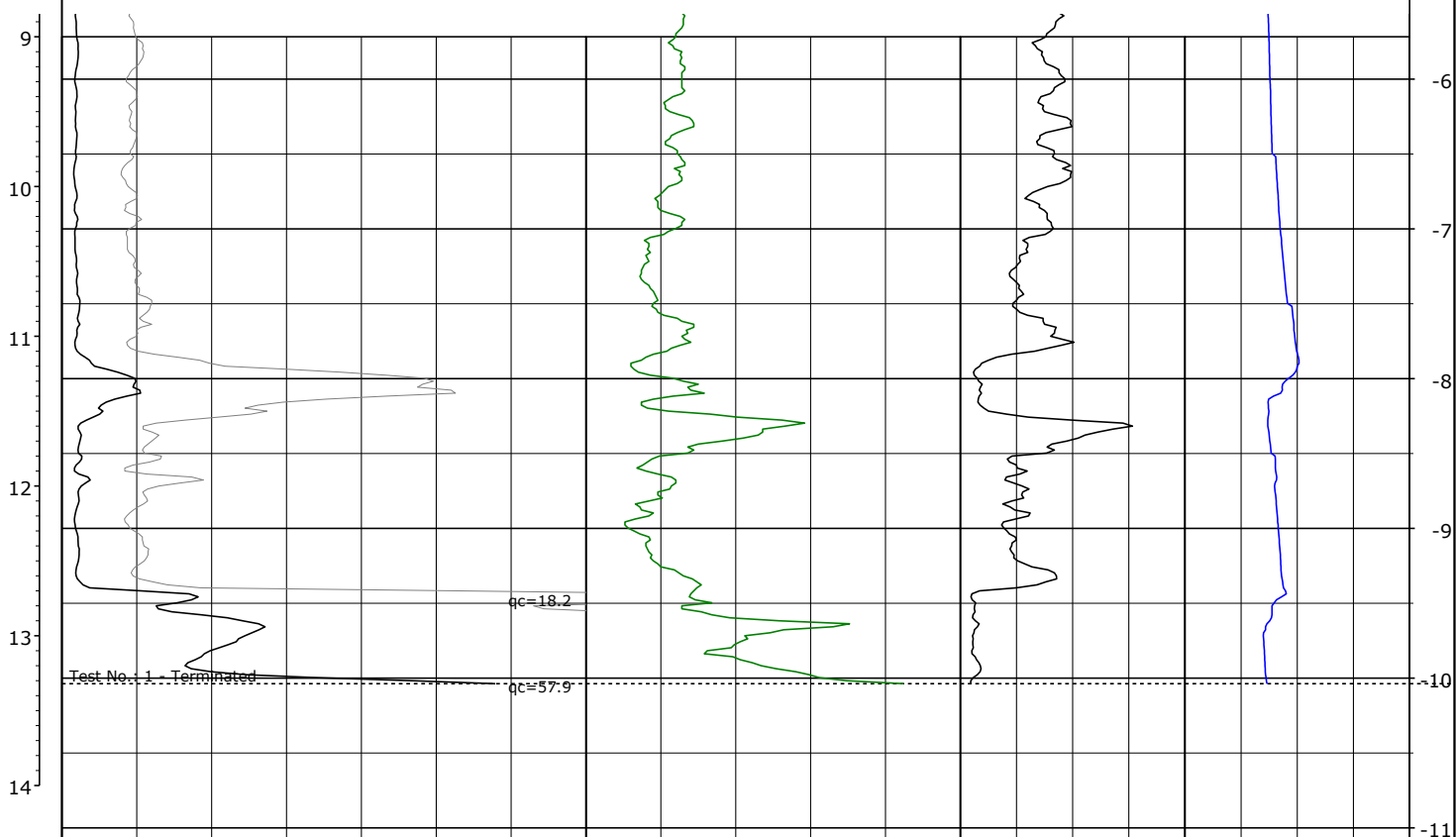


Test Results

Depth (m)

Level (m)

Continued



→ 2 4 6 8 10 q_c (MPa)	→ 0.05 0.1 0.15 f_s (MPa)	→ 2 4 R_f (%)	→ 0 0.2 u_2 (MPa)
→ 10 20 30 40 50 q_c (MPa)			

Data for the used CPT is: Probe no.: 200806
 Ares factor A: 0.75
 Tip area: 10 cm²

Method: CPT
 Projection: UTM32E89
 Plan:
 X: 446366 (m)
 Y: 6257310 (m)

Project: A224691-001 Thor offshore wind farm. Landfall site investigations

Drilled by: Geob./CH

Date: 2021.03.09 Geologist:

Public No.:

Borehole: CPT6

Prepared by: LNJE

Checked by: TKS Approved by: HRMO

Date: 2021.04.16

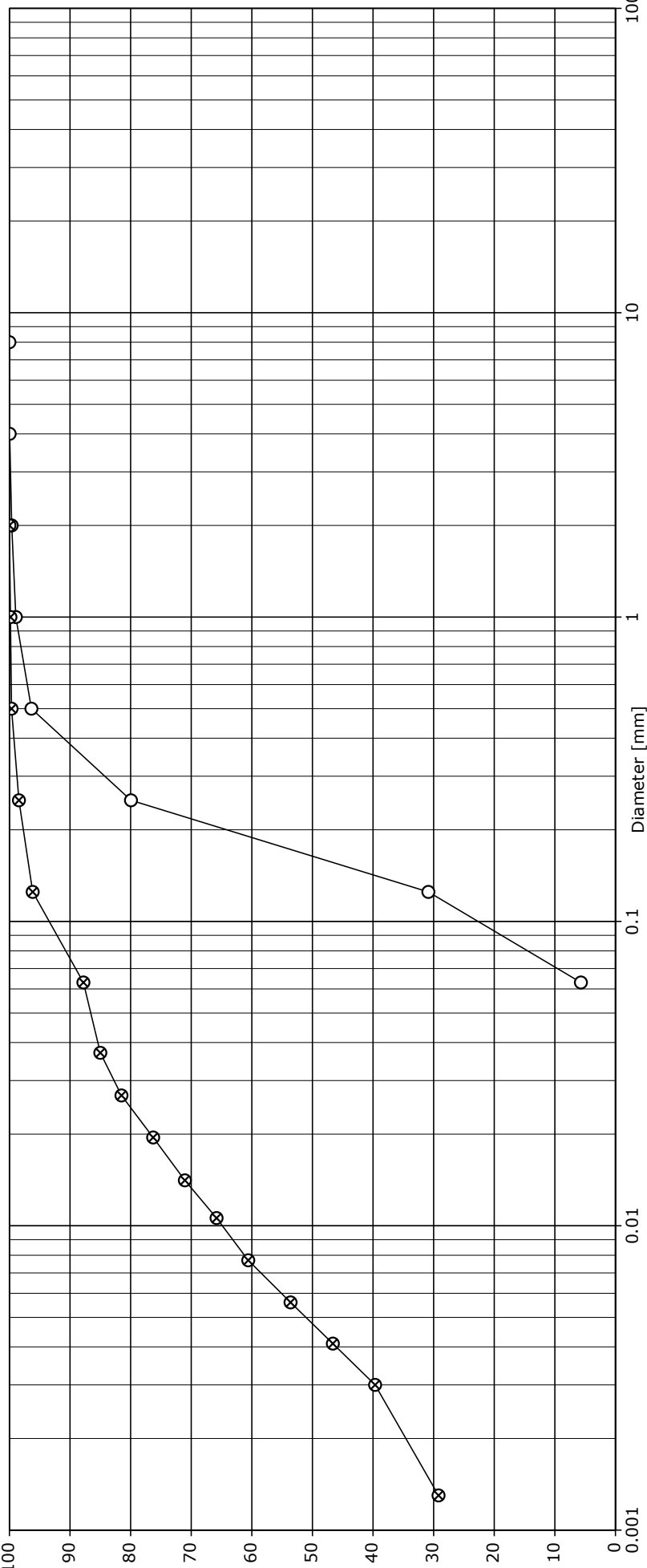
Encl. No.: 1.6CPT

P. 2/2

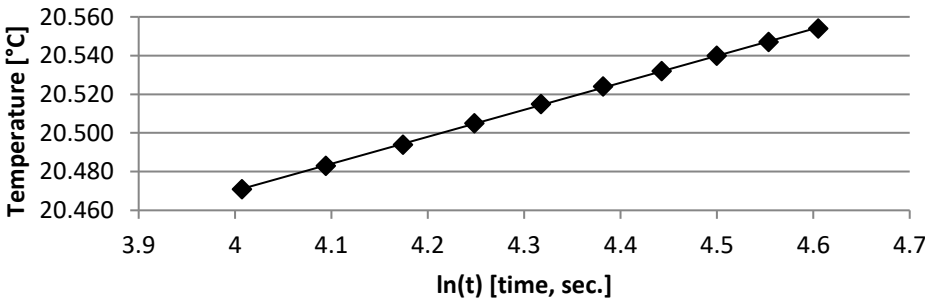
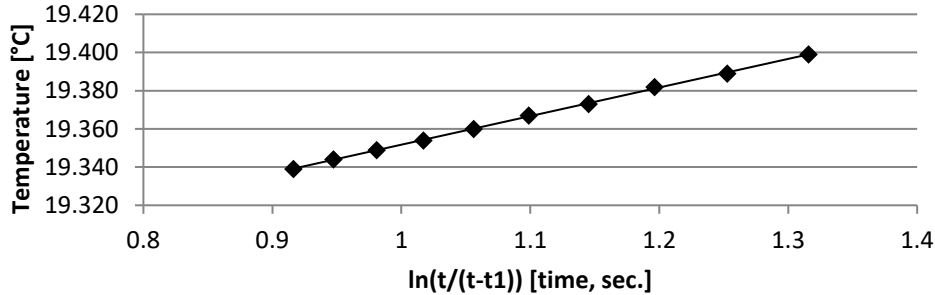
COWI

CPT Log

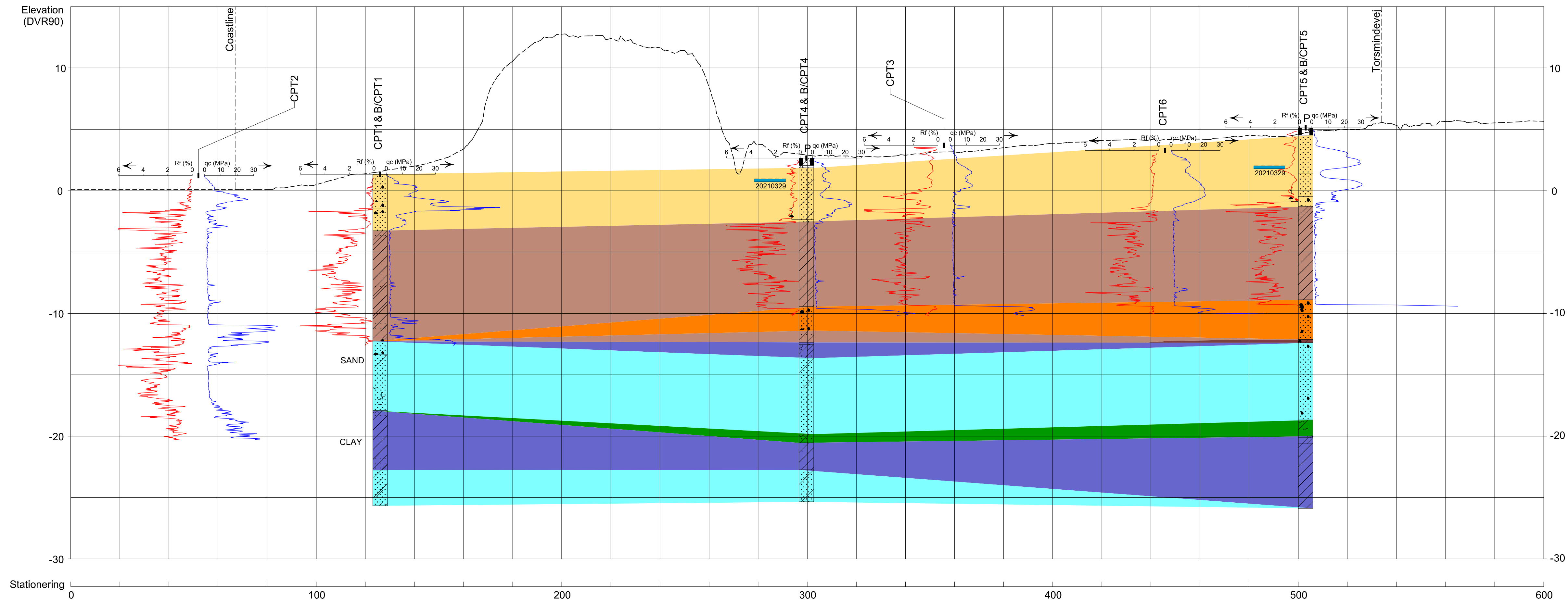
Percentage Passing [%]



Sample parameters					
Geological classification		CLAY, very high plasticity, micaceous			
Sample Preparation:		Undisturbed soil sample, Thin-Walled steel tube, $\varnothing 72\text{mm}$			
Sample diameter, D	[mm]	72	Bulk Density, ρ_m	[Mg/m ³]	1.84
Sample height, H	[mm]	26	Dry Density, ρ_d	[Mg/m ³]	1.39
Moisture content, w	[%]	32.1	Moist unit weight, γ_m	[kN/m ³]	18.1
Particle density, ρ_s (assumed)	[Mg/m ³]	2.65	Dry Unit weight, γ_d	[kN/m ³]	13.7
Initial Degree of Saturation	[%]	94	Void Ratio, e	[-]	0.90
Apparatus					
Product and model no.: Decagon KD2 Pro			Sensor: Decagon TR-1 (100 mm)		
Calibration constant, C			Heat input, Q		
	[-]	1.003		[W/m]	4.650
	Pushed	Pre-drilled	Read time		
				[min.]	5
Needle insertion method: x			Current, I		
				[A]	0.095
Test data					
<div> <div> <div>Heating data</div> <div> $y = 0.2253x + 21.735$ $R^2 = 0.9999$ </div> <div> <div>◆ Heating data</div> <div>— Linear (Heating data)</div> </div> </div> <div> <div>Cooling data</div> <div> $y = 0.2627x + 20.894$ $R^2 = 0.9998$ </div> <div> <div>◆ Cooling data</div> <div>— Linear (Cooling data)</div> </div> </div> </div>					
Test results					
Thermal Conductivity, K		[W m ⁻¹ K ⁻¹]	1.549	Thermal Resistivity, ρ	[(m K W ⁻¹)]
					0.645
Notes:					
			Thermal Conductivity		Test standard: ASTM D 5334 (2008)
Lab. tech.:	SNHS	Date:	14-04-2021	Project:	Thor offshore wind farm Landfall site
Checked:	MATP	Date:	16-04-2021	Job no.:	A224691
Approved:	HRMO	Date:	16-04-2021	Boring no.:	B/CPT1
				Sample no.:	40A
				Depth [m]:	20.0-20.6
				Revision	1.0
				Encl. no.:	1.10

Sample parameters					
Geological classification		SAND, fine, micaceous, with small fragments of lignite, sorted			
Sample Preparation:		Large bag (LB) sample compacted in 208 mm high Standard Proctor Mold			
Sample diameter, D		[mm]	102	Bulk Density, ρ_m	
Sample height, H		[mm]	208	Dry Density, ρ_d	
Moisture content, w		[%]	21.6	Moist unit weight, γ_m	
Particle density, ρ_s (assumed)		[Mg/m ³]	2.65	Dry Unit weight, γ_d	
Initial Degree of Saturation		[%]	78	Void Ratio, e	
Apparatus					
Product and model no.:			Decagon KD2 Pro		
Calibration constant, C			[-]	1.003	
			Pushed	Pre-drilled	
Needle insertion method:			x		
			Current, I		
Test data					
Heating data					
				$y = 0.1395x + 19.912$ $R^2 = 0.9998$	
				◆ Heating data	
				— Linear (Heating data)	
Cooling data					
				$y = 0.1497x + 19.202$ $R^2 = 0.9995$	
				◆ Cooling data	
				— Linear (Cooling data)	
Test results					
Thermal Conductivity, K		[W m ⁻¹ K ⁻¹]	2.207	Thermal Resistivity, ρ	
				[(m K W ⁻¹)]	
Notes: Measurements have been performed on saturated sample.					
COWI		Thermal Conductivity		Test standard: ASTM D 5334 (2008)	
Lab. tech.:		SNHS	Date:	15-04-2021	Project:
Checked:		MATP	Date:	16-04-2021	Job no.:
Approved:		HRMO	Date:	16-04-2021	Boring no.:
					Depth [m]:
					Encl. no.:
					Sample no.:
					Revision
					1.11
					1.0

Sample parameters					
Geological classification		CLAY, very high plasticity, with many thin layers of silt			
Sample Preparation:		Undisturbed soil sample, Thin-Walled steel tube, $\varnothing 72\text{mm}$			
Sample diameter, D	[mm]	72	Bulk Density, ρ_m	[Mg/m ³]	1.82
Sample height, H	[mm]	27	Dry Density, ρ_d	[Mg/m ³]	1.38
Moisture content, w	[%]	32.4	Moist unit weight, γ_m	[kN/m ³]	17.9
Particle density, ρ_s (assumed)	[Mg/m ³]	2.65	Dry Unit weight, γ_d	[kN/m ³]	13.5
Initial Degree of Saturation	[%]	93	Void Ratio, e	[-]	0.92
Apparatus					
Product and model no.:			Decagon KD2 Pro		
Sensor:			Decagon TR-1 (100 mm)		
Calibration constant, C			1.003		
Heat input, Q			[W/m]		
Read time			[min.]		
Needle insertion method:			x		
Current, I			[A]		
Test data					
<div><div><div>Heating data</div><div><div><div>$y = 0.1903x + 21.145$ $R^2 = 1$</div><div><div>◆ Heating data</div><div>— Linear (Heating data)</div></div></div></div><div><div>Cooling data</div><div><div><div>$y = 0.2015x + 20.499$ $R^2 = 0.9998$</div><div><div>◆ Cooling data</div><div>— Linear (Cooling data)</div></div></div></div></div></div></div>					
Test results					
Thermal Conductivity, K		[W m ⁻¹ K ⁻¹]	1.669	Thermal Resistivity, ρ	
				[(m K W ⁻¹)]	0.599
Notes:					
<div><div><div>COWI</div><div>Thermal Conductivity</div><div>Test standard: ASTM D 5334 (2008)</div></div><div><div>Lab. tech.: SNHS</div><div>Date: 14-04-2021</div><div>Project: Thor offshore wind farm Landfall site</div><div>Encl. no.: 1.12</div></div><div><div>Checked: MATP</div><div>Date: 16-04-2021</div><div>Job no.: A224691-001</div><div>Sample no.: 26A</div></div><div><div>Approved: HRMO</div><div>Date: 16-04-2021</div><div>Boring no.: B/CPT5</div><div>Depth [m]: 13.0-13.4</div></div><div><div>Revision</div><div>1.0</div></div></div>					



Enclosure 1.131.0

Legend

TOPSOIL

Postglacial deposits

SAND and GRAVEL (S1)

Lateglacial/Glacial deposits

CLAY (C1)

CLAY TILL (C2)

SAND and GRAVEL (S2)

Miocene deposits

CLAY (C3)

SAND (S3)

GYTTJA (G1)

Terrain along the centerline (DHM/Terrain (0.4 m), Styrelsen for Dataforsyning og Effektivisering.

Borehole

B/CPT5

Borehole no.

CPT

CPT1

CPT no.

Water level in stand pipe and date for measurement 20210329

Layer boundary

Soil signature (see enclosure)

Coordinates on this drawing refer to UTM32 ETRS89

Vertical heights refer to DVR90

VER. | DATE | REMARKS | DRAW. | CHECKED | APPROVED

Energinet Eltransmission A/S

Thor offshore wind farms. Landfall site investigations

Geotechnical Investigations

Geotechnical longitudinal section

PROJECT NO.

A224691

DRAW.

LNJE

CHECKED

HRMO

APPROVED

HRMO

REMARKS

SCALE

1:200 / 1:1000

DATE

2021.04.16

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ENCLOSURE NO.

1.13

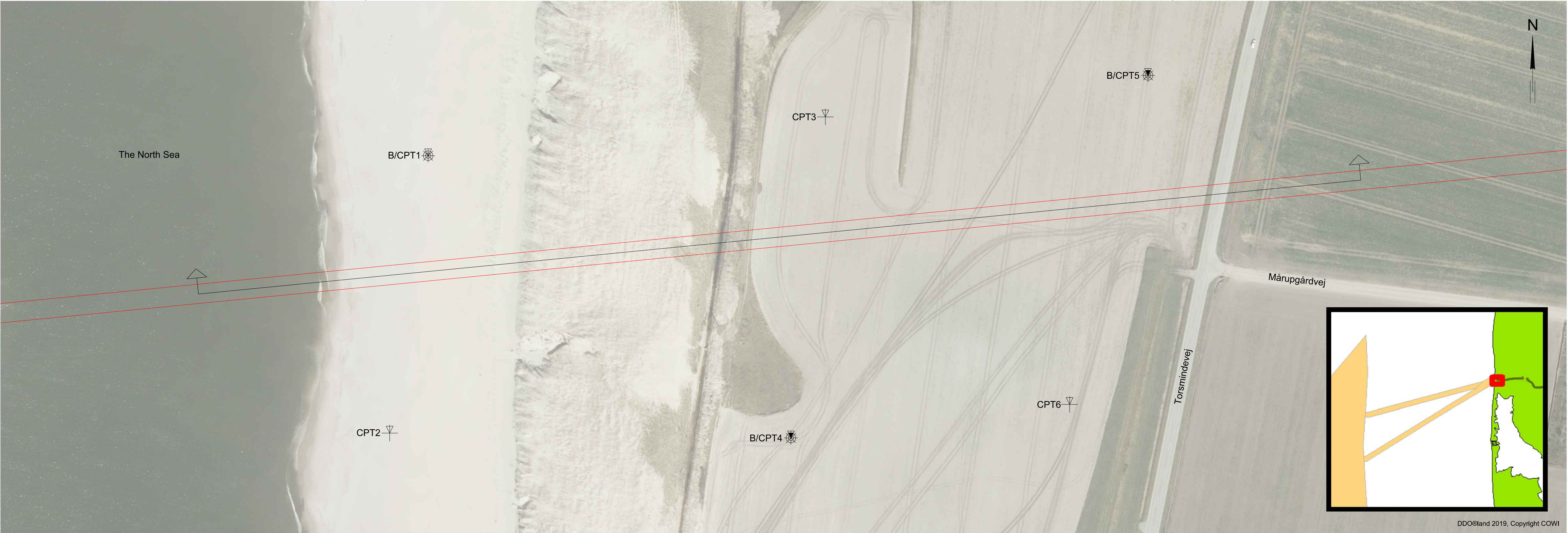
VERSION

1.0

LNJE

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21-04-2021 12:07:09



Legend

- Borehole with CPT and SPT
- Borehole with CPT
- CPT

Coordinates on this drawing refer to UTM32 ETRS89
Vertical heights refer to DVR90

VER.	DATE	REMARKS	DRAW.	CHECKED	APPROVED
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Energinet Eltransmission A/S
Thor offshore wind farms. Landfall site investigations

Geotechnical Investigations	PROJECT NO.	A224691
Location plan	DRAW.	LNJE
	CHECKED	HRMO
	APPROVED	HRMO
REMARKS	SCALE	1:1000
	DATE	2021.04.16